

DYESS TESTING LABORATORY, INC.

PROFESSIONAL TESTING & INSPECTIO
CHEMICAL & MATERIALS TESTIN

BUSINESS PHONE: 806 - 372-4911
RESIDENCE PHONE: 806 - 355-7734

506 SOUTH LIPSCOMB
AMARILLO, TEXAS 7910

March 3, 1975

Mr. Pat Christal
% City of Amarillo
P. O. Box 1971
Amarillo, Texas

Dear Sirs:

On Feb. 12, 1975 a site investigation was conducted on Section 126, Block 9, of the BS & F Survey Northwest of Amarillo. The soils investigation was performed to secure approval of this site as a sanitary landfill. This investigation was conducted as requested by your office.

The section of land is two miles North and two miles East of Bushland. The major portion of the section is pasture land, covered with native grass, and a large excavation utilized as a caliche pit. The section drains to the North & Northeast and is well drained in its present condition. Approximately 100 to 120 acres, located in the southwest quarter of the section, are under cultivation and irrigated permanent pasture.

The following general subsurface & site conditions exist at this section location:

1. The soil in the Northwest quarter-section is predominately caliche and sandy clay. This quarter has some abrupt grade changes from the canyons and hills. Some grade changes of 80 to 100-ft. will exist between the high and low areas. Some rock will be encountered in this quarter section.
2. A "caliche pit" is located at the East edge of the Northwest quarter-section. This pit has had an extensive quantity of

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material removed and still has a significant amount of usable caliche available.

3. The Northeast quarter section is "rolling" pastureland. The low hills have only 1 to 2-ft. of topsoil, turning to Reddish-tan to Dark tan Sandy Clay at all other depths. Rock was encountered at 50 to 55-ft. in this area.
4. The Southeast quarter section is fairly level pastureland. This area is easily excavated and should serve as an excellent area for a landfill operation.
5. The southwest quarter section is mostly farmland and under irrigation. This quarter section is nearly level with some grade change and drainage to the North and East. This quarter-section has more topsoil (3 to 5-ft.) than any other area of the section. No rock or sand was encountered in this quarter section to the 40-ft. drilled depth.

Soil classification and plastic properties are as follows:

<u>Type soil</u>	<u>Liquid Limit(%)</u>	<u>Plasticity Index</u>	<u>Linear Shrinkage(%)</u>	<u>Permeability (cm/sec.)</u>
Reddish-Tan "Caliche"(CL)	32.6	12.2	4.7	1.3×10^{-7}
DK.Reddish-Tan Sandy Clay(CL)	35.1	16.3	8.9	8.1×10^{-8}
Lt.Tan to Reddish-Tan Sandy Clay	36.7	17.8	9.7	2.3×10^{-8}
Lt.Tan "Caliche"(CL)	30.1	10.7	3.6	6.3×10^{-7}
Sand Reddish-Tan (SC)	28.1	8.6	2.3	7.7×10^{-5}
Brown to Dk.Brown(Topsoil)(CL)	38.9	18.2	10.3	2.9×10^{-8}
Lt.Reddish-Tan Sandy Clay(CL)	33.6	14.9	7.8	3.6×10^{-8}

Note: The above samples are typical of the soil types encountered at the locations indicated on the attached Logs of Borings.

The only areas where sand or rock will be a problem is the vicinity of Boring No. 3 and to the East to the area of Boring No. 9. The

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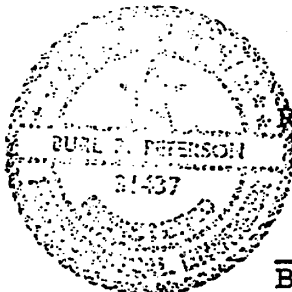
506 SOUTH LIPSCOMB
AMARILLO, TEXAS 791

higher hills and deep canyons are located in the area between Borings No. 3, 4 and 9 (see attached Location of Borings. The sand encountered in Boring No. 3 will have a solid rock strata beneath it, however, due to "caving" the drill was withdrawn at the 40ft. depth.

This site should meet all Texas Water Quality Board requirements, for permeability, due to the impervious clay stratas in all areas except the sand in the Northwest portion, which, has a solid limestone or "caliche" strata beneath it. The area of this sand (Boring No. 3) will probably not be utilized, as a landfill, due to layers of hard to highly cemented limestone and caliche located fairly shallow depths.

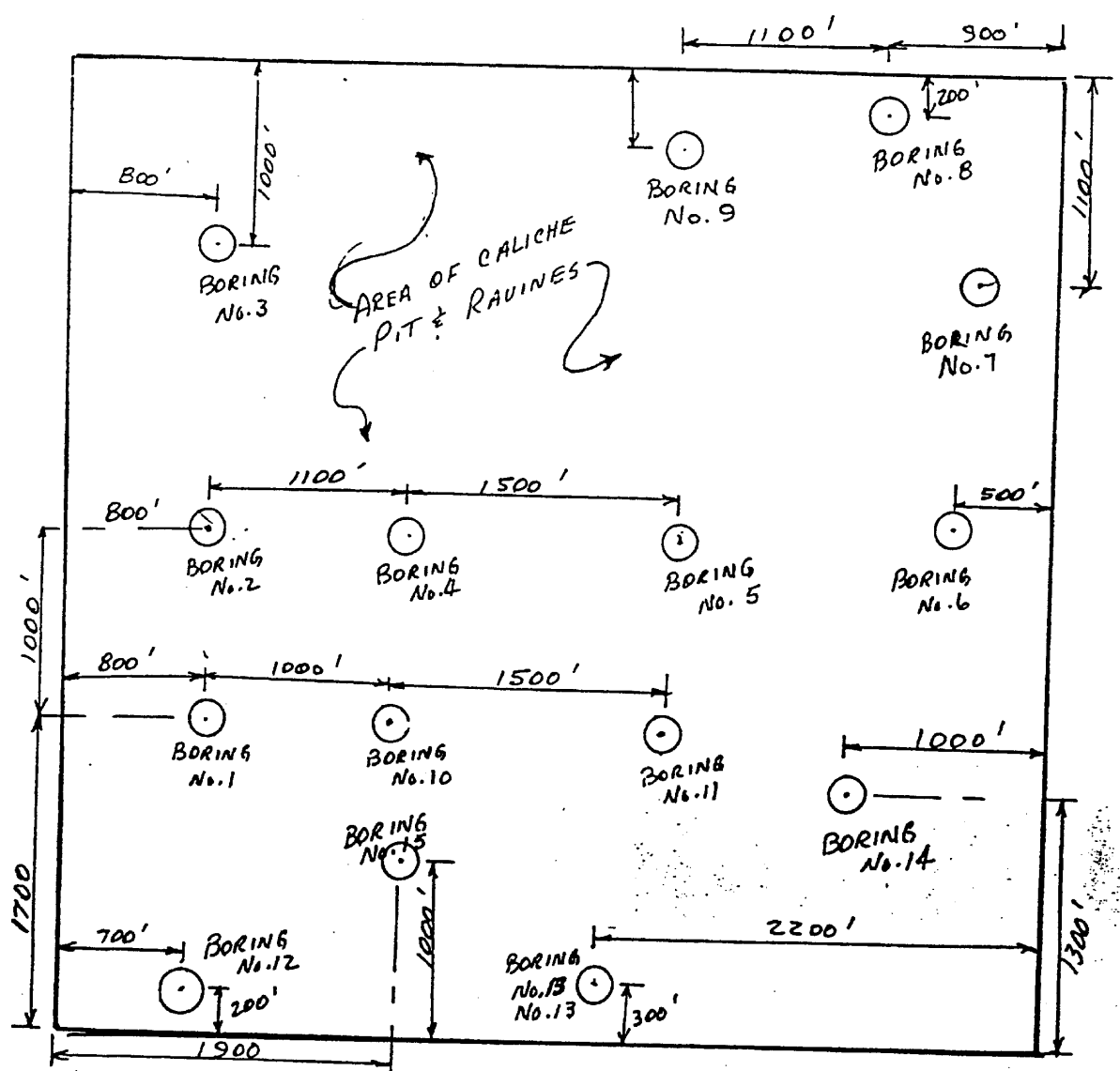
SUMMARY & CONCLUSIONS

The site of this soil investigation (Section 126, Block 9 - B.S. & F Survey) should serve as an adequate sanitary landfill. The Northwest Quarter-Section may have up to 10% or 15% of its area with unsuitable soil or rock conditions. The soil in all areas, has a permeability rate of less than 1.0×10^{-7} cm./sec., or is underlaid by an impervious strata of rock or highly cemented caliche. Groundwater in this area is at 175 to 210-ft. depth. The entire section is sloped to provide adequate drainage and should present no significant excavation problems. There are sufficient canyons to be filled with the excess soil, excavated from the burial trenches, to dispose of any waste.



Respectively Submitted

Burl R. Peterson P.E.
Burl R. Peterson, President

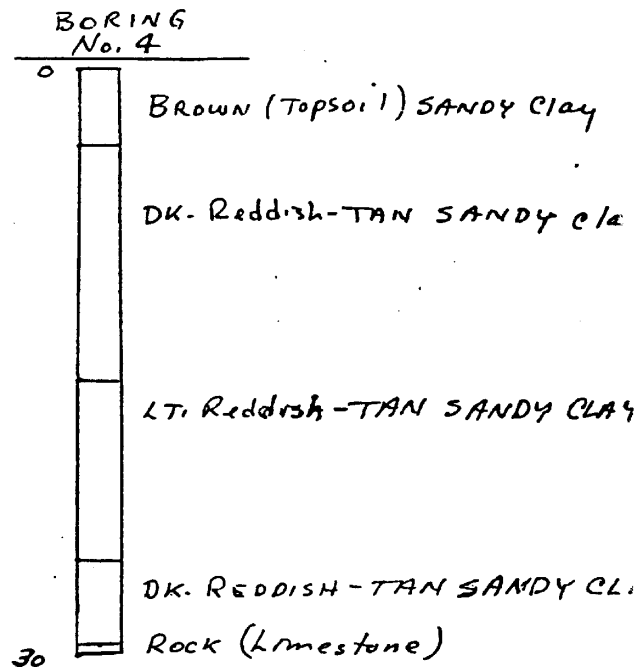
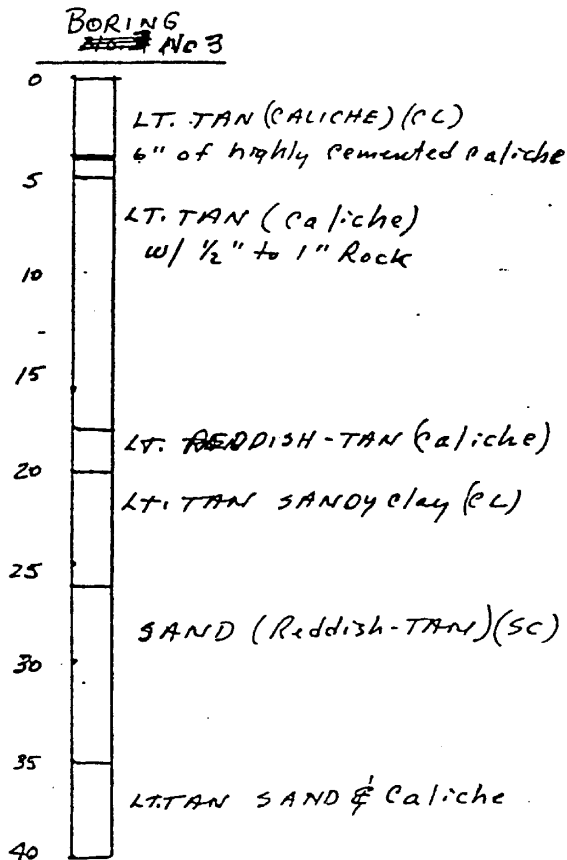
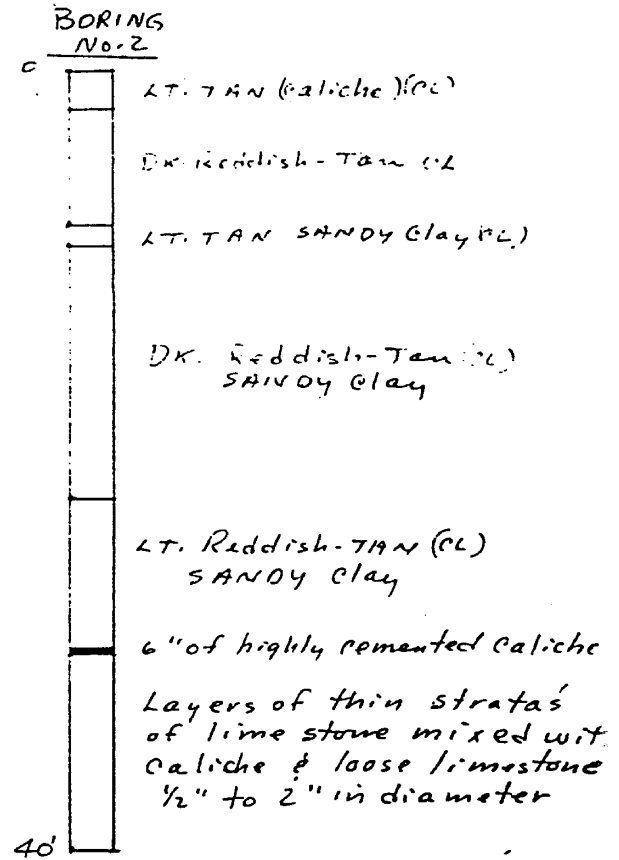
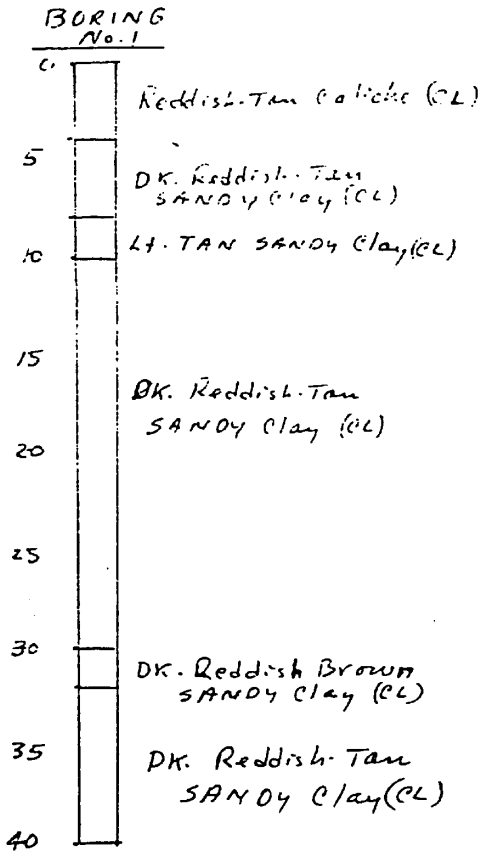


LOCATION OF BORINGS

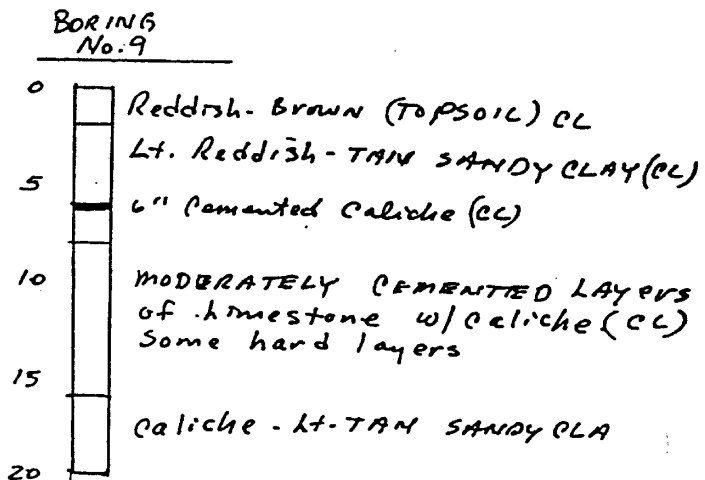
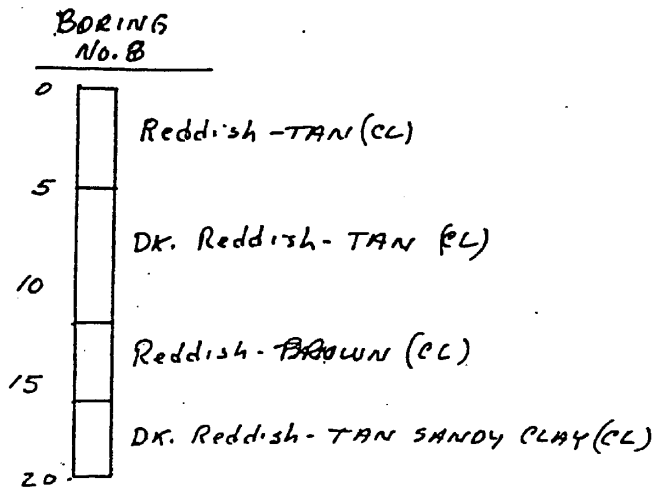
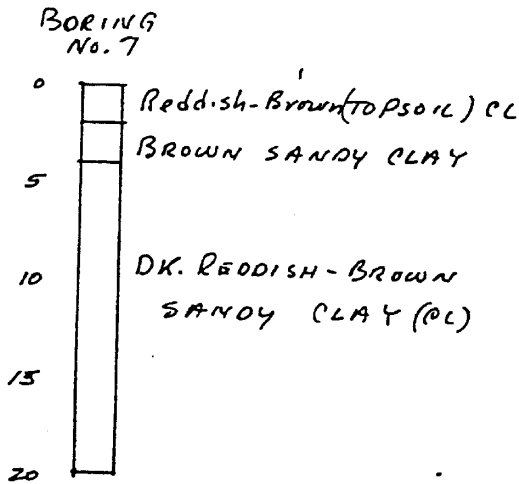
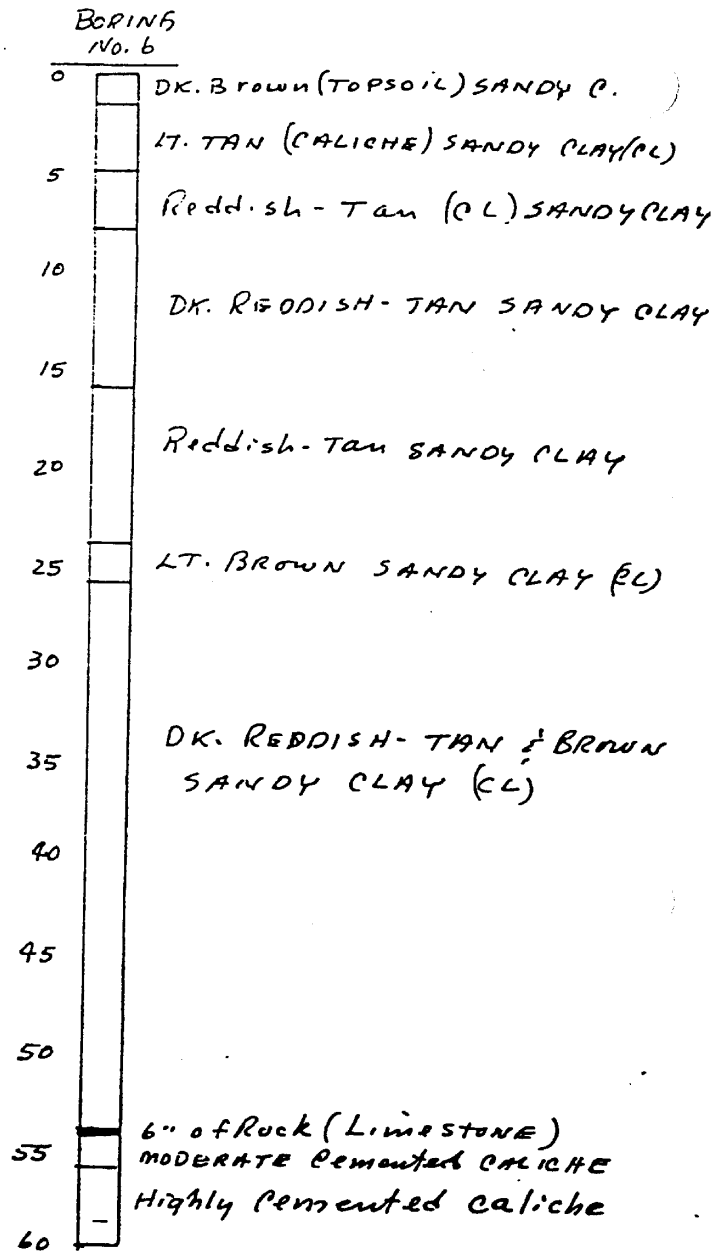
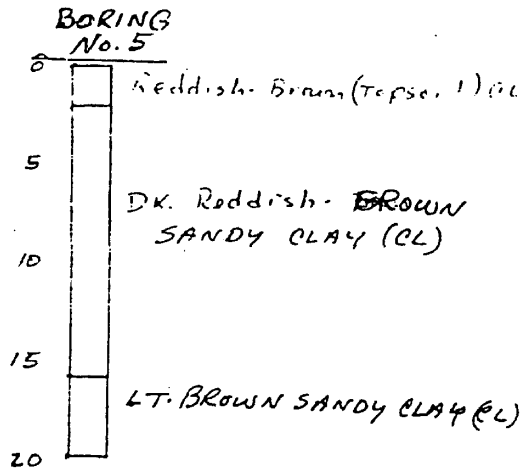
SECTION 126, BLOCK 9 - BS & F SURVEY

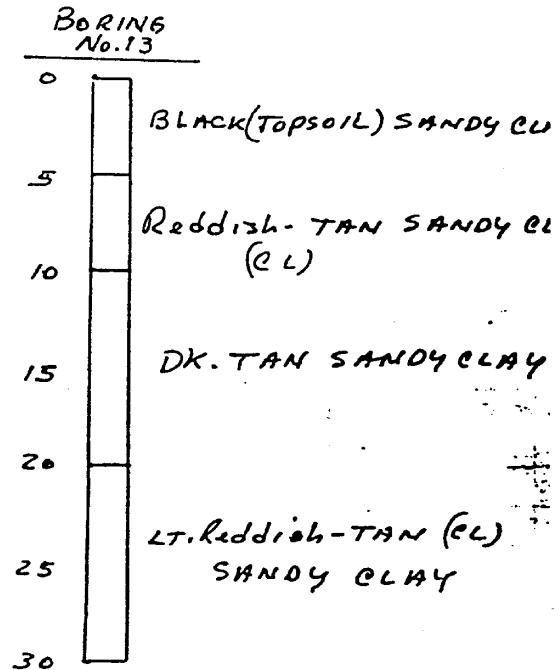
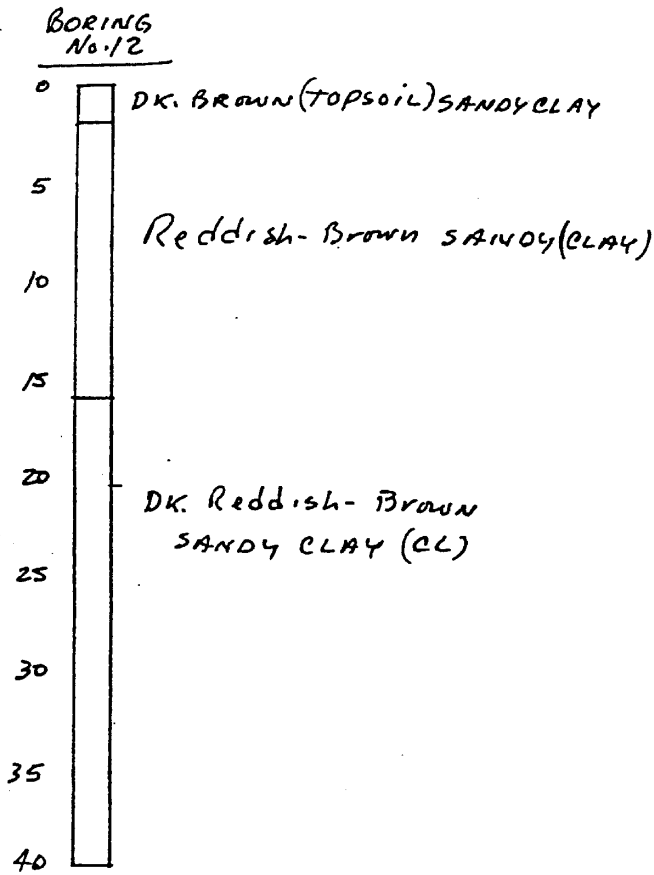
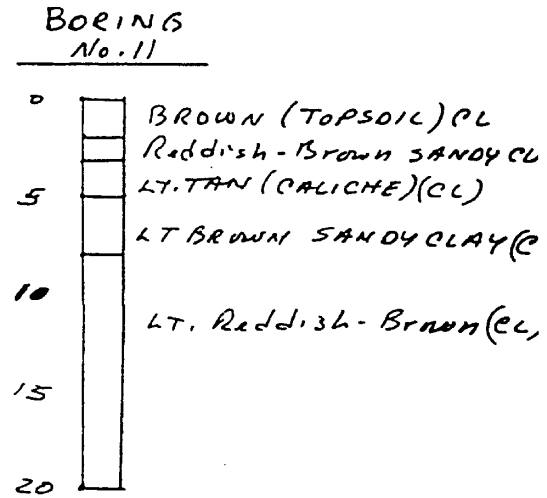
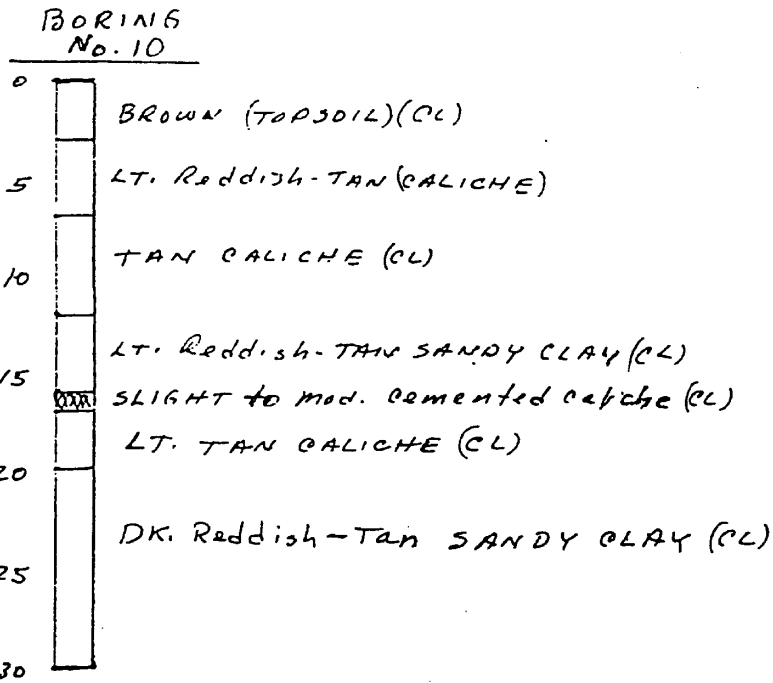
2/26/75
1" = 1000'

LIST OF BORINGS



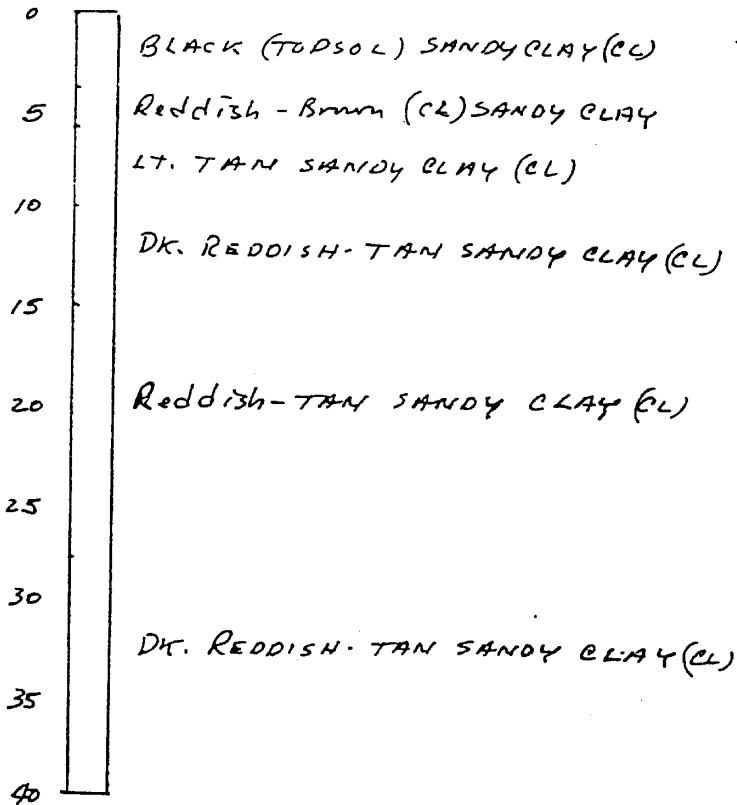
LOG OF BORINGS



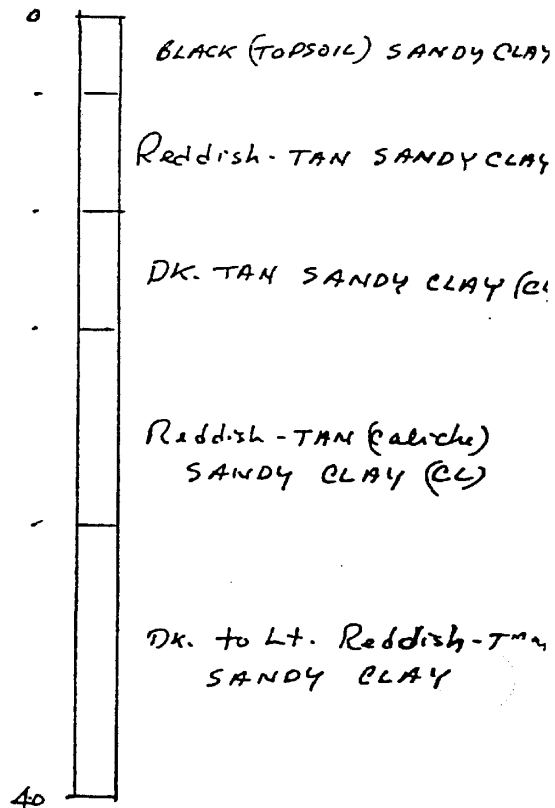


LOG OF BORINGS

BORING
No. 14



BORING
No. 15



APPENDIX G

1979 SITE INVESTIGATION REPORT

BUSINESS PHONE: 806 - 372-4911
RESIDENCE PHONE: 806 - 355-7734

506 SOUTH LIPSCOMB
AMARILLO, TEXAS 79101

September 28, 1979

City of Amarillo
% Pat Christal
P.O. Box 1971
Amarillo, Texas

Re: Landfill Site - Soil Borings

SITE INVESTIGATION & RESULTS

On 8/30/79 this Engineer drilled four (4) borings to determine the subsurface soils conditions. The main concern was the permeability and strata types to be utilized as a land fill area.

Boring No. 1 was located in the area of a liquid waste pit. The soil in this boring was sand from 0 to 26-ft. The soil is classified as Silty or Clayey Sand (SM-SC) and silty sand (SM) at all depths. The permeability of the soil from 0 to 3-ft. is 4.1×10^{-6} cm./sec. and 6.3×10^{-6} cm./sec. from 3 to 12-ft. This soil will require a lining, in any liquid pit, of at least 4-ft. of compacted clay soil. This soil should have a P.I. of at least 18 and a permeability rate $K = 1.0 \times 10^{-7}$ cm./sec. minimum. This lining should be compacted to at least 95% of maximum dry density (ASTM Designation: D698-70).

The borings 2, 3 & 4 were taken in the area of proposed future landfill sites. The areas were designated by Mr. Pat Christal and drilled to the 26-ft. depth. These borings indicate similar soil (SM & SM-SC) at all depths, except, boring No. 4 where some Sandy Clay (CL) was encountered to the 12-ft. depth. This soil was significantly more impervious than any soil in any other boring. The rate of flow for the soil in boring No. 4 (0 to 12-ft.) is $K = 3.1 \times 10^{-7}$ cm./sec. Typical soil permeabilities in borings 2 & 3 at all depths are as follows:

Boring No. 2 0 to 15-ft. $K = 4.6 \times 10^{-6}$ cm./sec.

Boring No. 2 15 to 26-ft. $K = 7.1 \times 10^{-6}$ cm./sec.

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AMARILLO, TEXAS 791

Boring No. 3 0 to 10-ft. $K = 4.0 \times 10^{-6}$ cm./sec.
Boring No. 3 12 to 26-ft. $K = 5.3 \times 10^{-6}$ cm./sec.
Boring No. 4 12 to 26-ft. $K = 6.2 \times 10^{-6}$ cm./sec.

There are some isolated layers of cemented limestone in boring No. 3 & 4. The strata at 18-ft. was 4-in. in thickness and was moderately hard, however, normal earth moving equipment will be able to excavate the strata.

All soil properties are shown on the attached Summary of Tests. All soil stratas encountered are shown on the Log of Borings.

LIMITATIONS

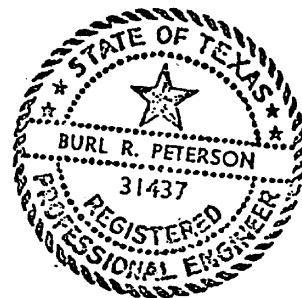
The above recommendations are based on the assumption that the soil and soil properties in the area between the borings are reasonably uniform the similar to those found in the borings. It is also assumed that the moisture levels encountered at this site will not be permitted to materially increase over those shown on the tests.

If any unusual conditions, not described in this report, are encountered during construction, this laboratory should be notified immediately.

Respectively Submitted,

Burl R. Peterson P.E.

Burl R. Peterson, President



CC: Above

SUMMARY OF TESTS

PROJECT A Landfill for the City of Amarillo, Texas

Drilled on:

DATE: 8/30/79

CLIENT City of Amarillo

BORING NO.	DEPTH FEET	TYPE OF MATERIAL	MOISTURE CONTENT %	LINEAR SHRINKAGE %	LIQUID LIMIT	PLASTICITY INDEX	NO. BLOWS	SOIL CLASSIFICATION	ALLOWABLE LOAD BEARING VALUE LBS./SQ FT
1	1	Reddish Tan Silty & Clayey Sands	5.7	3.2	23.2	5.8		SM-SC	
	3	Dk. Reddish Tan Silty Sand	6.0	1.6	20.3	2.7		SM	
	12	Same	6.0	Similar to Soil @ 3-ft.				SM	
	20	Lt. Reddish Tan Silty & Clayey Sands	6.6	3.2	23.3	5.7		SM-SC	
	26	Dk. Reddish Tan Silty Sand	4.4	3.0	23.0	5.2		SM	
2	1	Brown Silty & Clayey Sands	7.8	3.4	23.6	5.9		SM-SC	
	3 1/2	Lt. Reddish Silty & Clayey Sands	3.5	3.0	22.6	4.5		SM-SC	
	12	Same	4.1	Similar to Soil @ 3 1/2-ft.				SM-SC	
	16 to 26	Reddish Tan Silty Sand	4.2	3.6	25.3	5.9		SM	

SUMMARY OF TESTS

PROJECT A Landfill for the City of Amarillo, Texas

Drilled on:
DATE: 8/30/79

CLIENT City of Amarillo

BORING NO.	DEPTH FEET	TYPE OF MATERIAL	MOISTURE CONTENT %	LINEAR SHRINKAGE %	LIQUID LIMIT	PLASTICITY INDEX	NO. BLOWS	SOIL CLASSIFICATION	ALLOWABLE LOAD BEARING VALUE LBS./SQ FT
3	1	Dk. Brown Clayey Sand	12.5	6.2	30.1	12.3		SC	
	2	Lt. Reddish Tan Silty & Clayey Sands	3.4	3.3	23.9	5.9		SM-SC	
	8	4" Limestone Rock		Moderately Hard					
	10	Reddish Tan Silty Sand	3.5	3.0	23.2	5.1		SM	
	15 to 26	Lt. Reddish Tan Silty & Clayey Sands	3.4	3.0	22.8	4.6		SM-SC	
4	1	Dk. Brown Sandy Clay	12.4	5.6	27.9	9.1		CL	
	3	Brown Sandy Clay	5.2	5.5	26.3	8.7		CL	
	9	Dk. Tan Sandy Clay	5.0	5.6	28.0	9.0		CL	
	12	Reddish Tan Silty Sand	3.4	3.1	23.0	5.6		SM	
* 15 to 26		Lt. Reddish Tan Silty & Clayey Sands	3.6	3.2	23.3	5.6		SM-SC	
	*4"	Limestone @ 18'							

KEY TO CLASSIFICATION USED ON LOGS

MAJOR DIVISIONS			GROUP SYMBOLS	DESCRIPTIONS	
COARSE-GRAINED SOILS More Than Half of Material is LARGER Than No. 200 Sieve Size.	GRAVELS More Than Half of Coarse Fraction is LARGER Than No. 4 Sieve Size.	Clean Gravels (Little or no Fines)	GW	Well-Graded Gravels, Gravel-Sand Mixtures, Little or no Fines.	
		Clean Gravels (Little or no Fines)	GP	Poorly-Graded Gravels, Gravel-Sand Mixtures, Little or no Fines.	
		Gravels With Fines (Appreciable Amount of Fines)	GM	Silty Gravels, Gravel-Sand-Silt Mixtures.	
		Gravels With Fines (Appreciable Amount of Fines)	GC	Clayey Gravels; Gravel-Sand-Clay Mixtures.	
	SANDS More Than Half of Coarse Fraction is SMALLER Than No. 4 Sieve Size.	Clean Sands (Little or no Fines)	SW	Well-Graded Sands, Gravelly Sands, Little or no Fines.	
		Clean Sands (Little or no Fines)	SP	Poorly-Graded Sands, Gravelly Sands, Little or no Fines.	
		Sands With Fines (Appreciable Amount of Fines)	SM	Silty Sands, Sand-Silt Mixtures.	
		Sands With Fines (Appreciable Amount of Fines)	SC	Clayey Sands, Sand-Clay Mixtures.	
		FINE-GRAINED SOILS More Than Half of Material is SMALLER Than No. 200 Sieve Size.	SILTS and CLAYS Liquid Limit Less Than 50	ML	Inorganic Silts & Very Fine Sands, Rock Flour, Silty or Clayey Fine Sands or Clayey Silts with Slight Plasticity.
				CL	Inorganic Clays of Low to Medium Plasticity, Gravelly Clays, Sandy Clays, Silty Clays, Lean Clays.
OL	Organic Silts & Organic Silty Clays of Low Plasticity.				
SILTS and CLAYS Liquid Limit Greater Than 50	MH		Inorganic Silts, Microceous or Diatomaceous Fine Sand or Silty Soils, Elastic Silts.		
	CH		Inorganic Clays of High Plasticity, Fat Clays.		
	OH		Organic Clays of Medium to High Plasticity, Organic Silts.		
Highly Organic Soils	Pt	Peat & Other Highly Organic Soils			

LOG OF BORING

Texas

PROJECT: A Landfill for the City of Amarillo,
 CLIENT: City of Amarillo - % Pat Christal

BORING NO.: 1 & 2
 LOCATION: As Directed by Pat Christal

Date: 9/27/79

Ground Elevation: Existing

Depth, Feet	Symbol	Sample	Legend:		
			☐ Sample	✕ Penetration	▽ Water
BORING NO. 1			Description of Stratum		
			Reddish Tan Silty & Clayey Sands (SM-SC)		
5			Dk. Reddish Tan Silty Sand (SM)		
10			Dk. Reddish Tan Silty Sand (SM)		
15			Dk. Reddish Tan Silty Sand (SM)		
20			Lt. Reddish Tan Silty & Clayey Sands (SM-SC)		
25			Dk. Reddish Tan Silty Sand (SM)		
			Borings Nos. 1 & 2 were advanced to the 26-ft. depth without the use of drilling fluid. No groundwater or hard rock was encountered to the drilled depth.		
BORING NO. 2			Description of Stratum		
			Brown Silty & Clayey Sands (SM-SC)		
5			Lt. Reddish Silty & Clayey Sands (SM-SC)		
10			Lt. Reddish Silty & Clayey Sands (SM-SC)		
15			Lt. Reddish Silty & Clayey Sands (SM-SC)		
20			Reddish Tan Silty Sand (SM)		
25			Reddish Tan Silty Sand (SM)		

LOG OF BORING Texas

PROJECT: A Landfill for the City of Amarillo, BORING NO.: 3 & 4
 CLIENT: City of Amarillo - % Pat Christal LOCATION: As Directed by Pat Christal
 Date: 9/27/79 Ground Elevation: Existing

Depth, Feet	Symbol	Sample	Legend:		
			☐ Sample	✕ Penetration	▽ Water
			BORING NO. 3	Description of Stratum	
				Dk. Brown Clayey Sand (SC)	
5				Lt. Reddish Tan Silty & Clayey Sands (SM-SC)	
				4" Limestone Rock	
				Lt. Reddish Tan Silty & Clayey Sands (SM-SC)	
10				Reddish Tan Silty Sand (SM)	
15					
20				Lt. Reddish Tan Silty & Clayey Sands (SM-SC)	
25					
			Borings No. 3 & 4 were advanced to the 26-ft. depth without the use of drilling fluid. No groundwater was encountered. Hard rock was encountered in both borings, in No. 3 @ 8' & in Boring No. 4 @ 18'		
			BORING NO. 4		
				Dk. Brown Sandy Clay (CL)	
5				Brown Sandy Clay (CL)	
10				Dk. Tan Sandy Clay (CL)	
15				Reddish Tan Silty Sand (SM)	
				Lt. Reddish Tan Silty & Clayey Sands	
				4" Limestone	
20					
				Lt. Reddish Tan Silty & Clayey Sands	
25					

APPENDIX B
LIMITED GROUNDWATER CHARACTERIZATION INVESTIGATION

LIMITED GROUNDWATER CHARACTERIZATION INVESTIGATION

**CITY OF AMARILLO
MUNICIPAL SOLID WASTE LANDFILL PERMIT NO. 73
POTTER COUNTY, TEXAS**

Prepared by:

HDR Engineering, Inc.
12700 Hillcrest Road, Suite 125
Dallas, Texas 75230
(214) 960-4400

December 1994



Brad A. McCardell
Geologist

12/15/94

**CITY OF AMARILLO
MUNICIPAL SOLID WASTE LANDFILL PERMIT NO. 73
POTTER COUNTY, TEXAS**

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Appendix A	Data From Area Well Survey
Appendix B	Slug Testing Data and Calculations

1.0 INTRODUCTION

The City of Amarillo operates a Type I Municipal Solid Waste Landfill (MSWL) under permit No. 73 issued by the Texas Department of Health, dated March 17, 1975. This report presents data collected during a limited groundwater characterization investigation at the existing facility. In conjunction with the groundwater data, a soils investigation report has been prepared by Dyess-Peterson Drilling and Testing, Inc. (Amarillo, Texas). Both of these reports were prepared to satisfy the requirements of Attachments 4 and 5 in the Texas Natural Resource Conservation Commission (TNRCC) MSWL 30 TAC 330 regulations.

The purpose of this limited groundwater characterization investigation was to 1) drill, sample borings, and install monitor wells to assess subsurface soil and groundwater conditions, and 2) bring the facility into compliance with the MSWL regulations for groundwater monitoring. The monitor wells were installed in accordance with the HDR Engineering, Inc (HDR) plan entitled, Groundwater Monitoring System Plan, For City of Amarillo Municipal Solid Waste Landfill Permit No. 73, Potter County, Texas, dated August 31, 1993 and approved by Mr. Dick Smith of the TNRCC (letter, dated December 14, 1993).

2.0 BACKGROUND

2.1 Site Conditions

The permitted landfill consists of one square mile of property located approximately 4 miles west of the City of Amarillo and two miles north of Interstate 40 (Figure 1). Currently, approximately 80 - 90 acres of property have been developed as landfill. Landfilling is currently taking place near the center of the one square mile and consists of an areal fill method (Figure 2).

Prior to this investigation, 19 borings were drilled during two geotechnical investigations conducted in February 1975 and August 1979. These two investigations focused on characterizing the soil conditions for development of the landfill. A groundwater investigation was not performed during either of these previous investigations. These two investigations indicated that the site consisted of a sandy clayey top soil that is underlain by sandy clay, silty sand, clayey sand, and caliche to the total depth drilled of 50 feet.

2.2 Physiography and Topography

The site lies within the Southern High Plains (High Plains) physiographic region in the Texas Panhandle (Figure 3). The High Plains encompasses approximately 22,000

square miles and extends eastward where it is defined by a sharp escarpment several hundred feet high (Cronin, 1971). The Southern High Plains form a relatively flat plateau that slopes toward the southeast at approximately 10 feet per mile. The surficial deposits consist mainly of clays and loams (Nativ, 1988) and also sandy and silty loams and fine sandy loams (Knowles, 1984). Figure 4 shows a distribution of soil types within Potter County, Texas.

Immediately to the north of the site is the Canadian River Basin, which has eroded much of the overlying surficial material and created essentially a large valley or canyon feature. Several tributaries branch off the main system creating valley and plateau features which gives rise to a much more pronounced relief in this area compared to areas farther south on the High Plains.

The site topography ranges from approximately elevation 3,700 feet on the northern section to approximately 3,800 feet on the southern section (Figure 5). The majority of the site is fairly flat with little relief. However, the northern section of the property is dissected by three main drainage features that divert drainage from the site to the north. These drainage features are most likely associated with the Canadian River Basin. The change in relief on the northern section of the site can be as much as 100 feet.

2.3 Climate and Precipitation

The High Plains area is essentially characterized as a semi-arid climate with an average mean precipitation ranging from 13 to nearly 20 inches annually (NOAA, No. 81, 1992). According to the data collected for a 30 year average, precipitation averages approximately 19 inches annually in the Amarillo area (TxDOT, 1993). The greatest amount of rainfall occurs during the months of May through July. In the High Plains area, evaporation rates typically range from 60 to 91 inches annually. This portion of Texas is typically windy with an average velocity of 15.5 mph in the winter months. The average annual wind velocity is 13.7 mph.

2.4 Area Well Survey

A review of agency files was conducted to locate existing wells in the area of the landfill. The agency search consisted of reviewing file records from the TNRCC, Texas Department of Water Resources, and the Texas Water Development Board (TWDB). At least 23 wells are reported. Of the 23 wells reported, 14 wells are within a one-mile radius of the site. Three of the 23 wells are located on the western portion of the landfill property. The first well, No. 07-56-301, is used by the landfill periodically to control dust on the access roads; the second well, identification unknown, is used as a source of potable water, and the third well, identification

unknown, is connected to a windmill that is not operational. Figure 6 shows the location of the wells relative to the landfill. Except for the wells on site, the remaining wells are used for irrigation purposes and draw water from the Ogallala Formation. One well (State No. 07-56-307) is also used as an observation well. This well is located just to the south of the landfill. Data from the TWDB indicates that the yields from these wells when they were installed ranged from 400 to 800 gallons per minute. Recent data is unavailable. Information for the wells found during the search is presented in Appendix A.

Water quality data collected from well No. 07-56-307 in 1980 indicated a total dissolved solids (TDS) concentration of 350 milligrams per liter (MGL).

3.0 REGIONAL GEOLOGY

3.1 Stratigraphy

The stratigraphy of the High Plains consists of deposits ranging in age from the Permian to Recent. In general, the deposits consist of sandstone, shales, limestones, clays, sands, and windblown deposits of sands and clays near the surface. The primary water-bearing deposits in the High Plains area are usually from the Cretaceous and Tertiary deposits. Of these deposits, the Ogallala (Pliocene Age) and the Washita, Fredericksburg, and Trinity groups (Cretaceous Age) supply the majority of the usable water in the High Plains. The general stratigraphy for the area is summarized in Figure 7.

In the vicinity of the Amarillo area, the Jurassic and Cretaceous deposits are absent. The stratigraphy consists in general of the Ogallala Formation unconformably overlying rocks of Triassic and Permian Ages (Nativ, 1988). In the Amarillo area, the Ogallala Formation specifically overlies rocks of Triassic age (Figure 8). Directly overlying the Ogallala are deposits consisting primarily of silty sands, fine sands, clays, and loams of the Blackwater Draw Formation that have been deposited by either wind or fluvial deposition. Near the top of the Ogallala Formation, caliche is typically encountered which is usually referred to as the "Caprock". The caprock forms an east facing escarpment toward the eastern most extent of the High Plains area. Triassic deposits are exposed north of Amarillo along the Canadian River Basin where the Canadian River has eroded the overlying Ogallala Formation. The thickness of these deposits has been measured up to 150 feet along portions of the Canadian River valley. The Triassic deposits are of continental origin (Cronin, 1971) and have been named the "Dockum Group" and typically consist of varicolored shale to sandy shale, sandstone, and conglomerate. Depending on the location within the High Plains, the Dockum Group can be subdivided into at least three formations consisting of 1) Tecovas Formation (basal member), 2) Santa Rosa Formation (middle member), and

3) Chinle Formation (upper member). The Triassic deposits also are typically referred to as the "redbed" because of their reddish color throughout the section.

3.2 Depositional History

According to Seni (1980), the Ogallala Formation was deposited in a deltaic environment as a series of overlapping alluvial fans derived from deposits from the uplift of the southern Rocky Mountains to the west. Figure 9 shows a generalized depositional facies map of the Ogallala. Prior to the deposition of the Ogallala, streams originating from the west eroded the existing Permian, Triassic, Jurassic, and Cretaceous strata forming valleys and basins. The erosion of these strata occurred until at least late Miocene to early Pliocene at the time when the climate was arid.

The Dockum Group is of continental origin and is believed to have been deposited as river-channel and flood-plain deposits (Cronin, 1971). Seni, 1988 indicates the depositional setting involved braided and meandering streams, alluvial fan deltas, lacustrine deltas, lacustrine systems, and mud flats. These deposits were laid down in a basin feature that underwent folding prior to and after deposition. The resultant surface of the Triassic deposits was one of valleys and basins.

3.3 Structure

The site lies within the northern portion of the Palo Duro Basin, which is considered a small subbasin to the Permian Basin of southwest Texas (Gustavson and others, 1981). To the northeast is the Amarillo uplift and to the south is the Matador Arch. The uplifts are thought to have occurred as the result of movement along high-angle reverse faults. Faulting within the region created displacement of small blocks which in turn formed subbasins, such as the Palo Duro Basin and others in this area. Figure 10 shows a generalized structure map of the region.

4.0 REGIONAL HYDROGEOLOGY

4.1 Ogallala Formation

The Ogallala Formation (also called the High Plains aquifer) is the major aquifer of the High Plains area. In Texas, the areal extent of the Ogallala is approximately 111,000 square kilometers (Figure 11). The Ogallala consists primarily of fluvial unconsolidated clastic deposits of sand, silt, clay and basal gravel. As discussed in Section 3.2, the Ogallala was deposited as a series of overlapping alluvial fans or lobes. Seni, 1980 describes three distinct fan lobes consisting of 1) Dalhart-Amarillo, 2) Clovis-Plainview, and 3) Brownfield-Lubbock. The site lies within the Dalhart-Amarillo fan lobe.

Throughout much of the High Plains, the Ogallala Formation is unconfined (water table conditions). In the Amarillo area, the depth to groundwater is approximately 200 to 230 feet below ground surface and the saturated thickness ranges from 0 (near the Canadian Breaks) to approximately 100 feet (McReynolds, 1990). The Canadian River Basin as well as withdrawal of groundwater are controlling factors on the depth and saturated thickness. The regional groundwater flow direction is toward the south-southeast (Figure 12) which is controlled by the structure of the High Plains. The rate of movement is on the order of 60 to 150 feet per year. The rate of movement is controlled by the gradient (approximately 0.008 ft/ft) and permeability of the material in the saturated zone. According to data presented by Knowles and others, 1984, transmissivities in the Ogallala range from approximately 315 to 201,000 gallons per day per foot (gpd/ft) with an average of 30,400 gpd/ft. In the Amarillo area, the transmissivities have been calculated to range from 6,000 to 7,000 gpd/ft (Cronin, 1971). The data presented by Cronin is in agreement with aquifer test data published by the Texas Water Development Board, Report 98 for wells in nearby Randall County. The hydraulic conductivity can range from several hundred to over 1,000 gallons per day per square foot (gpd/ft²). Based on data published by Nativ, 1988, from an aquifer test conducted near the Randall/Potter County line, the hydraulic conductivity was approximately less than or equal to 200 gpd/ft².

Recharge to the Ogallala Formation is usually small. According to data published by Knowles and others, 1984, an average of less than 0.2 inches of water reaches the water table as natural recharge. Areas where natural recharge is the highest are usually associated with where the Ogallala outcrops and caliche layers are absent, through Quaternary deposits that overlie the Ogallala, and potentially along river channels of flowing streams.

Discharge from the Ogallala occurs through natural outlets such as seeps and springs or as leakage to the underlying formations (Nativ, 1988). Similar chemical composition between the Ogallala aquifer and underlying formations that the Ogallala is in contact with suggest that flow between the Ogallala and deeper aquifers does occur. Pumping, however accounts for the greatest amount of discharge from the Ogallala.

4.1.1 Water Quality

The water quality of the Ogallala aquifer is acceptable for numerous applications. Generally, the concentrations of total dissolved solids and chloride increase from north to south on the High Plains. This is usually caused by a thinning of the aquifer and its shallower depths which make it susceptible to surface contamination from various activities. Total dissolved solids (TDS) in the Amarillo area as reported by Nativ, 1988 and Knowles and others, 1984 indicate that TDS are around 400 milligrams per liter (mg/L). Chemical data collected in August 1980 from well 07-56-307, located just

south of the site, indicated a TDS and chloride concentration of 350 and 7 mg/L, respectively. More recent data collected in September 1988 from well 06-49-101, located approximately one mile east of the site, indicated TDS and chloride concentrations of 321 and 4 mg/L, respectively. These values are well within acceptable drinking water limits.

4.2 Dockum Group

The Dockum Group is divided into at least three distinct formations. The lowermost or basal formation is the Tecovas Formation that consists of shales and clays. In localized areas the Tecovas contains lenses of fine-grained sandstone and conglomerates. The middle member is the Santa Rosa Sandstone, which is the major water-producing unit within the Dockum Group. The Santa Rosa consists of fine to coarse-grained, cross-bedded sandstone and conglomerate with interbedded shale and clay (Knowles and others, 1984). The upper formation is the Chinle Formation that consists of clays and shales. In certain areas of the section, thin layers of micaceous sandstone and conglomerate are present, which can yield small quantities of water.

The water-bearing formations of the Dockum Group are under confined conditions, except where the formation outcrops toward the east and Canadian River Basin. Groundwater flow is generally toward the east-southeast direction. Over most of the High Plains, the Dockum Group is not in hydraulic communication with the overlying Ogallala or the Cretaceous Edwards/Trinity Group. This is because of the potentiometric head difference between the Dockum Group and overlying aquifers. Also, the chemical makeup of the water between the aquifers indicates that hydraulic connection is not occurring. In the Amarillo area, the head difference between the Ogallala and underlying Dockum Group is approximately 200 feet (Dutton and others, 1986 and Nativ, 1988). Other areas within the High Plains suggest hydraulic interconnection. Recharge to the Dockum Group is negligible and according to data published by Dutton and others, 1986 it may be as low as 0.188 inches per year. Dutton and others, 1986 suggest that recharge to the Dockum Group may come from the overlying Ogallala and Edward/Trinity Formations where a downward component of flow occurs. Recharge from precipitation on the outcrop is also believed to be negligible (Dutton and others, 1986).

Water quality within the Dockum Group tends to be variable depending on it's location, but generally is considered poor because of mineralization.

5.0 SITE CONDITIONS

5.1 Groundwater Level Measurements

The groundwater encountered on site is from the Ogallala Formation. No perched groundwater above the saturated zone of the Ogallala was encountered during the drilling program. Groundwater was encountered in the eleven borings ranging from approximately 143 to 148 feet below ground surface (bgs) on the northern portion of the site to approximately 205 to 215 feet bgs on the southern portion of the site. Groundwater level measurements have been collected in the monitor wells since July 1994. Since September 20, 1994, water level measurements have been collected once a week. Table 1 summarizes the post-development stabilized groundwater elevations from July to December 7, 1994. Groundwater elevations range from approximately 3,614 feet in MW-5 to approximately 3,590 feet in MW-1 through MW-3. Hydrographs for the wells are shown on Figures 13 and 14. Except for two measurements for P-3 on October 5 and 12, 1994, the water level readings are fairly consistent for all of the wells. The two measurements for P-3 are believed to be measurement errors. The groundwater elevations are in agreement with the data in the Hydrologic Atlas for Potter County, Texas, published by the High Plains Underground Water Conservation District No. 1 (HPUWCD).

5.1.1 Groundwater Flow and Gradients

Groundwater level measurements for three dates, September 28, October 12, and October 26, 1994 are plotted on Figures 15 through 17). The data indicates that the groundwater flow is toward the southwest in the northern portion of the site and then becomes more southerly toward the southern portion of the site. Groundwater flow on the southern portion of the site is in good agreement with regional maps from the HPUWCD. The gradient in the northern portion of the site ranges from approximately 0.005 to 0.007ft/ft, and in the southern portion of the site the gradient is approximately 0.003 ft/ft. Variations in the gradient for the Ogallala are not uncommon because of the depositional history of the formation. Since the Ogallala was deposited on an irregular surface consisting of valleys and ridges, the thickness of the formation is not uniform which can cause variations in the hydraulic properties. In addition, groundwater withdrawal from pumping can also cause variations in the gradient and flow direction over time.

5.2 Aquifer Testing

On September 20 and 21, 1994, Slug tests were conducted in wells MW-2, MW-3, MW-6, P-1, P-2, and P-3 to estimate the horizontal hydraulic conductivity. The procedure involved lowering a submersible pump in the wells and pumping them for

approximately one hour. The discharge rate was checked periodically during pumping. After one hour the pump was shut off and the water level recovery was measured using an electric well sounder and a Hermit 2000 data logger. The rate of recovery was measured until the water level was nearly equal to the static level prior to pumping. The data was analyzed using Hvorslev's Method G, Bouwer and Rice (1976), and an equilibrium well equation (Driscoll, 1986). Table 2 summarizes the results of the slug tests. The data and calculations are presented in Appendix B.

The results of the hydraulic conductivity using the Bouwer and Rice method range from approximately 6.58×10^{-4} centimeters per second (cm/sec) in well MW- 3 to approximately 1.47×10^{-3} cm/sec in well P-1. The results using the Hvorslev method range from approximately 1.80×10^{-4} cm/sec in well MW-3 to approximately 3.77×10^{-2} cm/sec in well P-1. The two methods show comparable results. When the two methods are averaged, the hydraulic conductivity ranges from 4.52×10^{-4} cm/sec in well MW-3 to 1.96×10^{-2} cm/sec in well P-1. These average values are in the range of fine-grained sand to silty sand mixtures. An equilibrium equation (Driscoll, 1986) was also used to compare the results. The results from the equilibrium equation are comparable to the other two methods.

5.3 Estimated Groundwater Velocity

Based on the slug test values for the two methods, an estimated rate of groundwater movement can be calculated using a variation of Darcy's equation. Using an effective porosity of approximately 30 percent and a hydraulic gradient of 0.006 ft/ft calculated for the northern portion of the site and 0.003 ft/ft for the southern portion of the site, the flow velocity ranges from approximately 20 to 50 feet per year.

$$K = \frac{K i}{n}$$

K = Hydraulic Conductivity, 2.01×10^{-3} (north) 5.54×10^{-3} (south),
cm/sec

i = Hydraulic Gradient, 0.006 ft/ft (north), 0.003 ft/ft (south)

n = Effective Porosity, 0.30

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- 2) Dutton, A. R. and others, Hydrogeochemistry and Water Resources of the Triassic Lower Dockum Group in the Texas Panhandle and Eastern New Mexico, 1986, Report of Investigations No. 161, Bureau of Economic Geology: The University of Texas at Austin.
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- 4) Knowles, T. C. and others, Evaluating the Ground-Water Resources of the High Plains of Texas, Volume 1, Report 288, May 1984. Texas Department of Water Resources.
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- 6) Nativ, R., Hydrogeology and Hydrochemistry of the Ogallala Aquifer, Southern High Plains, Texas Panhandle and Eastern New Mexico, 1988, Report No. 177, Bureau of Economic Geology: The University of Texas at Austin.
- 7) NOAA, Climatology of the United States No. 81, for 1961-1990.
- 8) Seni, S.J., Sand-Body Geometry and Depositional Systems, Ogallala Formation, Texas, 1980, Report No. 105, Bureau of Economic Geology: The University of Texas at Austin.
- 9) Texas Department of Transportation, Climate Data for Texas, September 1993.
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TABLE 1

CITY OF AMARILLO
MUNICIPAL SOLID WASTE LANDFILL
PERMIT NO. 73

GROUNDWATER ELEVATIONS

DATE MEASURED

WELL NO.	ELEVATION (FT)											9/20/94		
	TOC	7/26/94	8/9/94	8/10/94	8/15/94	8/17/94	8/19/94	8/23/94	8/24/94	8/24/94	8/24/94			
MW-1	3816.82	NA	NA	3599.07	3594.42	3592.22	NA	NA	NA	NA	NA	NA	NA	3590.24
MW-2	3809.54	3593.14	3593.04	NA	NA	3592.94	NA	NA	NA	NA	NA	NA	NA	3590.44
MW-3	3792.72	NA	3591.12	NA	NA	3592.17	NA	NA	NA	NA	NA	NA	NA	NA
MW-4	3750.26	NA	NA	NA	NA	3597.87	NA	NA	NA	NA	NA	NA	NA	3596.26
MW-5	3737.39	NA	NA	NA	NA	NA	NA	NA	NA	3617.34	3617.09	3617.09	3617.09	3613.78
MW-6	3750.40	NA	NA	NA	NA	NA	NA	NA	3603.90	NA	NA	NA	3603.88	3601.55
P-1	3812.31	NA	3598.96	NA	NA	3596.98	NA	NA	NA	NA	NA	NA	NA	3595.12
P-2	3797.95	NA	3597.49	NA	NA	3597.49	NA	NA	NA	3597.49	NA	NA	NA	3594.75
P-3	3746.34	NA	3545.88	NA	NA	3545.88	NA	NA	NA	3545.88	NA	NA	NA	3599.57

TABLE 1 cont.

CITY OF AMARILLO
MUNICIPAL SOLID WASTE LANDFILL
PERMIT NO. 73

GROUNDWATER ELEVATIONS

DATE MEASURED

WELL NO.	ELEVATION (FT) TOC	9/28/94	10/5/94	10/12/94	10/19/94	10/26/94	10/31/94	11/9/94	11/16/94	11/23/94
MW-1	3816.82	3568.65	3590.32	3590.27	3590.32	3590.27	3590.22	3590.17	3590.22	3590.22
MW-2	3809.54	3587.34	3590.44	3590.44	3590.44	3590.44	3590.39	3590.39	3590.39	3590.34
MW-3	3792.72	3588.98	3590.12	3590.07	3590.12	3590.12	3589.97	3589.87	3590.02	3590.02
MW-4	3750.26	3595.69	3598.51	3598.56	3596.51	3596.66	3596.66	3596.76	3596.81	3596.91
MW-5	3737.39	3613.03	3613.84	3613.89	3613.84	3613.84	3613.99	3614.09	3614.24	3614.34
MW-6	3750.40	3601.06	3601.55	3601.55	3601.55	3601.50	3601.50	3601.50	3601.45	3601.45
P-1	3812.31	3594.51	3595.20	3595.01	3595.11	3595.16	3594.98	3595.01	3595.06	3595.11
P-2	3797.95	3594.11	3594.80	3594.75	3594.75	3594.80	3594.65	3594.95	3594.75	3594.75
P-3	3748.34	3599.24	3597.59	3597.54	3599.59	3599.54	3599.44	3599.44	3599.44	3599.49

TABLE 1 cont.

CITY OF AMARILLO
MUNICIPAL SOLID WASTE LANDFILL
PERMIT NO. 73

GROUNDWATER ELEVATIONS

DATE MEASURED

WELL NO.	ELEVATION (FT)		DATE MEASURED
	TOC		
MW-1	3816.82	3589.92	12/7/94
MW-2	3809.54	3590.34	3590.12
MW-3	3782.72	3590.02	3590.24
MW-4	3750.26	3597.06	3590.02
MW-5	3737.39	3614.39	3597.06
MW-6	3750.40	3601.45	3614.39
P-1	3812.31	3595.01	3601.40
P-2	3797.95	3594.75	3594.65
P-3	3746.34	3599.44	3594.65
			3599.39

TABLE 2

SUMMARY OF SLUG TESTING RESULTS

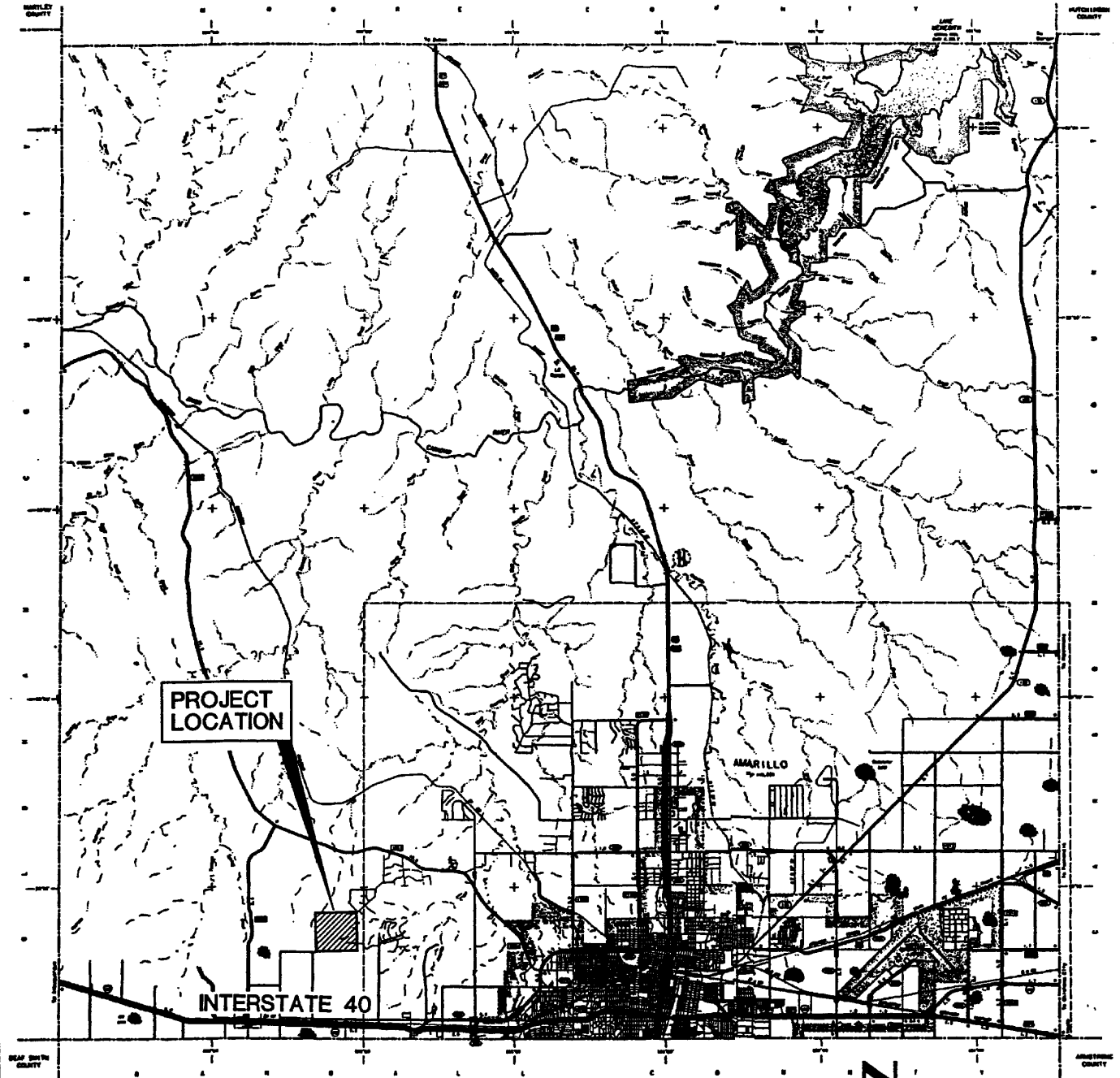
<u>Well No.</u>	<u>Bouwer and Rice</u>	<u>Hvorslev Method G</u>	<u>Equilibrium Well Equation</u>
MW-2	6.58×10^{-4}	1.32×10^{-3}	3.34×10^{-3}
MW-3	7.24×10^{-4}	1.80×10^{-4}	4.40×10^{-4}
MW-6	1.35×10^{-3}	1.33×10^{-3}	3.30×10^{-3}
P-1	1.47×10^{-3}	3.77×10^{-2}	-----
P-2	1.25×10^{-3}	1.03×10^{-3}	-----
P-3	1.09×10^{-3}	4.28×10^{-3}	3.77×10^{-3}

AVERAGE OF THE BOUWER AND RICE AND HVORSLEV METHODS

MW-2	9.89×10^{-4}
MW-3	4.52×10^{-4}
MW-6	1.34×10^{-3}
P-1	1.96×10^{-2}
P-2	1.14×10^{-3}
P-3	2.69×10^{-3}

All values reported in centimeters per second (cm/sec)

FILENAME: E:\AMARILLO\DWG\AMAVMAP



MAP SOURCE:
GENERAL HIGHWAY MAP,
POTTER COUNTY, TEXAS
1989



HDR

HDR Engineering, Inc.

CITY OF AMARILLO, TEXAS
MUNICIPAL LANDFILL

VICINITY MAP

Date	11/94
Figure	1

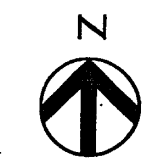
SITE MAP

Project Manager
T. HOTCHKISS
Designed
HDR
Drafted
HDR
Checked

Project Number
06625-015-037
Date
NOVEMBER, 1994
Issue




Figure Number

2



0 300 600
SCALE IN FEET

LEGEND

-  EXISTING WATER WELLS
-  MONITOR WELL LOCATION
-  PERMIT BOUNDARY

NOTES

1. TOPOGRAPHIC MAP WAS COMPILED BY PHOTOGRAMMETRIC METHODS BY UNITED AERIAL MAPPING, SAN ANTONIO, TEXAS FROM AERIAL PHOTOGRAPHY DATED MARCH 9, 1993. VERTICAL DATUM BASED ON MEAN SEA LEVEL. MAPPING GROUND CONTROL PROVIDED BY THE CITY OF AMARILLO, COMPLETED IN ACCORDANCE WITH NATIONAL MAP ACCURACY STANDARDS.
2. PROPERTY BOUNDARY INFORMATION BASED ON BOUNDARY SURVEY DATA PROVIDED BY THE CITY OF AMARILLO.





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SCALE IN FEET



CITY OF AMARILLO
MUNICIPAL LANDFILL
PERMIT MODIFICATIONS

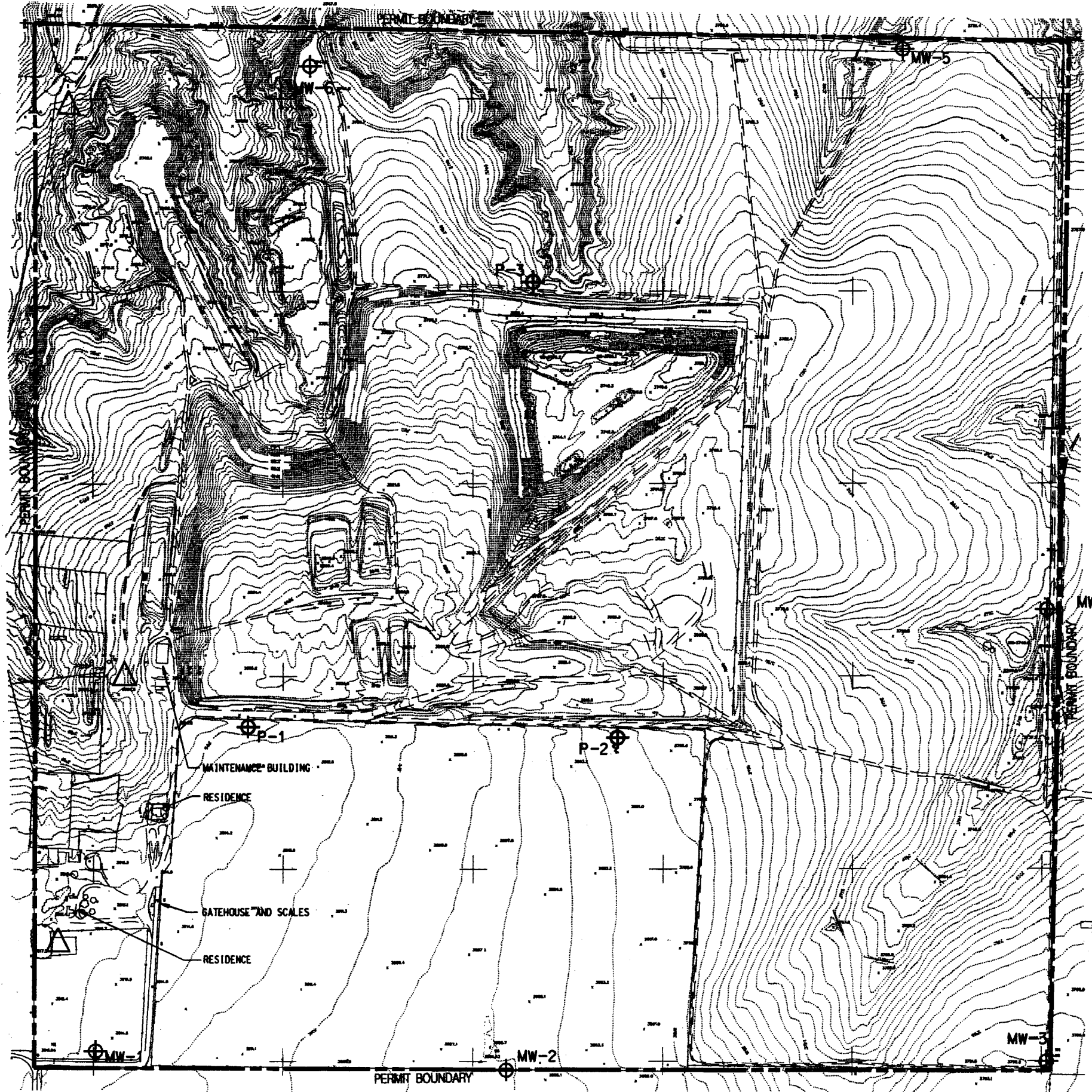
SITE MAP

Project Manager
T. HOTCHKISS
Designed
HDR
Drafted
HDR
Checked

Project Number
06625-015-037
Date
DECEMBER, 1994
NOVEMBER, 1994




USE FOR CALIBRATION

Utility Number
Figure Number



5500
5000
4500
4000
3500
3000
2500
2000
1500
1000

LEGEND

-  EXISTING WATER WELLS
-  MONITOR WELL LOCATION
-  PERMIT BOUNDARY

NOTES











1. TOPOGRAPHIC MAP WAS COMPILED BY PHOTOGRAMMETRIC METHODS BY UNITED AERIAL MAPPING, SAN ANTONIO, TEXAS FROM AERIAL PHOTOGRAPHY DATED MARCH 9, 1993. VERTICAL DATUM BASED ON MEAN SEA LEVEL. MAPPING GROUND CONTROL PROVIDED BY THE CITY OF AMARILLO. COMPLETED IN ACCORDANCE WITH NATIONAL MAP ACCURACY STANDARDS.
2. PROPERTY BOUNDARY INFORMATION BASED ON BOUNDARY SURVEY DATA PROVIDED BY THE CITY OF AMARILLO.

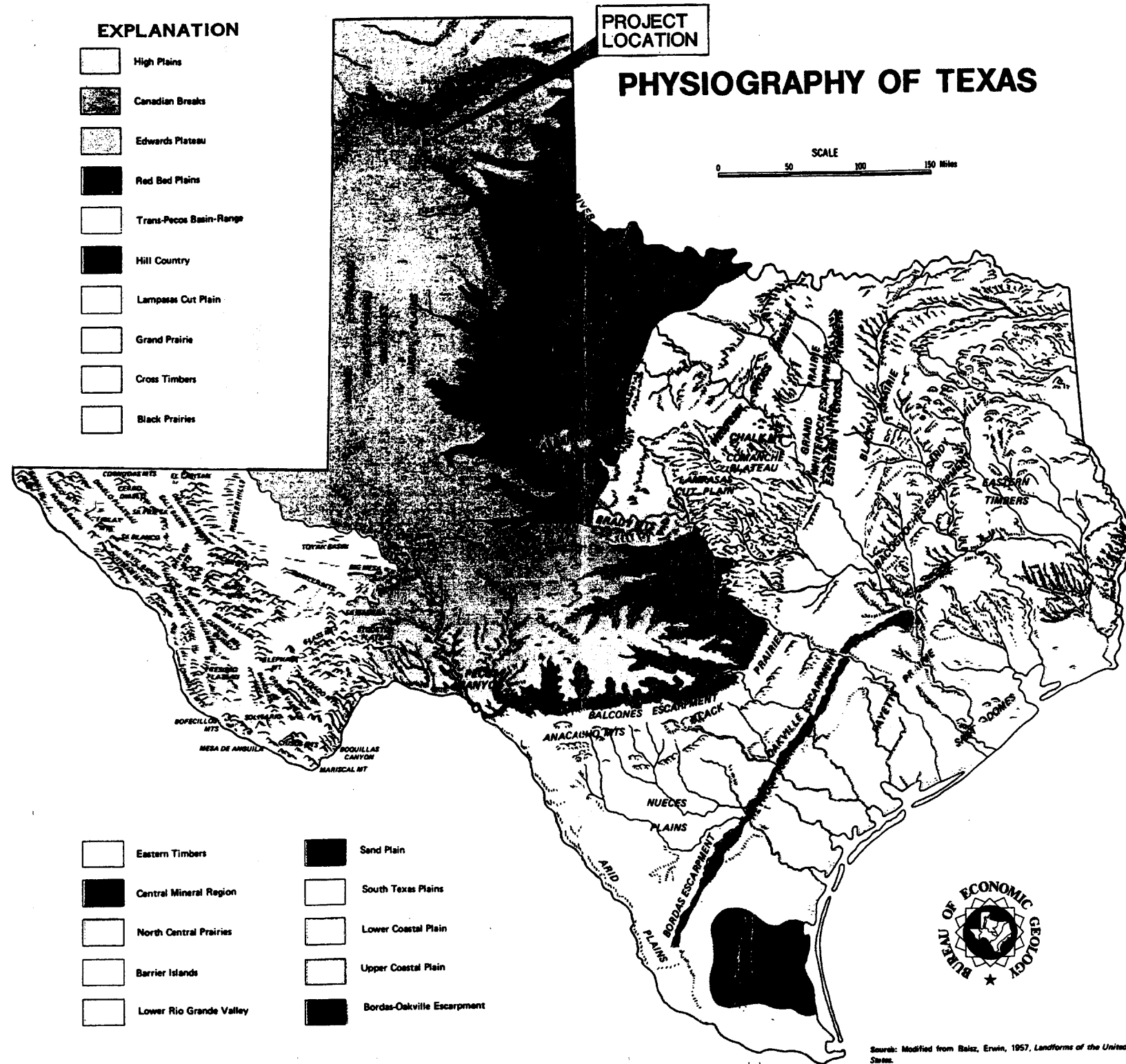
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MAP**











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Designed
HDR
Drafted
HDR
Checked

Project Number
06625-015-037
Date
NOVEMBER, 1994
Issue

EXPLANATION

-  High Plains
-  Canadian Breaks
-  Edwards Plateau
-  Red Bed Plains
-  Trans-Pecos Basin-Range
-  Hill Country
-  Lampasas Cut Plain
-  Grand Prairie
-  Cross Timbers
-  Black Prairies



-  Eastern Timbers
-  Central Mineral Region
-  North Central Prairies
-  Barrier Islands
-  Lower Rio Grande Valley
-  Sand Plain
-  South Texas Plains
-  Lower Coastal Plain
-  Upper Coastal Plain
-  Borden-Oakville Escarpment



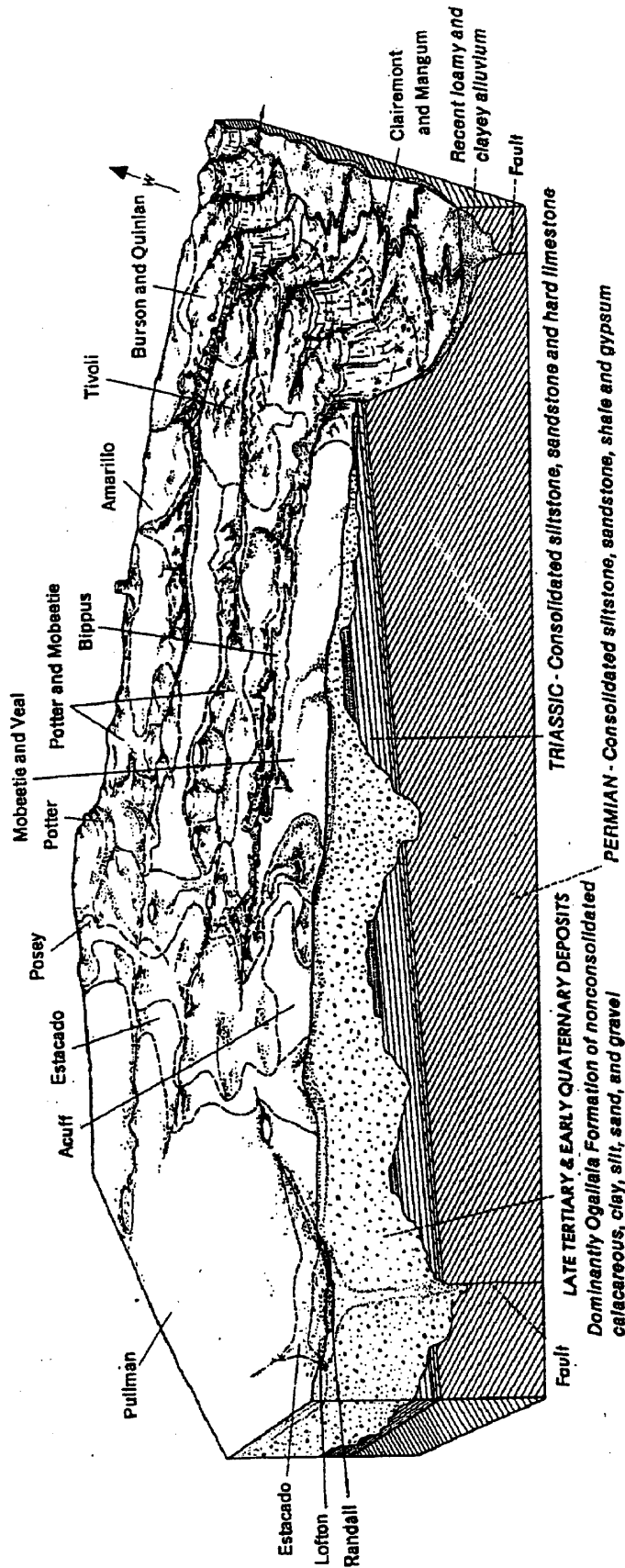
Source: Modified from Raisz, Erwin, 1957, Landforms of the United States.



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CITY OF AMARILLO, TEXAS
MUNICIPAL LANDFILL

DISTRIBUTION OF SOIL TYPES



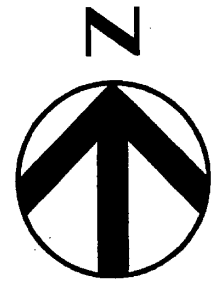
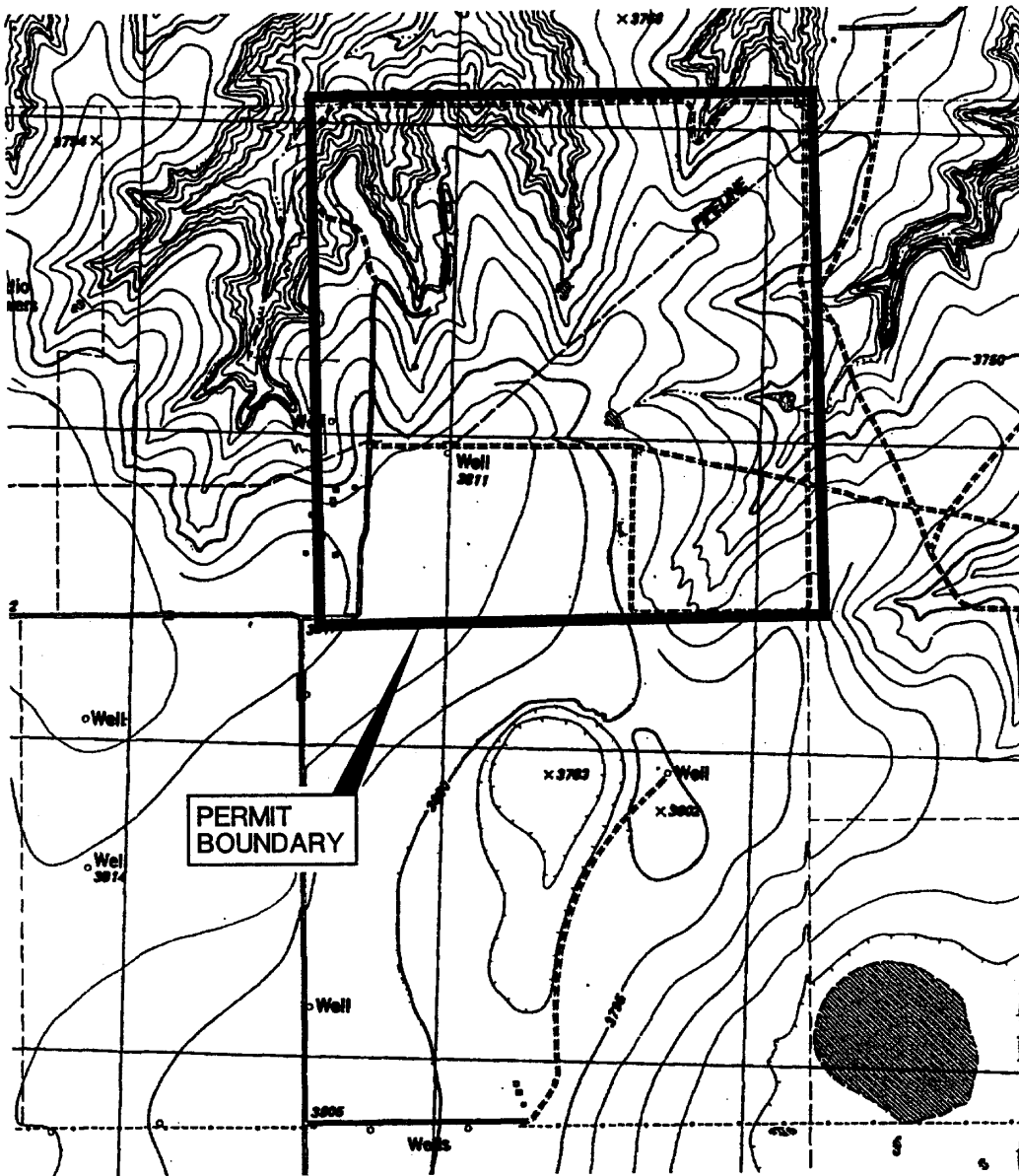
Pattern of soils in Potter County.

MAP SOURCE:
UNITED STATES DEPARTMENT OF AGRICULTURE
SOIL CONSERVATION SERVICE
SOIL SURVEY OF POTTER COUNTY, FEBRUARY, 1980

Date
11/94

Figure
4

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MAP SOURCE:
USGS 7.5 MINUTE QUADRANGLE, BUSHLAND, TEXAS, 1984



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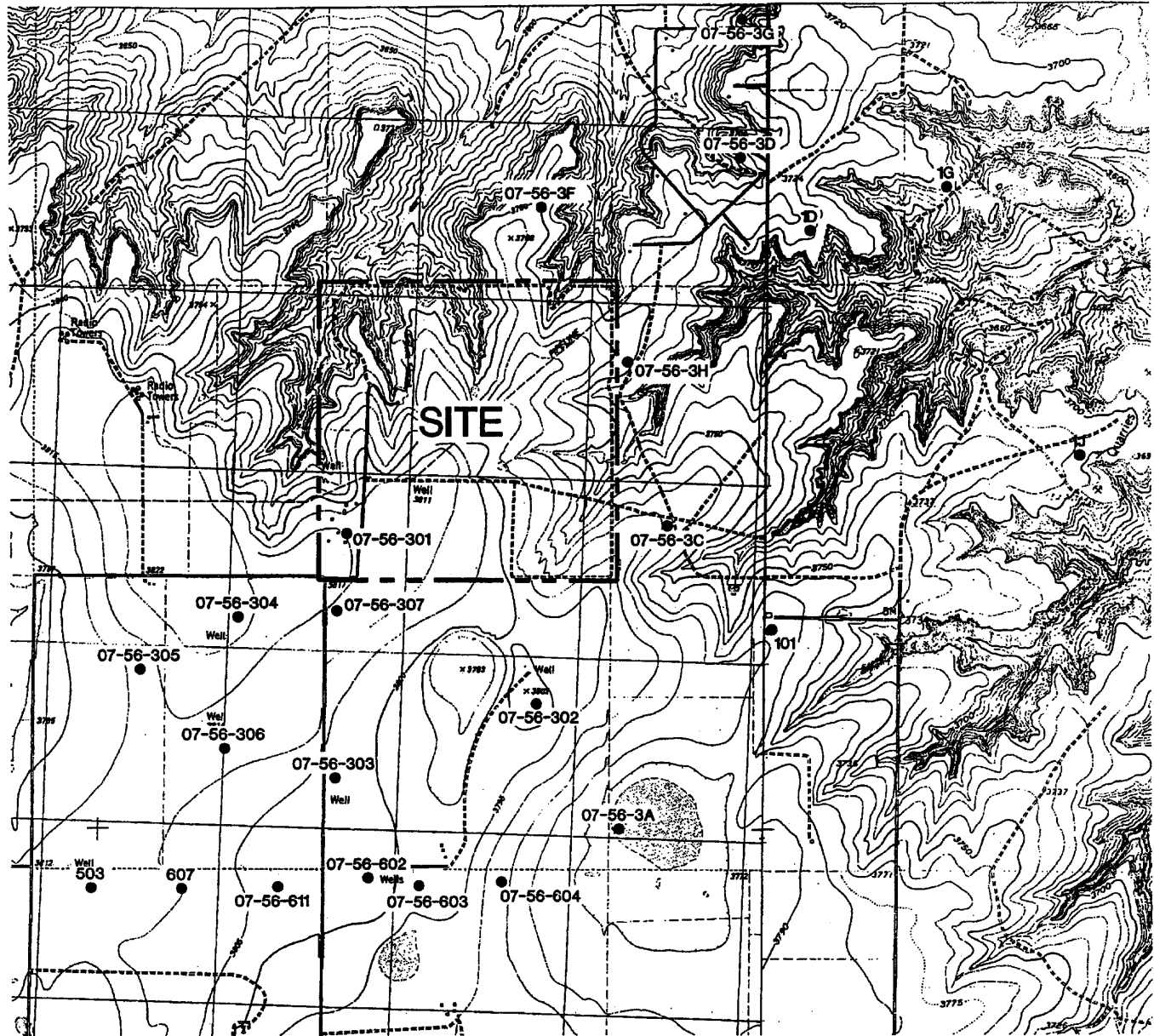
CITY OF AMARILLO, TEXAS
MUNICIPAL LANDFILL

TOPOGRAPHIC MAP

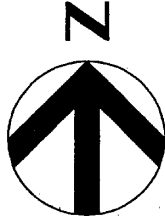
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11/94

Figure
5

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MAP SOURCES:
USGS 7.5 MINUTE QUADRANGLES
BUSHLAND, TEXAS, 1984
AMARILLO WEST, TEXAS, 1960
(PHOTOREVISED 1967 AND 1973)



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CITY OF AMARILLO, TEXAS
MUNICIPAL LANDFILL

AREA WELL SURVEY

Date	11/94
Figure	6



HDR Engineering, Inc.

CITY OF AMARILLO, TEXAS
MUNICIPAL LANDFILL

GENERALIZED STRATIGRAPHY

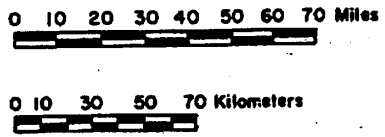
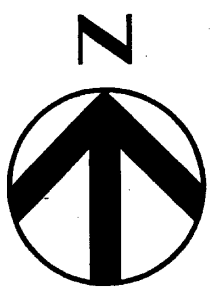
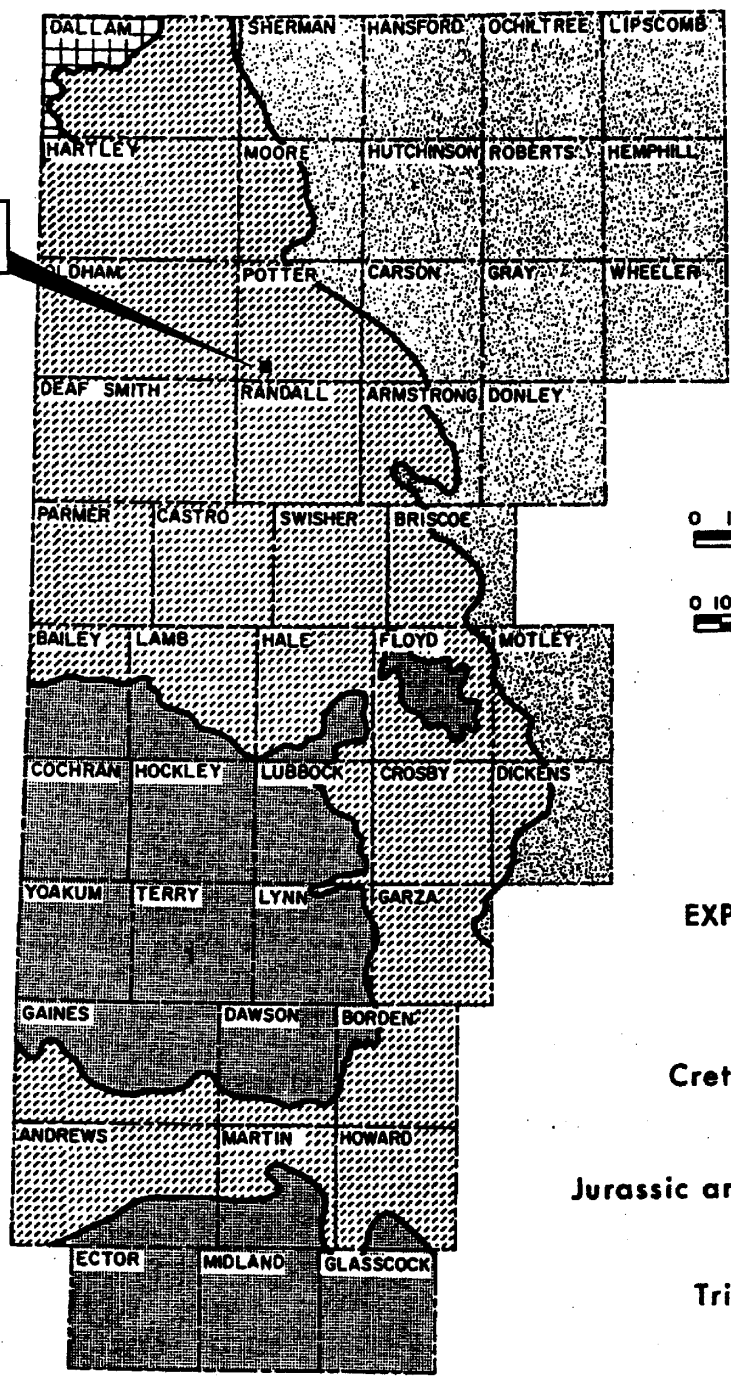
System	Series	Formation or Group	Thickness (feet)	Lithologic Description	Water Supply
Quaternary	Recent		0-15	Chiefly Windblown sand and silt.	Yields no water to wells. Sandy areas form excellent recharge facilities.
	Pleistocene		0-144	Sand, clay, diatomaceous earth, volcanic ash, limestone.	Mostly above water table. Does not yield large supplies.
Tertiary	Pliocene	Ogallala Formation	0-500	Fine to coarse sand and gravel; clay, silt, and caliche.	Yields large supplies of water throughout the Southern High Plains
Cretaceous		Not present in Amarillo area.	Unconformity		
Triassic		Dockum Group Tecovas Formation Santa Rosa sandstone Chinle Formation equivalent	150-1800+	Varicolored shale and sandy shale, gray or brown crossbedded sandstone and conglomerate.	Probably capable of yielding small to moderate supplies of water; most of the water is at least slightly saline.
Permian		Not present in Amarillo area.			

REFERENCE:
SENI, S.J.
SAND-BODY GEOMETRY AND
DEPOSITIONAL SYSTEMS,
OGALLALA FORMATION, TEXAS
REPORT NO. 105, 1980





Date
11/94

Figure
7

FILENAME: E:\AMARILLO\DWG\AMAFIG2



EXPLANATION

-  Cretaceous rocks
-  Jurassic and Cretaceous rocks
-  Triassic rocks
-  Permian rocks

MAP SOURCE:
 EVALUATING THE GROUNDWATER RESOURCES OF THE HIGH PLAINS OF TEXAS,
 REPORT 288, VOL. I, MAY, 1984.
 TEXAS DEPARTMENT OF WATER RESOURCES



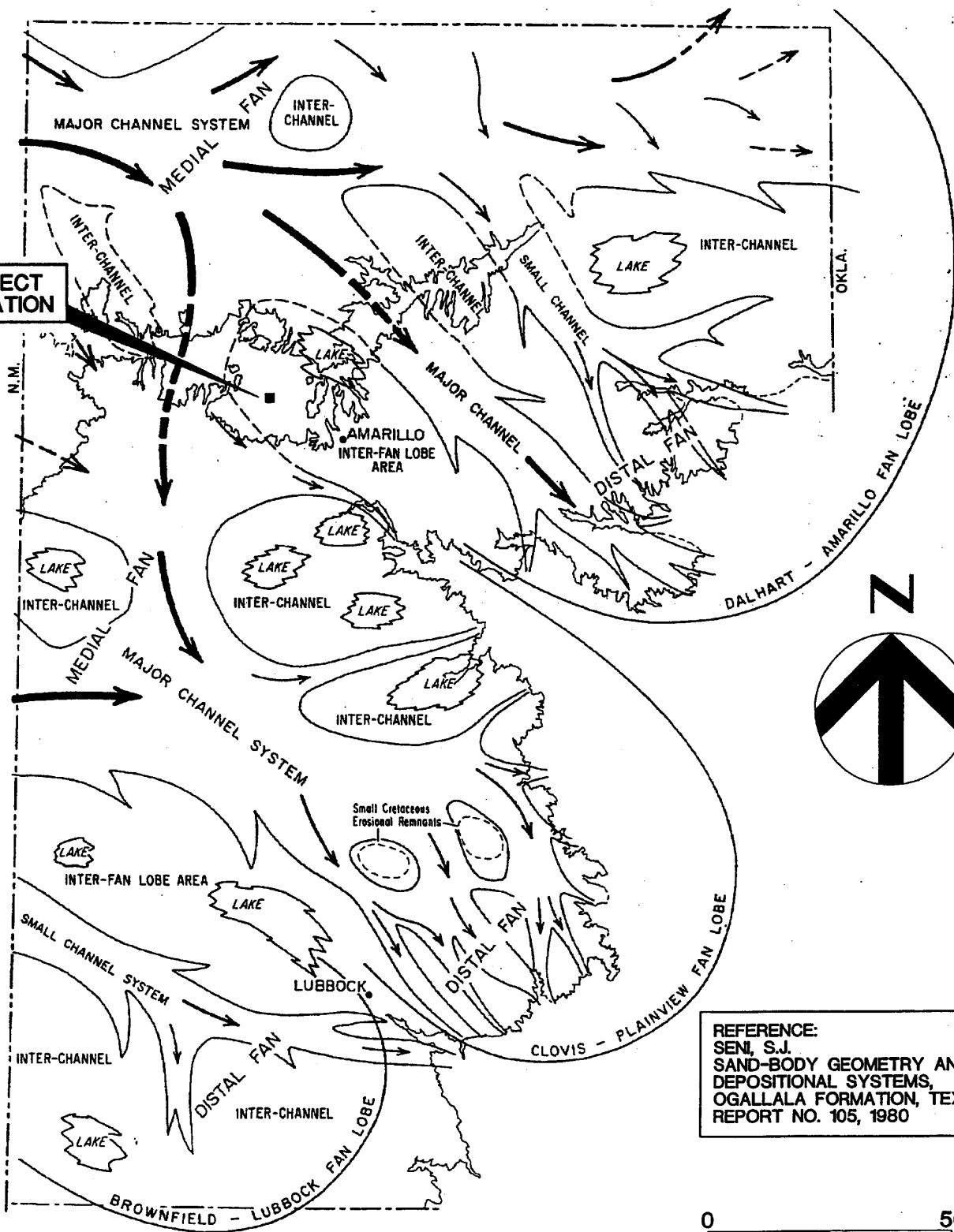
HDR Engineering, Inc.

CITY OF AMARILLO, TEXAS
 MUNICIPAL LANDFILL
 GEOLOGIC UNITS UNDERLYING
 THE OGALLALA FORMATION

Date	11/94
Figure	8

FILENAME: \\AMARILLO\DWG\AMADPFAC

PROJECT LOCATION



REFERENCE:
 SENI, S.J.
 SAND-BODY GEOMETRY AND
 DEPOSITIONAL SYSTEMS,
 OGALLALA FORMATION, TEXAS
 REPORT NO. 105, 1980



HDR Engineering, Inc.

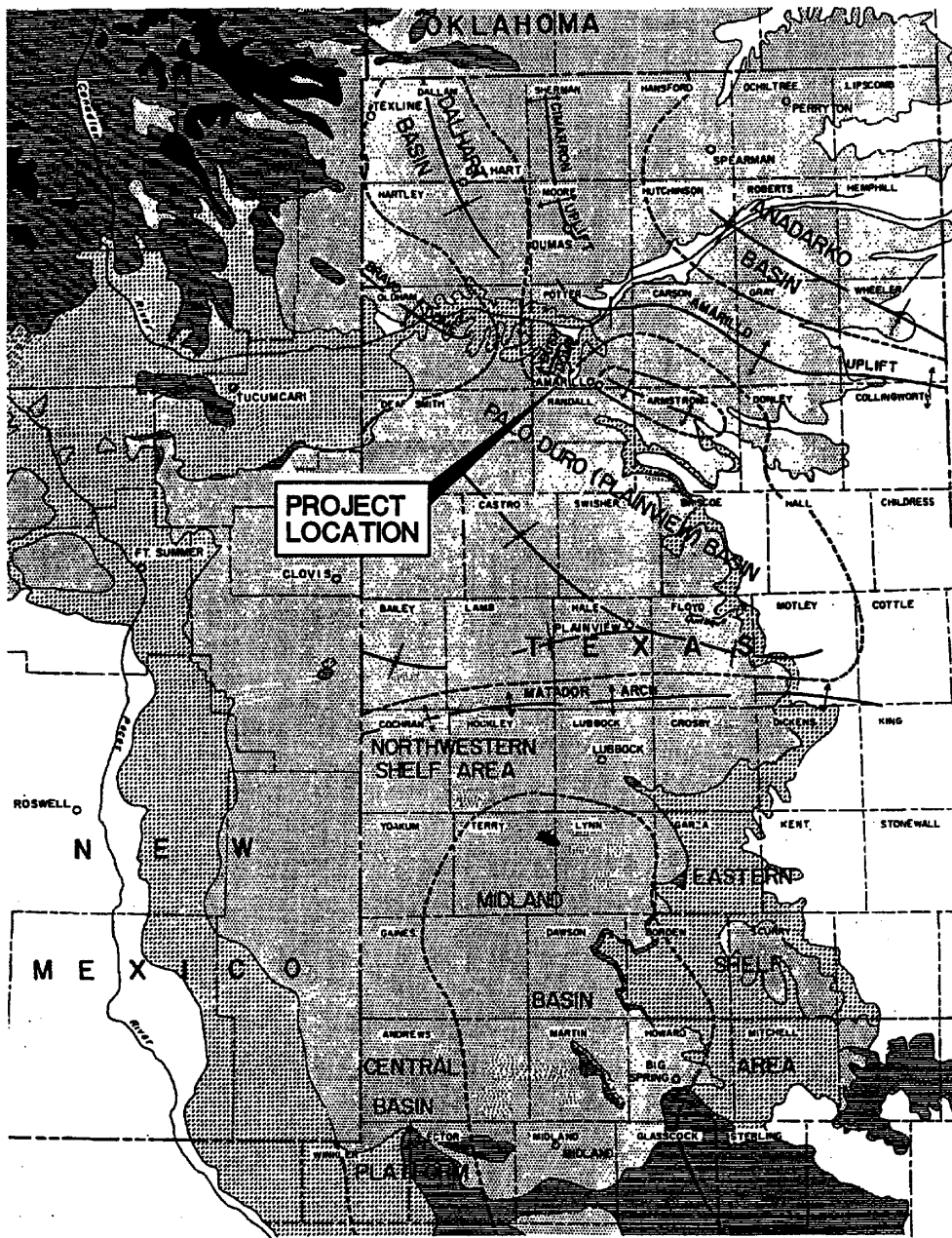
CITY OF AMARILLO, TEXAS
 MUNICIPAL LANDFILL

DEPOSITIONAL FACIES MAP

Date
 11/94

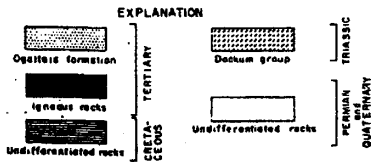
Figure
 9

FILENAME: RWARGSTC



Modified from geologic map of United States, U. S. Geological Survey, 1932

Structural features after Tilton (1956, p. 1963) and King, (1934, p. 704)



REFERENCE: CRONIN, J.G.
 A SUMMARY OF THE OCCURRENCE AND DEVELOPMENT
 OF GROUNDWATER IN THE SOUTHERN HIGH PLAINS
 OF TEXAS, TEXAS BOARD OF WATER ENGINEERS,
 BULLETIN 6107, 1971.



HDR Engineering, Inc.

CITY OF AMARILLO, TEXAS
 MUNICIPAL LANDFILL

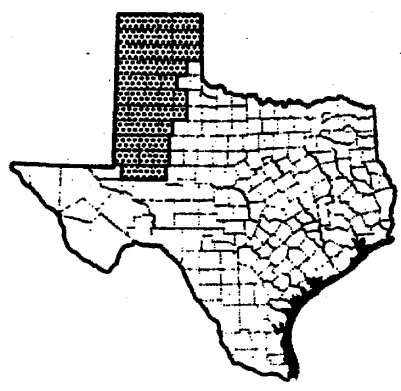
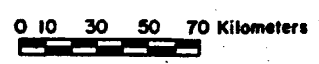
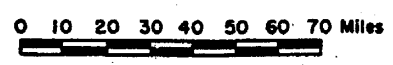
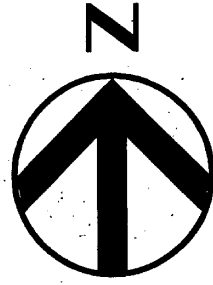
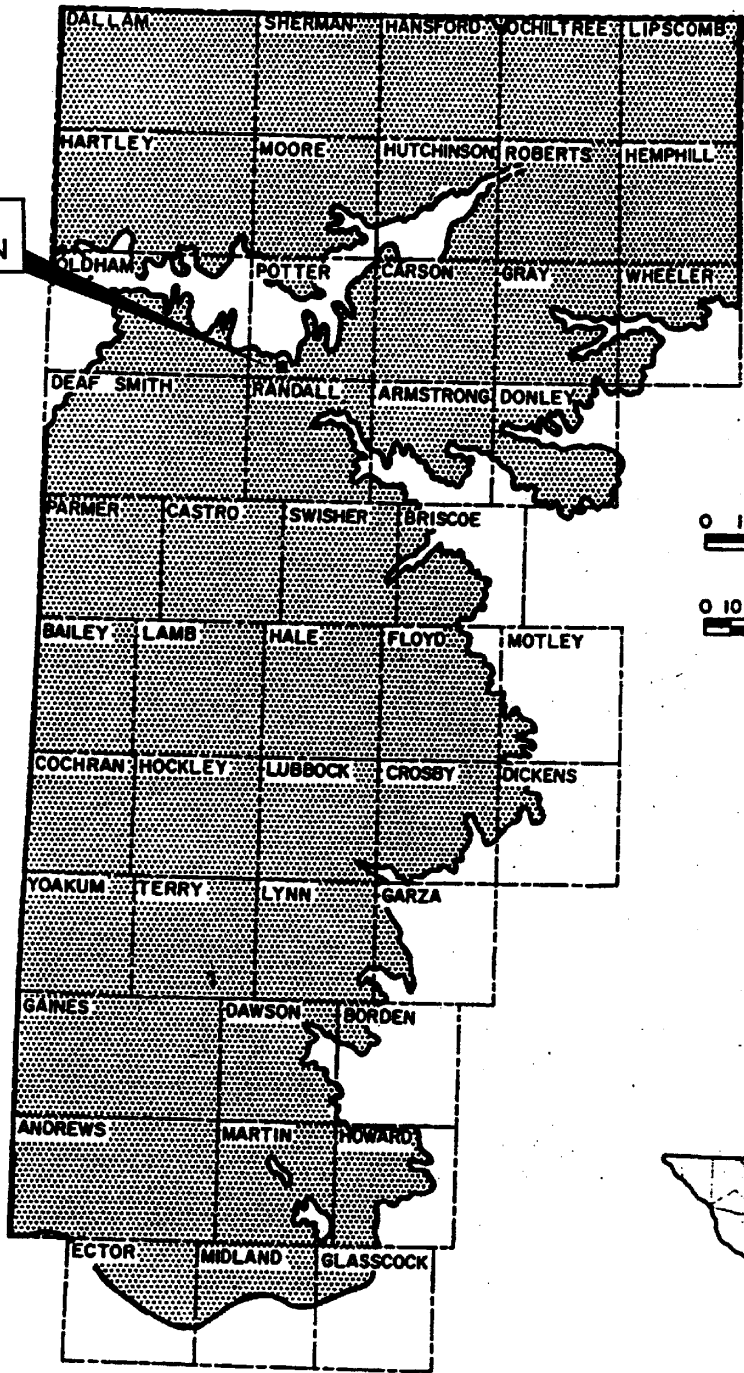
REGIONAL STRUCTURE MAP

Date
 11/94

Figure
 10

FILENAME: \\AMARILLO\DWG\AMAFIG1

PROJECT LOCATION



MAP SOURCE:
 EVALUATING THE GROUNDWATER RESOURCES OF THE HIGH PLAINS OF TEXAS,
 FINAL REPORT, VOL. I, AUGUST, 1982.
 TEXAS DEPARTMENT OF WATER RESOURCES



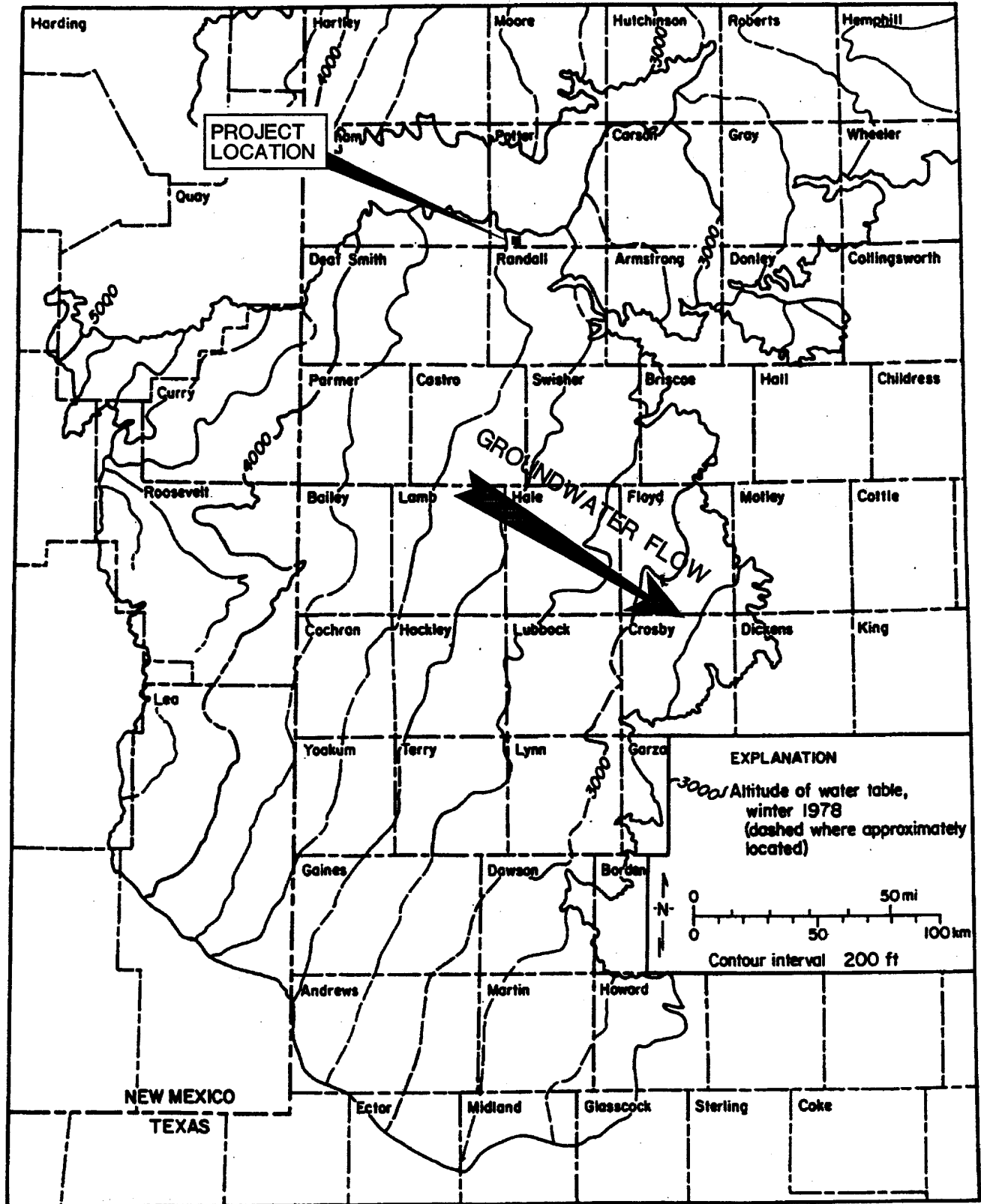
HDR Engineering, Inc.

CITY OF AMARILLO, TEXAS
 MUNICIPAL LANDFILL

HIGH PLAINS AQUIFER

Date	11/94
Figure	11

FILENAME: \\AMARILLO\DWG\OGALLA



MAP SOURCE:
 HYDROGEOLOGY AND HYDROCHEMISTRY OF THE OGALLALA AQUIFER, SOUTHERN HIGH PLAINS, TEXAS PANHANDLE AND EASTERN NEW MEXICO, 1988.
 BUREAU OF ECONOMIC GEOLOGY



CITY OF AMARILLO, TEXAS
 MUNICIPAL LANDFILL

Date
 11/94

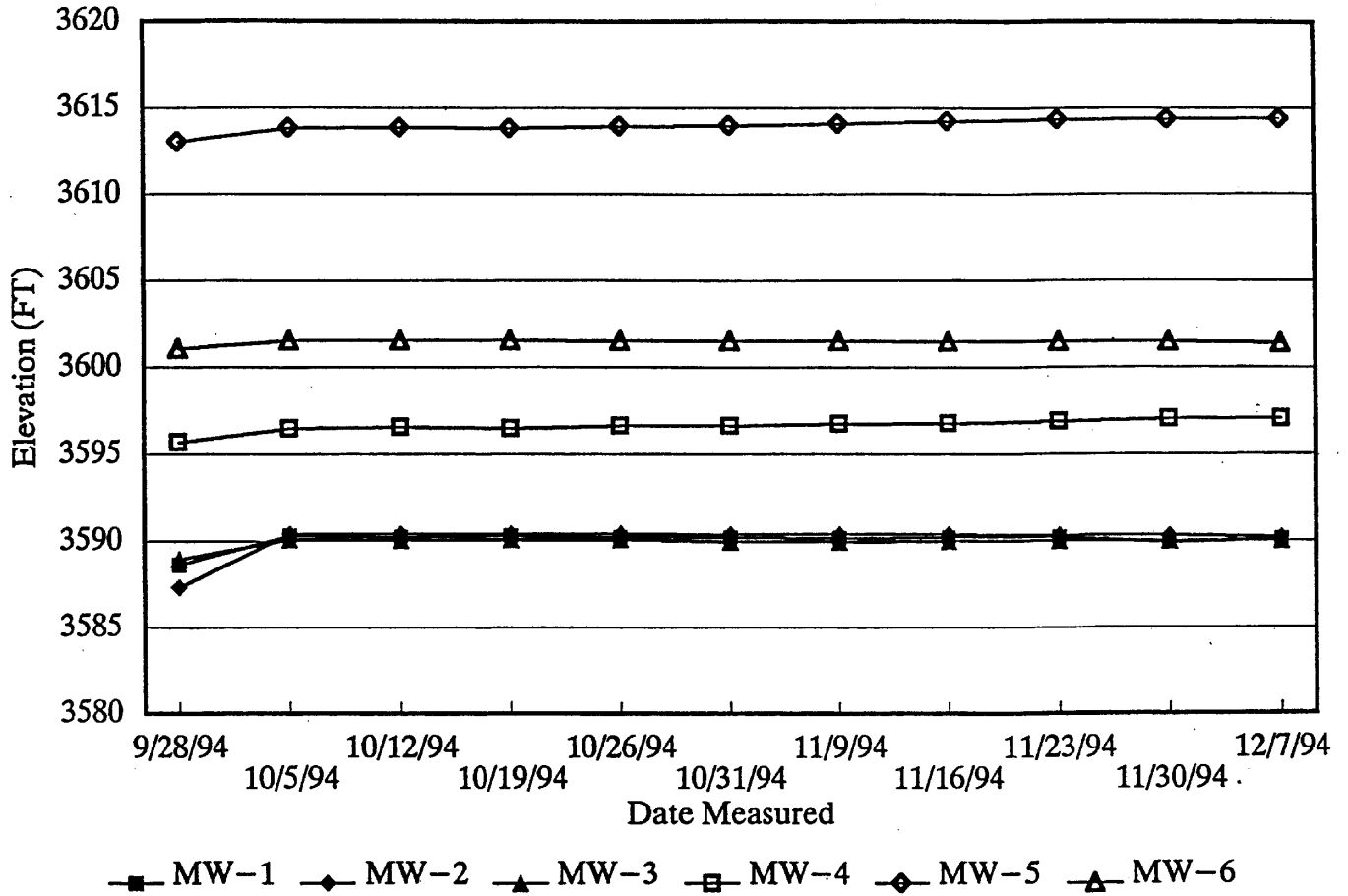
HDR Engineering, Inc.

REGIONAL GROUNDWATER CONTOUR MAP

FIGURE
 12

Groundwater Elevations

Amarillo Landfill



FILENAME: E:\AMARILLO\DWG\AMAHYD1



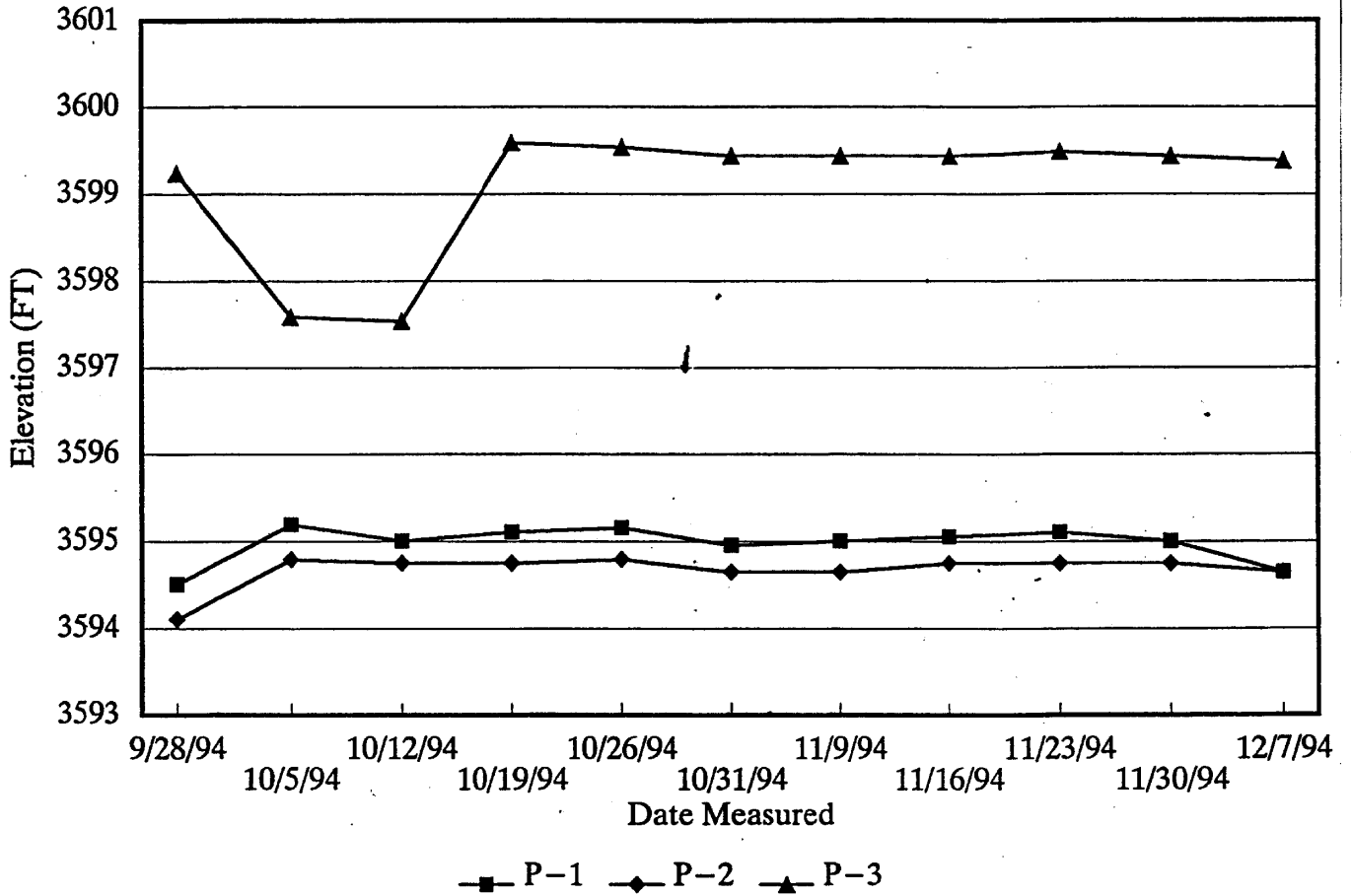
HDR Engineering, Inc.

CITY OF AMARILLO, TEXAS
 MUNICIPAL LANDFILL
 HYDROGRAPHS
 MW-1 THROUGH MW-6

Date	11/94
Figure	13

Groundwater Elevations

Amarillo Landfill



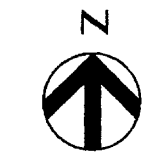
FILENAME: AMAMWHYD



HDR Engineering, Inc.

CITY OF AMARILLO, TEXAS
 MUNICIPAL LANDFILL
 HYDROGRAPHS
 P-1 THROUGH P-3

Date	11/94
Figure	14



0 300 600
SCALE IN FEET

CITY OF AMARILLO
MUNICIPAL LANDFILL
PERMIT MODIFICATIONS

GROUNDWATER
CONTOUR MAP
SEPT. 28, 1994

Project Manager
T. HOTCHKISS
Designed
HDR
Drafted
HDR
Checked

Project Number
06625-015-037
Date
DECEMBER, 1994
NOVEMBER, 1994

Figure Number
15



LEGEND

- EXISTING WATER WELLS
- MONITOR WELL LOCATION
- PERMIT BOUNDARY
- GROUNDWATER ELEVATION CONTOUR IN FEET, MSL
- 3600 GROUNDWATER ELEVATION IN WELL, MEASURED ON SEPTEMBER 28, 1994

NOTES

1. TOPOGRAPHIC MAP WAS COMPILED BY PHOTOGRAMMETRIC METHODS BY UNITED AERIAL MAPPING, SAN ANTONIO, TEXAS FROM AERIAL PHOTOGRAPHY DATED MARCH 9, 1993. VERTICAL DATUM BASED ON MEAN SEA LEVEL. MAPPING GROUND CONTROL PROVIDED BY THE CITY OF AMARILLO, COMPLETED IN ACCORDANCE WITH NATIONAL MAP ACCURACY STANDARDS.
2. PROPERTY BOUNDARY INFORMATION BASED ON BOUNDARY SURVEY DATA PROVIDED BY THE CITY OF AMARILLO.



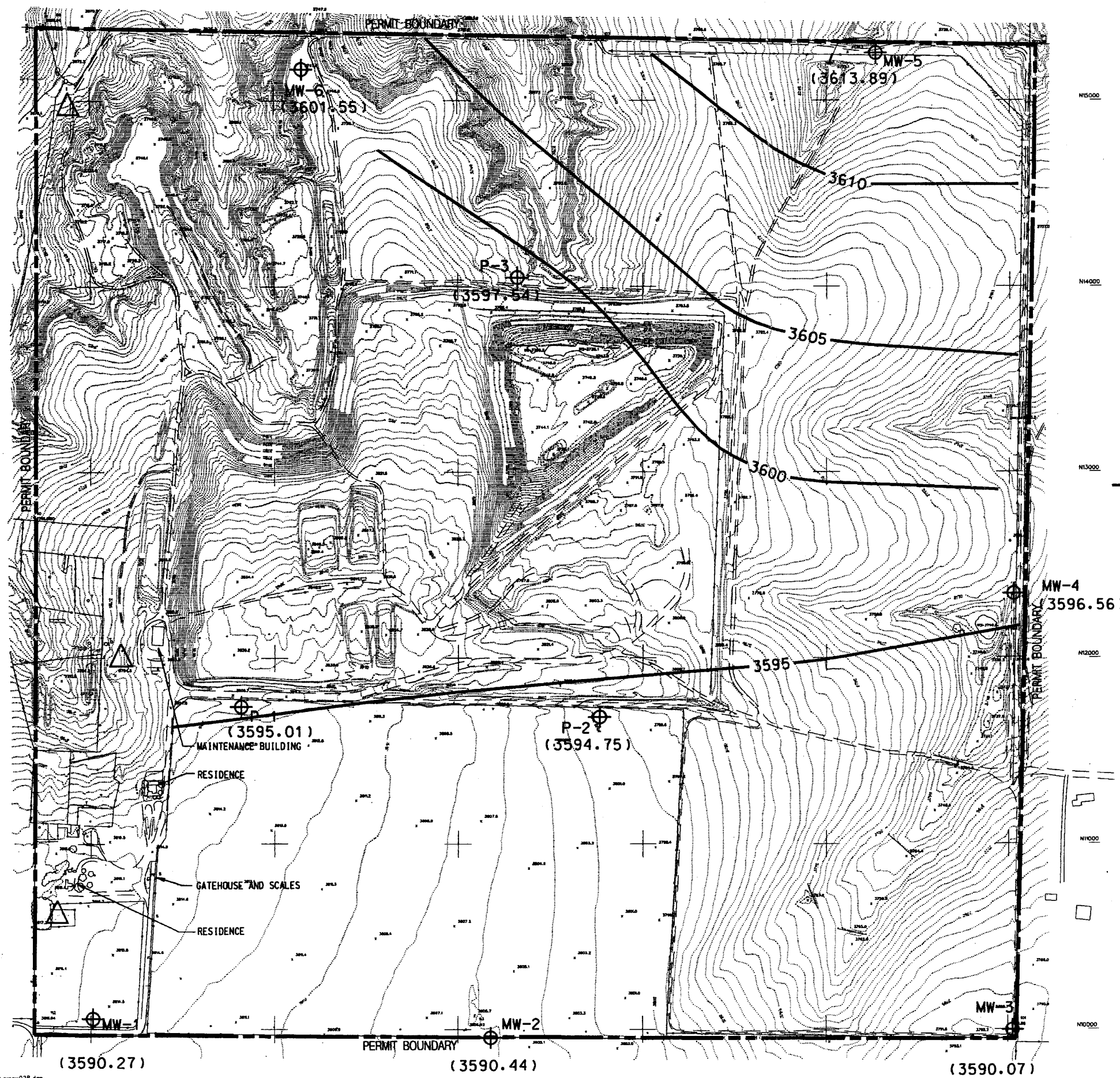
0 300 600
SCALE IN FEET

Project Manager
T. HOTCHKISS
Designed
HDR
Drafted
HDR
Checked

Project Number
06625-015-037
Date
DECEMBER, 1994
NOVEMBER, 1994

NOT FOR CONSTRUCTION

In Drawing Number
Figure Number



LEGEND

- EXISTING WATER WELLS
- MONITOR WELL LOCATION
- PERMIT BOUNDARY
- GROUNDWATER ELEVATION CONTOUR IN FEET, MSL
- (3595.69) GROUNDWATER ELEVATION IN WELL, MEASURED ON OCTOBER 12, 1994

NOTES

1. TOPOGRAPHIC MAP WAS COMPILED BY PHOTOGRAMMETRIC METHODS BY UNITED AERIAL MAPPING, SAN ANTONIO, TEXAS FROM AERIAL PHOTOGRAPHY DATED MARCH 9, 1993. VERTICAL DATUM BASED ON MEAN SEA LEVEL. MAPPING GROUND CONTROL PROVIDED BY THE CITY OF AMARILLO. COMPLETED IN ACCORDANCE WITH NATIONAL MAP ACCURACY STANDARDS.
2. PROPERTY BOUNDARY INFORMATION BASED ON BOUNDARY SURVEY DATA PROVIDED BY THE CITY OF AMARILLO.



0 300 600
SCALE IN FEET

CITY OF AMARILLO
MUNICIPAL LANDFILL
PERMIT MODIFICATIONS

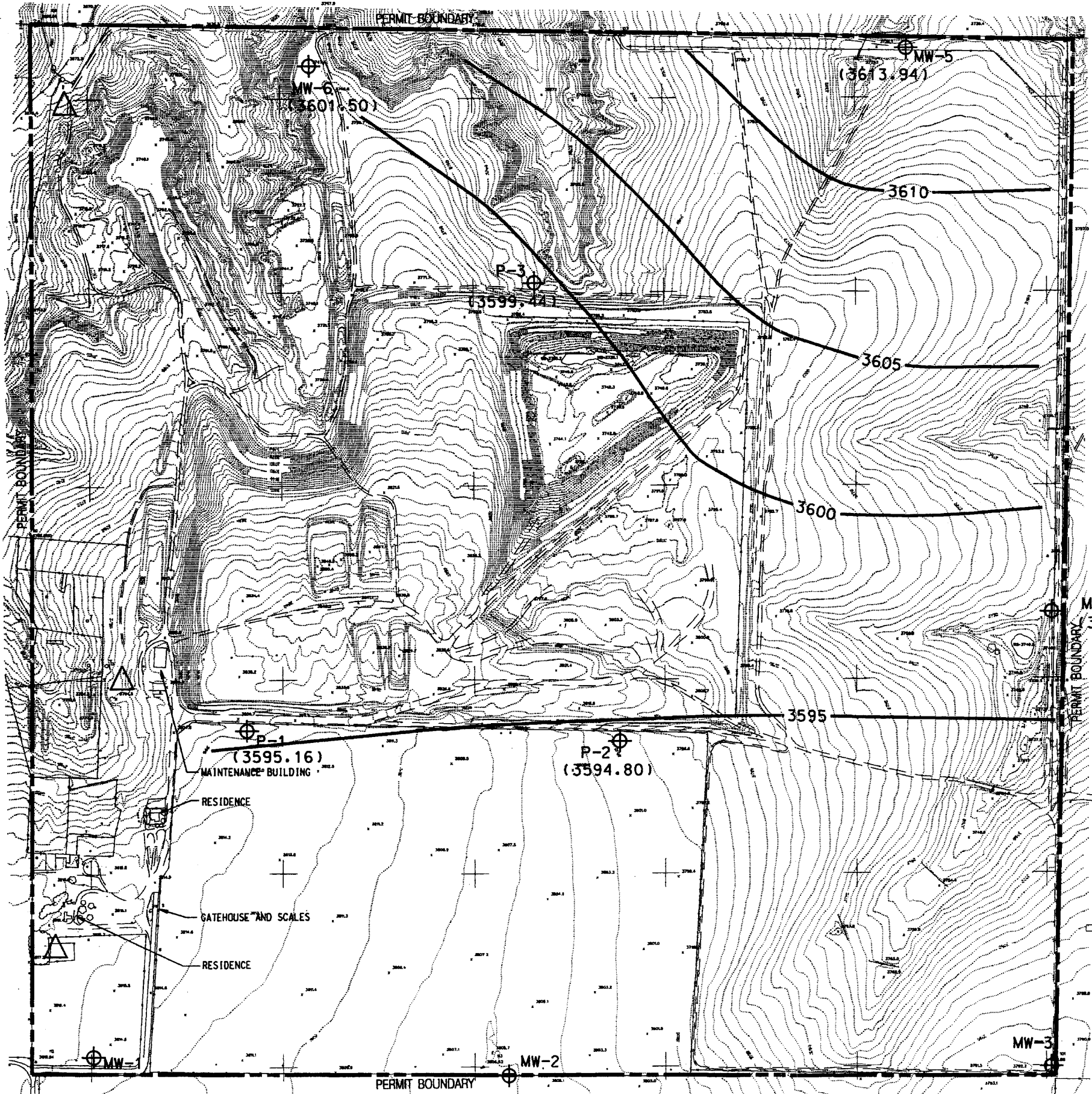
GROUNDWATER
CONTOUR MAP
OCT. 26, 1994

Project Manager
T. HOTCHKISS
Designed
HDR
Drafted
HDR
Checked






Project Number
06625-015-037
Date
DECEMBER, 1994
NOVEMBER, 1994

NOT FOR CONSTRUCTION

Utility Number
Figure Number



LEGEND

-  EXISTING WATER WELLS
-  MONITOR WELL LOCATION
-  PERMIT BOUNDARY
-  3600 GROUNDWATER ELEVATION CONTOUR IN FEET, MSL
-  (3595.69) GROUNDWATER ELEVATION IN WELL, MEASURED ON OCTOBER 26, 1994

NOTES

1. TOPOGRAPHIC MAP WAS COMPILED BY PHOTOGRAMMETRIC METHODS BY UNITED AERIAL MAPPING, SAN ANTONIO, TEXAS FROM AERIAL PHOTOGRAPHY DATED MARCH 9, 1993. VERTICAL DATUM BASED ON MEAN SEA LEVEL. MAPPING GROUND CONTROL PROVIDED BY THE CITY OF AMARILLO, COMPLETED IN ACCORDANCE WITH NATIONAL MAP ACCURACY STANDARDS.
2. PROPERTY BOUNDARY INFORMATION BASED ON BOUNDARY SURVEY DATA PROVIDED BY THE CITY OF AMARILLO.

APPENDIX A

DATA FROM AREA WELL SURVEY

James W. Sansom, Jr.
Consulting Geologist
Certified Professional Geologist
AIPG No. 2406

9506 Queenswood Drive
Austin, Texas 78748
512/282-1598
FAX 512/280-1761

October 29, 1994

Mr. Brad McCardell
HDR Engineering, Inc.
12700 Hillcrest Road
Suite 125
Dallas, Texas 75230-2096

Dear Brad,

In reference to your telephone call on October 26, 1994, about my supplementing the ground water inventory that I did for Troy Hotchkiss west of Amarillo, Texas in May, 1993, the following information is enclosed:

1. I reviewed the locations and data for the wells within the radius that Troy requested in 1993. I did not find pump test data for any of the wells. Two of the wells were found to have water quality analyses: 06-49-101 and 07-56-307

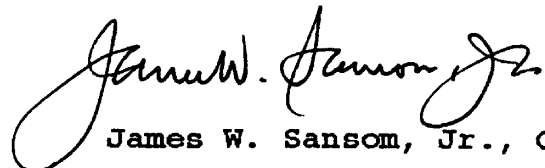
2. Logs and maps are provided for well numbers 07-56-3E and 07-56-3J since you are interested in the wells on site. Please note that two logs for well number 3J are included.

3. Three new wells were found; 07-56-3, 06-49-1, and a unnumbered well drilled in 1993.

The two 3J well logs look like duplicates because they are almost exactly the same in all aspects (TD, water level, etc.). Upon close examination the wells were completed two days apart. As to the three new wells, well data is continuously added to the files, and often it is a very slow process from the time the log is received until it is placed in the Central Records File.

I hope this will be of some benefit to you.

Sincerely,



James W. Sansom, Jr., CPG

**Texas Water Development Board
Well Schedule**

State Well No. 07 56307 Previous Well No. County Other 375
 River Basin Red River 02 Zone 1 Region Lat. 351327 Long. 1022137 Source of Coord.
 Owner's Well No. Location NW 14, NW 1.4, Section 127, Block B-9, Survey B.S.F.F.

Owner CAROLINE B. EMEMY Driller BUD GIBBONS

Address P.O. Box 1230, Amarillo TX Tenant/Oper. VICTOR PLUNK RT 1, Box 544 Amarillo

Date Drilled 03 08 1974 Depth 295 Source of Depth Datum D Altitude 3815 Source of Alt. Datum A
 Aquifer OGALLALA 1210644 Well Type U User

Well Construction Method Rotary Casing Material Steel

Completion Perforated Screen Material Steel

Lift Data Pump Mfr. NONE Type No. Stages

Bowls Diam. in. Setting ft. Column Diam. in.

Motor Mfr. NONE Fuel or Power Horsepower

Yield Flow GPM Pump GPM Meas., Rept., Est. Date

Performance Test Date Length of Test Production GPM

Static Level ft. Pumping Level ft. Drawdown ft. Sp.Cap. GPM/ft.

Quality (Remarks)

Water Use Primary UNUSED Secondary Tertiary

Other Data Available Water Level Water Quality Logs Other Data

Date 01 06 1993 Meas. 226.59 Below LSD.

Water Levels Date Meas.

Date Meas.

Recorded By DAN SEALE Date Record Collected or Updated 07 25 1994 (20 max) Reporting Agency

1	REMARKS	1	ID	PLATE	INTACT	ON	WEST	SIDE	OF	
2		2	STAND	PIPE	APPROX.	3	FT	ABOVE	G.L.	
3		3								
4		4								
5		5	NO	HOLE	IN	TOP	OF	PUMP	BASE	COVER
6		6	CASING	IS	1.0	FT				

	Casing or Blank Pipe (C)		
	Diam. (in.)	Setting (feet) From	To
1	C 14	0	19
2	S 14	197	29
3			
4			
5			
6			
7			
8			
9			
10			
11			
12			
13			
14			
15			
16			

Aquifer OGM
Well No. 0756

NTY Potter

NO. 07-56-307

LOCATION SKETCH

BY DAN SEALE

DATE 9-13-76

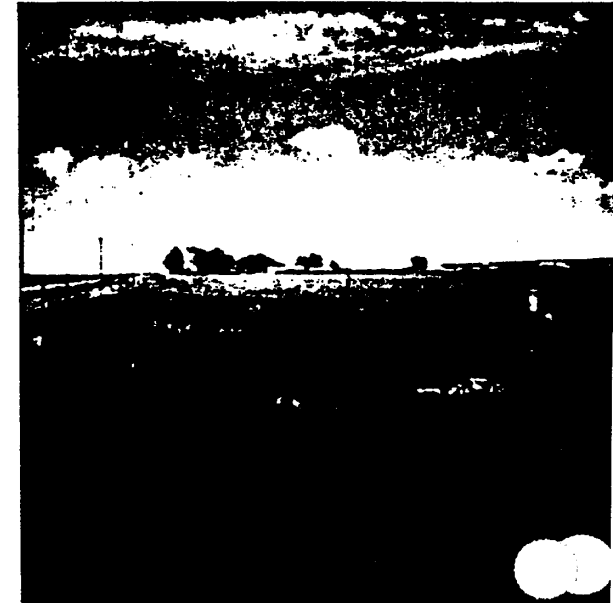
PHOTOGRAPHS

BY DAN SEALE

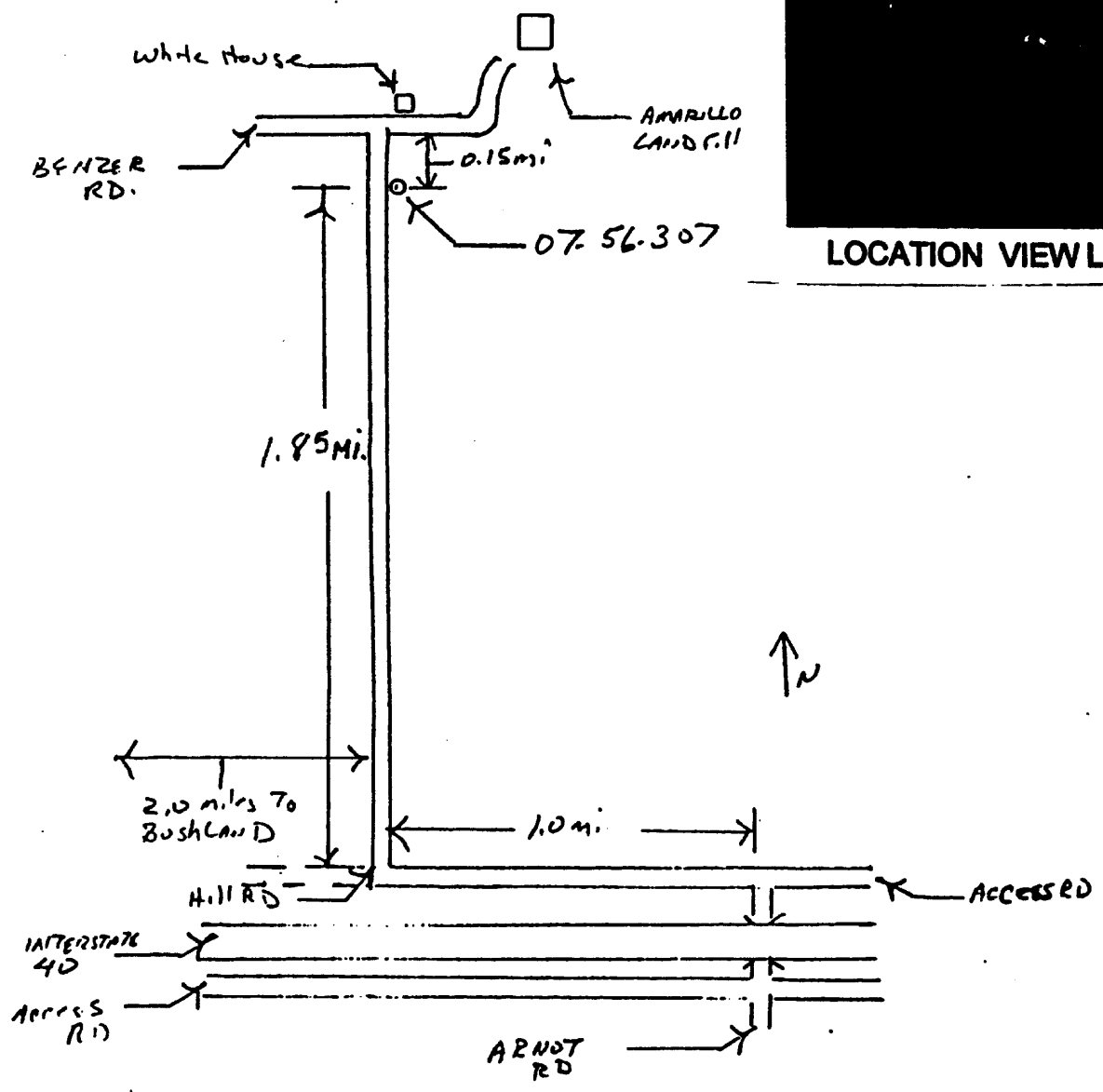
DATE 7-21-94



MP-ID VIEW LOOKING E.



LOCATION VIEW LOOKING N.



NO. 07-56-307

Send original copy by certified mail to the Texas Water Development Board P. O. Box 13087 Austin, Texas 78711

State of Texas
WATER WELL REPORT

For TWDB use only
Well No. 17-36
Located on map
Received: 7-7

1) OWNER: Person having well drilled Caroline B. Dmney Address Box 1230 Amarillo Texas
(Name) (Street or RFD) (City) (State)
Landowner Same Address Same
(Name) (Street or RFD) (City) (State)

2) LOCATION OF WELL: County Potter 3/4-N & 2-E miles in NE direction from Eushland, Texas
(Town)

Locate by sketch map showing landmarks, roads, creeks, highway number, etc.*

OR Give legal location with distances and directions from adjacent sections or survey lines.

Labor _____ League _____
Block 9 Survey SE & F

Abstract No. _____
(WATER WELL) of Section 127

(Use reverse side if necessary)

North
↑

3) TYPE OF WORK (Check):
New Well Deepening _____
Reconditioning _____ Plugging _____
4) PROPOSED USE (Check):
Domestic _____ Industrial _____ Municipal _____
Irrigation Test Well _____ Other _____
5) TYPE OF WELL (Check):
Rotary Driven _____ Dug _____
Cable _____ Jetted _____ Bored _____

6) WELL LOG: Diameter of hole 10" in. Depth drilled 295' ft. Depth of completed well _____ ft. Date drilled 3-8-
All measurements made from _____ ft. above ground level.

From (ft.)	To (ft.)	Description and color of formation material
00	4	Top Soil
4	82	Caliche Clay
82	153	Clay Sand Fock & Sand
153	259	Clay and Layers Sand
259	279	Fine sand
279	289	Course Sand
289	295	Blue Clay and Red Bed

9) CASING: Type: Old _____ New Steel Plastic _____ Other _____
Cemented from _____ ft. to _____

Diameter (inches) _____ Setting From (ft.) _____ To (ft.) _____ Gap _____
1 1/2" OD. 0 295 .188"
(197' - 295' - 4 row Perforation)

10) SCREENS: Type _____
Perforated _____ Slotted _____

Diameter (inches) _____ Setting From (ft.) _____ To (ft.) _____ Size _____

(Use reverse side if necessary)

7) COMPLETION (Check):
Straight well Gravel packed _____ Other _____
Under reamed _____ Open Hole _____

8) WATER LEVEL: Static level _____ ft. below land surface Date _____
Artesian pressure _____ lbs. per square inch Date _____
Depth to pump bowls, cylinder, jet, etc., _____ ft. below land surface.

11) WELL TESTS: Was a pump test made? Yes _____ No If yes, by whom _____
Yield: _____ gpm with _____ ft. drawdown after _____
Bailer test _____ gpm with _____ ft. drawdown after _____
Artesian flow _____ gpm
Temperature of water _____

12) WATER QUALITY: Was a chemical analysis made? Yes _____ No
Did any strata contain undesirable water? Yes _____
Type of water? _____ depth of strata _____

I hereby certify that this well was drilled by me (or under my supervision) and that each and all of the statements herein are true to the best of my knowledge and belief.

NAME Bud Gibbons Water Well Drillers Registration No. 299
(Type or Print)
ADDRESS 1004 E. 5th, P.O. Box 1972 Plainview Texas
(Street or RFD) (City) (State)
(Signed) Bud Gibbons Bud Gibbons Drilling Contractor
(Water Well Driller) (Company Name)

Please attach electric log, chemical analysis, and other pertinent information, if available. UU07-56-30

*Additional instructions on reverse side.

TEXAS WATER DEVELOPMENT BOARD

WELL SCHEDULE

Aquifer Ogallala

Field No. Permit # 276

State Well No. 07-56-307

Owner's Well No. _____

County Potter

1. Location: NW 1/4, NW 1/4 Sec. 127, Block B-9, Survey B.S. & F

0		
	Sec. 127	

2. Owner: Caroline B. Emery Address: Box 1230, Amarillo, Tx.

Tenant: Victor Plunk Address: Rt 1, Box 544, Amarillo, Tx.

Driller: Bud Gibbons Address: Plainview, TX

3. Elevation of _____ is 3814 ft. above msl, determined by _____

4. Drilled: 3-8-74; Dug, Cable Tool Rotary

5. Depth: Rept. 295 ft. Meas. _____ ft. Red Bed Reported @ 287.5 ft.

6. Completion: Open Hole Straight Wall Underreamed, Gravel Packed

7. Pump: Mfg. Johnston p.b., Amarillo GA. Type Turbine

No. Stages 7, Bore Diam. 10 in., Setting 290 ft.

Column Diam. 6 in., Length Tailpipe 10 ft.

8. Motor: Fuel NAT. GAS Make & Model M.M. 6cyl. HP.

9. Yield: Flow _____ gpm, Pump 400 gpm, Meas. Rept. Est. Driller

10. Performance Test: Date _____ Length of Test _____ Made by _____

Static Level _____ ft. Pumping Level _____ ft. Drawdown _____ ft.

Production _____ gpm Specific Capacity _____ gpm/ft.

11. Water Level: 227.98 ft. 9/13 1976 above See MP Below

_____ ft. meas.	_____	_____	_____	_____	_____	_____	_____
_____ ft. rept.	_____	_____	_____	_____	_____	_____	_____
_____ ft. meas.	_____	_____	_____	_____	_____	_____	_____
_____ ft. rept.	_____	_____	_____	_____	_____	_____	_____
_____ ft. meas.	_____	_____	_____	_____	_____	_____	_____
_____ ft. rept.	_____	_____	_____	_____	_____	_____	_____

12. Use: Dom., Stock, Public Supply, Ind. Irr. Waterflooding. Observation Not Used.

13. Quality: (Remarks on taste, odor, color, etc.) _____

Temp. _____ °F, Date sampled for analysis _____ Laboratory _____

Temp. _____ °F, Date sampled for analysis _____ Laboratory _____

Temp. _____ °F, Date sampled for analysis _____ Laboratory _____

14. Other data available as circled: Driller's Log Radioactivity Log, Electric Log,

Formation Samples, Pumping Test,

15. Record by: DAN SCALE Date 9/13 1976

Source of Data Field & HPUCD #1 Records

16. Remarks: Permission from Mr. F. E. Collard III, manager to enter this well into the program

CASING & BLANK PIPE			
Cemented From _____ ft. to _____ ft.		Setting, ft.	
Diam. (in.)	Type	from	to
14	Steel	Surface	295

WELL SCREEN			
Screen Openings			
Diam. (in.)	Type	Setting, ft.	
		from	to
14	Perforated	197	295
	Casing Perforated with 3/8" slits		
	4 row pattern.		

Obs Well

3814
289
3525

M.P. - Edge of Airline hole
inside pump part
S. side = +0.50 ft

Typewrite (Black ribbon) or Print Plainly
(soft pencil or black ink)
Do not use ball point pen

Texas Department of Health Laboratories
1100 West 49th Street
Austin, Texas 78756

TDWR ONLY

Organization No. _____ Lab No.

Work No. _____

CHEMICAL WATER ANALYSIS REPORT

Send report to:

Data Collection and Evaluation Section
Texas Department of Water Resources
P.O. Box 13087
Austin, Texas 78711

S. R. S.

SEP 19 1980

County 188 Butler

State Well No. 07 56 307

Well No. 276

Date Collected 08 01 80

Location NW 1/4, NW 1/4, Sec. 127, Blk B-9, BS+F Survey Sample No. By HPAWCD #1 B2

Source (type of well) turbine Owner Caroline Embry

Date Drilled 3-8-74 Depth 295 ft. WBF Ogallala

Producing intervals _____ Water level _____ ft. Sample depth ft.

Sampled after pumping cont hrs. Yield _____ GPM meas. est. Temperature °F °C

Point of collection faucet on discharge Appearance clear turbid colored other

Use Irr. Remarks _____

(FOR LABORATORY USE ONLY)

CHEMICAL ANALYSIS

SEP 17 '80

Laboratory No. CO15975 Date Received AUG 18 1980 Date Reported _____

	MG/L	ME/L		MG/L	ME/L
Silica . . . 00955 . . .	57		Carbonate . . . 00445 . . .	0	
Calcium . . . 00915 . . .	47	2.36	¹⁴⁴ Bicarbonate . . . 00440 . . .	293	4.80
Magnesium . . . 00925 . . .	26	2.11	Sulfate . . . 00945 . . .	30	0.62
Sodium . . . 00929 . . .	29	1.26	Chloride . . . 00940 . . .	7	0.20
		Total 5.73	Fluoride . . . 00951 . . .	2.4	0.13
<input type="checkbox"/> Potassium . . . 00937 . . .			Nitrate . . . 71850 . . .	2.9	
<input type="checkbox"/> Manganese . . . 01055 . . .			pH . . . 00403 . . .	8.2	Total 5.75
<input type="checkbox"/> Boron . . . 01022 . . .			¹ Dissolved Solids (residue at 180°C) . . . 70300 . . .		350
<input type="checkbox"/> Total Iron . . . 01045 . . .			Phenolphthalein Alkalinity as CaCO ₃ . . . 00415 . . .		0
<input type="checkbox"/> (other) _____ MG/L			Total Alkalinity as CaCO ₃ (4.80) . . . 00410 . . .		240
Specific Conductance (micromhos/cm ³) . . . 00095 . . .	490		Total Hardness as CaCO ₃ (4.47) . . . 00900 . . .		224
Diluted Conductance (micromhos/cm ³) <u>4</u> x <u>144</u>		576	² Nitrogen Cycle		
			Ammonia - N . . . 00610 . . .		
			Nitrite - N . . . 00615 . . .		
			Nitrate - N . . . 00620 . . .		
			Organic Nitrogen . . . 00605 . . .		

items will be analyzed if checked.

The bicarbonate reported in this analysis can be converted by computation (multiplying by 0.4917) to an equivalent amount of carbonate, and the carbonate figure used in the computation of dissolved solids.
² Nitrogen cycle requires separate sample.
³ Total Iron and Manganese require separate sample.

JUL 25 1981

Analyst _____ Checked By _____

102°00'
35°15'

228000m. E.

729

730

5730' 731

3904000m. N.

3903

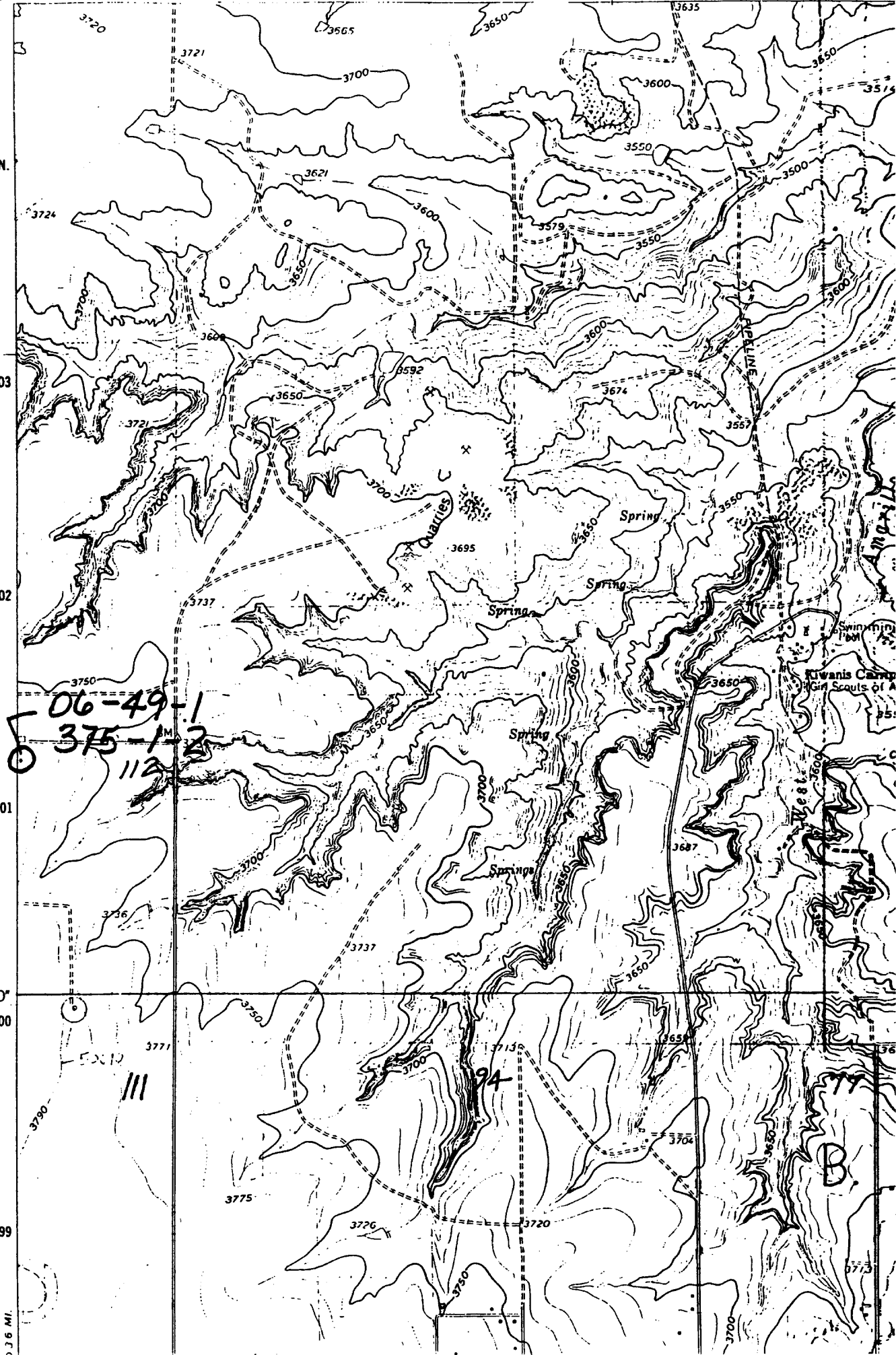
3902

3901

1230'

3900

3899



TEXAS WATER DEVELOPMENT BOARD

CHEMICAL WATER ANALYSIS REPORT
DW3900 FORM 1/DG#5

Send Reply To:
Water Availability Data
and Studies Section
Texas Water Development Board
Stephen F. Austin Building
1700 Congress Avenue
Austin, Texas 78711

TWDB ONLY
Organization No. 375-1-2
Work No. _____

Attn: Phil Nordstrom Room: _____

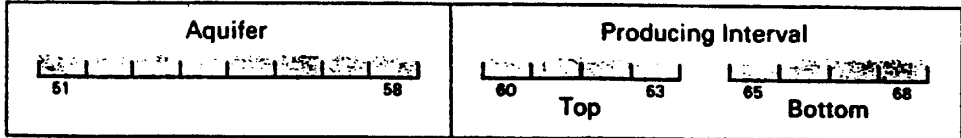
Laboratory Code 01
10 11

County Potter State Well No. 06 49 101
Date Collected 08 04 1988 Sample No. 1 Time 14 : 43
By HPWCD #1 D.S. + C.G. Code for Sample Collecting Agency 07

Temperature 18 °C
42 43

If Different From Completed Well

Analysis Reliability Remark 45 46
Chemical Constituent Remark 48 49



Remarks _____

Owner Marshall Cutwright, Jr. Send copy to owner

Address P.O. Box 3176, Amarillo, Tx. 79116

Date Drilled _____ Depth _____ ft. WBF 12106LL Point of collection Faucet

Sampled after pumping .75 hrs. Yield _____ GPM megs. Use domestic
est.

CHEMICAL ANALYSIS

Date Received

SEP 07 '88

Date Reported

OCT 17 '88

Laboratory No.	Date Received	ME/L	Date Reported	Flag	MG/L
EB9-135	090888		101088		
Silica	00955				49
Calcium	00915	2.14			42.00
Magnesium	00925	2.22			27.00
Sodium	00930	.91			21
Potassium	00935	.13			5.0
T.Cations(+)		5.4			
Carbonate	00445	.12			3.0
Bicarbonate	00440	4.7			287.0
Sulfate	00946	.46			22
Chloride	00940	.11			4
Fluoride	00950	.09			1.7
Nitrate as NO3	71851	.06			3.46
Total Anions(-)		5.54			
pH	00403				8.6
Dissolved Solids (Sum)	70301				321
P.Alk as CaCO3	00415				3
T.Alk as CaCO3	00410				241
T.Hardness as CaCO3	00900				218
Specific Conductance (umhos @ 25 C)	00095				548

KEY PUNCHED

Phenol Alk as CaCO₃ 00415 25 27 32
Total Alk as CaCO₃ 00410 34 36 41
Total Hardness as CaCO₃ 00900 43 45 50
Specific Conductance (umhos at 25C) 00095 52 54 59

Send original copy by certified mail to the Texas Department of Water Resources P. O. Box 13087 Austin, Texas 78711

State of Texas WATER WELL REPORT

ATTENTION OWNER: Confidentiality Privilege Notice on Reverse Side

For TDWR use only Well No. 07-56-3E Located on map YES Received: C.F.D.

OWNER John Porter (Name) Address Box 162 (Street or RFD) Cactus Texas 79013 (City) (State) (Zip) LOCATION OF WELL: Potter 5 (County) miles in NW (Direction) direction from Amarillo, Tex. (Town) Well Location Bishop Hills Estate

Driller must complete the legal description to the right with distance and direction from two intersecting section or survey lines, or he must locate and identify the well on an official Quarter- or Half-Scale Texas County General Highway Map and attach the map to this form.

Legal description: Section No. Block No. Township Abstract No. Survey Name Distance and direction from two intersecting section or survey lines See attached map.

3) TYPE OF WORK (Check): New Well Deepening Reconditioning Plugging 4) PROPOSED USE (Check): Domestic Industrial Public Supply Irrigation Test Well Other 5) DRILLING METHOD (Check): Mud Rotary Air Hammer Driven Bored Air Rotary Cable Tool Jetted Other

6) WELL LOG: Date drilled March 19, 1981 DIAMETER OF HOLE Dia. (in.) From (ft.) To (ft.) 8 3/4 Surface 350 7) BOREHOLE COMPLETION: Open Hole Straight Wall Underreamed Gravel Packed Other If Gravel Packed give interval ... from 0 ft. to 350 ft.

Table with 5 columns: From (ft.), To (ft.), Description and color of formation material, Dia. (in.), New or Used. Rows include Topsoil & Caliche, Galiche & rock, Rock & Clay, White Clay & Sand, Sand & Gravel, Sand & Gray clay, Gray & white clay, White, gray, & red clay, Gray & red clay, Red clay & gravel, Red clay, Red clay, TD.

8) CASING, BLANK PIPE, AND WELL SCREEN DATA: Table with 5 columns: Dia. (in.), New or Used, Steel, Plastic, etc. Perf., Slotted, etc. Screen Mfg., if commercial, Setting (ft.) From To, Gage Casing Screen. Row: 6 New Steel, Perf. 250 350

CEMENTING DATA Cemented from ft. to ft. Method used Cemented by (Company or Individual)

9) WATER LEVEL: Static level 250 ft. below land surface Date 3-19-81 Artesian flow gpm. Date

10) PACKERS: Table with 3 columns: Type, Depth

11) TYPE PUMP: Turbine Jet Submersible Cylinder Other Depth to pump bowls, cylinder, jet, etc., 315 ft.

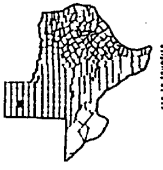
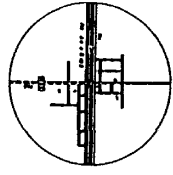
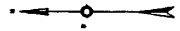
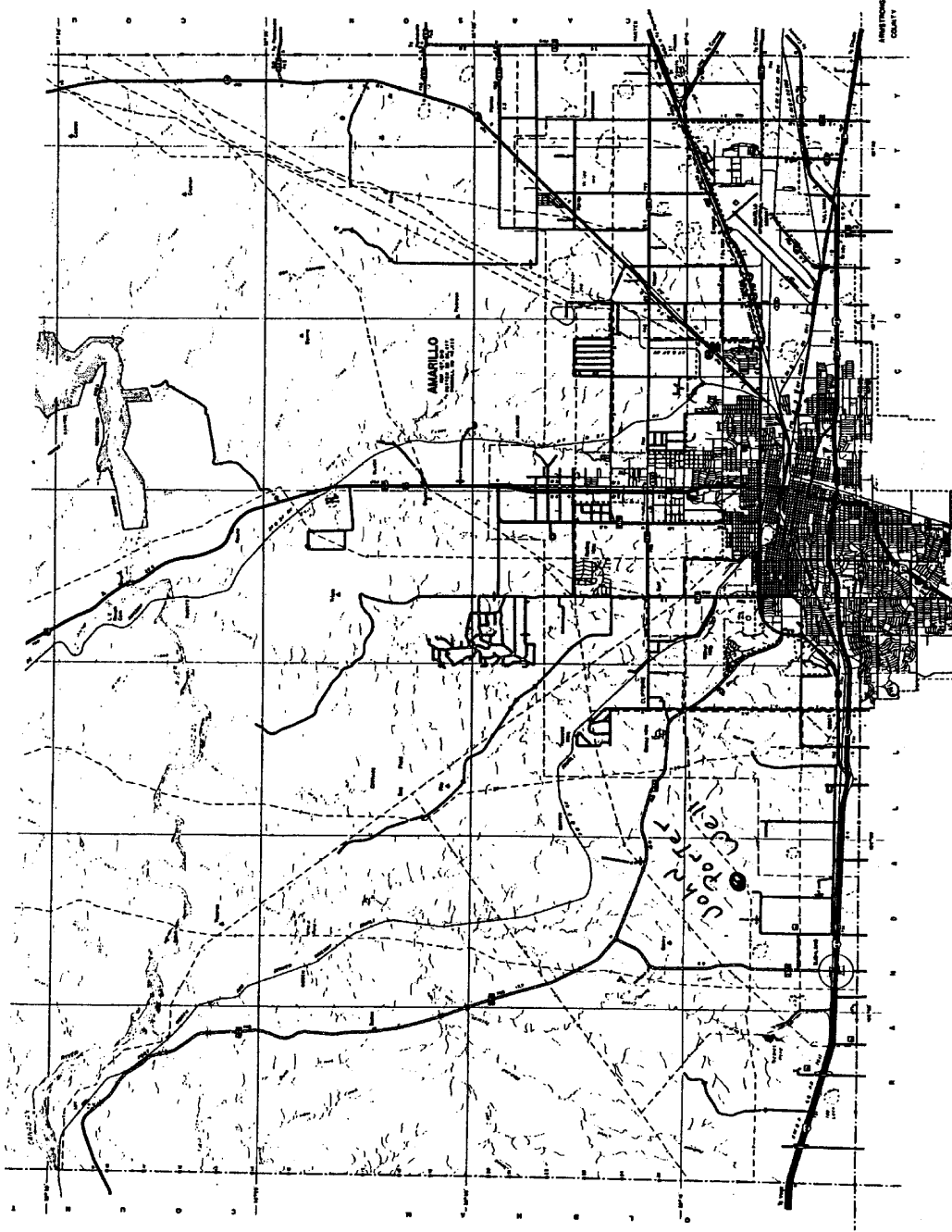
13) WATER QUALITY: Did you knowingly penetrate any strata which contained undesirable water? No If yes, submit "REPORT OF UNDESIRABLE WATER" Type of water? Depth of strata? Was a chemical analysis made? No

12) WELL TESTS: Type Test: Pump Bailer Jetted Estimated Yield: 23 gpm with 25 ft. drawdown after 3 hrs.

I hereby certify that this well was drilled by me (or under my supervision) and that each and all of the statements herein are true to the best of my knowledge and belief.

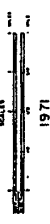
Driller: Jimmy McCaskill (Type or Print) Water Well Drillers Registration No. 1771 ADDRESS: 8018 River Road (Street or RFD) Amarillo (City) Texas (State) 79108 (Zip) (Signed) Jimmy McCaskill (Water Well Driller) A & A Drilling Company (Company Name)

Please attach electric log, chemical analysis, and other pertinent information, if available.



**GENERAL HIGHWAY MAP
POTTER COUNTY
TEXAS**

PREPARED BY THE
STATE DEPARTMENT OF HIGHWAYS
AND PUBLIC TRANSPORTATION
IN COOPERATION WITH THE
FEDERAL DEPARTMENT OF TRANSPORTATION
FEDERAL HIGHWAY ADMINISTRATION



1971
HIGHWAYS SHOWN TO 1:100,000
Scale of this map is 1:100,000
Copyright © 1971 by the State Department of Highways and Public Transportation
U.S. GOVERNMENT PRINTING OFFICE: 1971 O-350-000

Send original copy by certified mail to the Texas Department of Water Resources P. O. Box 13087 Austin, Texas 78711

State of Texas
WATER WELL REPORT

Texas Water Well Drillers Board
P. O. Box 13087
Austin, Texas 78711

ATTENTION OWNER: Confidentiality Privilege Notice on Reverse Side

1) DRILLER Day and Company (Name) Address 6309 S. Indiana Lubbock TX 79413
(Street or RFD) (City) (State) (Zip)
2) LOCATION OF WELL: Potter County 6 miles in W.N.W. direction from Amarillo
(N.E., S.W., etc.) (Town)

Driller must complete the legal description to the right with distance and direction from two intersecting section or survey lines, or he must locate and identify the well on an official Quarter- or Half-Scale Texas County General Highway Map and attach the map to this form.
 Legal description: Section No. _____ Block No. _____ Township _____
Abstract No. _____ Survey Name _____
Distance and direction from two intersecting section or survey lines _____
 See attached map. map on 07-56-31

3) TYPE OF WORK (Check):
 New Well Deepening Reconditioning Plugging
4) PROPOSED USE (Check):
 Domestic Industrial Public Supply Irrigation Test Well Other _____
5) DRILLING METHOD (Check):
 Mud Rotary Air Hammer Driven Bored
 Air Rotary Cable Tool Jetted Other _____

3) WELL LOG:
Date drilled 3/14/85
DIAMETER OF HOLE
Dia. (in.) From (ft.) To (ft.)
8 3/4' Surface 300'
7) BOREHOLE COMPLETION:
 Open Hole Straight Wall Underreamed
 Gravel Packed Other _____
If Gravel Packed give interval ... from 10 ft. to 300 ft.

From (ft.)	To (ft.)	Description and color of formation material	Dia. (in.)	New or Used	Steel, Plastic, etc. Perf., Slotted, etc. Screen Mfg., if commercial	Setting (ft.)	Gage Casing Screen
						From	To
<u>1-15</u>		<u>Top soil w/ sandy caliche</u>					
<u>5-6</u>		<u>caliche + caliche rock</u>	<u>4 1/2"</u>	<u>N</u>	<u>Plastic</u>	<u>0</u>	<u>180'</u>
<u>10-75</u>		<u>caliche w/ sandy clay</u>	<u>4 1/2"</u>	<u>N</u>	<u>P.V.C. Perforated</u>	<u>170'</u>	<u>300'</u>
<u>5-105</u>		<u>med. to coarse sand w/ sandstone</u>					
<u>20</u>		<u>fine sand w/ cemented sand</u>					
<u>20-135</u>		<u>Fine sand</u>					
<u>35-240</u>		<u>fine to med. sand w/ sltk cemented sand</u>					
<u>40-255</u>		<u>fine to med. sand w/ fine gravel</u>					
<u>55-270</u>		<u>gray sandy clay w/ sand strips</u>					
<u>170-285</u>		<u>Red + gray clay w/ sandstone & cemented sand</u>					
<u>25-300</u>		<u>Red + gray clay w/ sandstone & cemented sand</u>					
<u>00'</u>		<u>Red clay</u>					

8) CASING, BLANK PIPE, AND WELL SCREEN DATA:
CEMENTING DATA
Cemented from 0 ft. to 10' ft.
Method used _____
Cemented by A-1 Pump + Well Service
(Company or Individual)

9) WATER LEVEL:
Static level 170' ft. below land surface Date 3/15/85
Artesian flow _____ gpm. Date _____

10) PACKERS: Type Depth

11) TYPE PUMP:
 Turbine Jet Submersible Cylinder
 Other _____
Depth to pump bowls, cylinder, jet, etc., 240' ft.

3) WATER QUALITY:
Did you knowingly penetrate any strata which contained undesirable water? Yes No
If yes, submit "REPORT OF UNDESIRABLE WATER"
Type of water? Fresh Depth of strata 130' ft
Was a chemical analysis made? Yes No

12) WELL TESTS:
 Type Test: Pump Bailer Jetted Estimated
Yield: 12 gpm with 60' ft. drawdown after 2 hrs.

I hereby certify that this well was drilled by me (or under my supervision) and that each and all of the statements herein are true to the best of my knowledge and belief.

NAME A-1 Pump + Well Service Water Well Driller's License No. 2119
(Type & Print)
ADDRESS Rt 2 Box 54-G Amarillo TX 79101
(Street or RFD) (City) (State) (Zip)
Signed Ricky O. Bush (Licensed Water Well Driller) (Signed) Ricky M. Jackson (Registered Driller Technician) DRP
Please attach electric log, chemical analysis, and other pertinent information, if available.
For TDWP use only
Well No. 07-56-31
Located on map YES C.F.S.

Send original copy by certified mail to the Texas Department of Water Resources P. O. Box 13087 Austin, Texas 78711

State of Texas
WATER WELL REPORT

Texas Water Well Drillers B
P. O. Box 13087
Austin, Texas 78711

ATTENTION OWNER: Confidentiality Privilege Notice on Reverse Side

1) OWNER DAY and Company (Name) Address 6309 B. Indiana (Street or RFD) Lubbock Tx. (City) (State) (Zip)
2) LOCATION OF WELL: Potter County 6 miles in W.N.W direction from Amarillo (N.E., S.W., etc.) (Town)

Driller must complete the legal description to the right with distance and direction from two intersecting section or survey lines, or he must locate and identify the well on an official Quarter- or Half-Scale Texas County General Highway Map and attach the map to this form.
 Legal description: Section No. _____ Block No. _____ Township _____
Abstract No. _____ Survey Name _____
Distance and direction from two intersecting section or survey lines _____
 See attached map.

3) TYPE OF WORK (Check): New Well Deepening Reconditioning Plugging
4) PROPOSED USE (Check): Domestic Industrial Public Supply Irrigation Test Well Other
5) DRILLING METHOD (Check): Mud Rotary Air Hammer Driven Bored Air Rotary Cable Tool Jetted Other

6) WELL LOG: Date drilled 3/12/85
DIAMETER OF HOLE: Dia. (in.) From (ft.) To (ft.)
2 3/4" Surface 300'
7) BOREHOLE COMPLETION: Open Hole Straight Wall Underreamed Gravel Packed Other
If Gravel Packed give interval ... from 10 ft. to 300

From (ft.)	To (ft.)	Description and color of formation material	Dia. (in.)	New or Used	Steel, Plastic, etc. Perf., Slotted, etc. Screen Mgt., if commercial	Setting (ft.)
						From To
		<u>0-15 Top soil w/ sandy caliche</u>				
		<u>15-60 Caliche + caliche rock</u>	<u>4 1/2"</u>	<u>N</u>	<u>Plastic</u>	<u>0 180'</u>
		<u>60-75 caliche w/ sandy clay</u>	<u>4 1/2"</u>	<u>N</u>	<u>P.U.C. Perforated</u>	<u>180' 300'</u>
		<u>75-105 med. to coarse sand w/ sandstone</u>				
		<u>105-120 Fine sand w/ cemented sand</u>				
		<u>120-135 Fine sand</u>				
		<u>135-240 Fine to med. sand w/ stks. cemented sand</u>				
		<u>240-255 Fine to med. sand w/ fine gravel</u>				
		<u>255-270 Gray sandy clay w/ sand strips</u>				
		<u>270-285 Red + gray clay w/ sandstone + cemented sand</u>				
		<u>285-300 Red + gray clay w/ sandstone + cemented sand</u>				
		<u>300' Red clay</u>				

8) CASING, BLANK PIPE, AND WELL SCREEN DATA:
CEMENTING DATA
Cemented from 0 ft. to 10
Method used _____
Cemented by A-1 Pump & Well Service (Company or Individual)

9) WATER LEVEL: Static level 170' ft. below land surface Date 3/14/85
Artesian flow _____ gpm. Date _____

10) PACKERS: Type _____ Depth _____
11) TYPE PUMP: Turbine Jet Submersible Cylinder Other
Depth to pump bowls, cylinder, jet, etc., 240' ft.

12) WELL TESTS: Type Test: Pump Bailor Jetted Estimate
Yield: 12 gpm with 60' ft. drawdown after 2 hr

13) WATER QUALITY: DEPT. OF WATER RESOURCES
Did you knowingly penetrate any strata which contained undesirable water? Yes No
If yes, submit "REPORT OF UNDESIRABLE WATER"
Type of water? Fresh Depth of strata 130' ft.
Was a chemical analysis made? Yes No

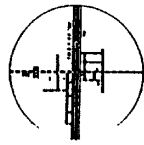
I hereby certify that this well was drilled by me (or under my supervision) and that each and all of the statements herein are true to the best of my knowledge and belief.

COMPANY NAME A-1 Pump & Well Service (Type or Print) Water Well Driller's License No. 2119
ADDRESS Rt. 2 Box 54-G (Street or RFD) Amarillo (City) Tx. (State) 79101 (Zip)
(Signed) Luby D. Bostick (Licensed Water Well Driller) (Signed) Richy D. Jackson (Registered Driller/Owner)

Please attach electric log, chemical analysis, and other pertinent information, if available. For TDWR use only Well No. 07-56-21 Located on map YES

LEGEND

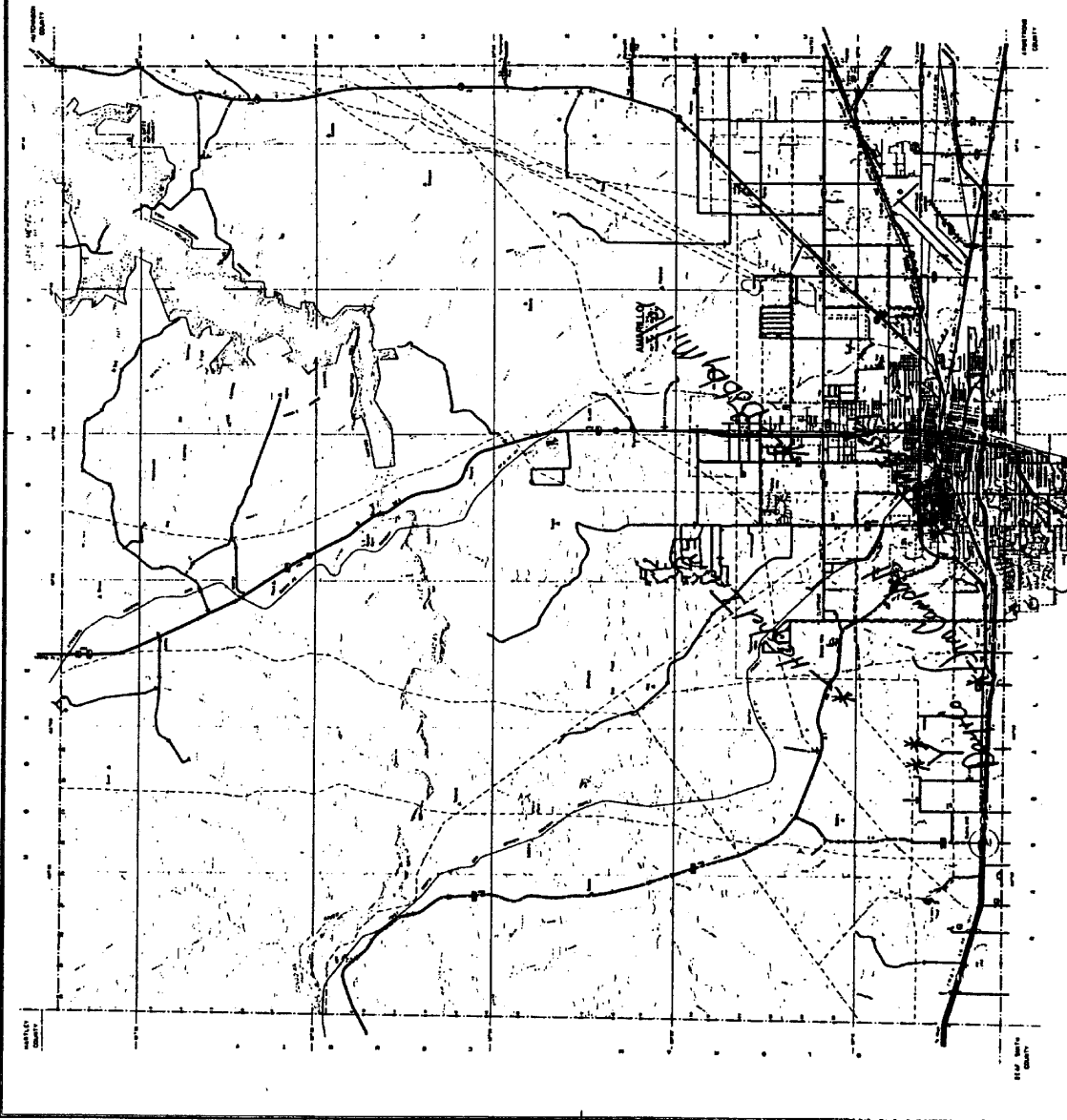
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[Symbol]	State Highway
[Symbol]	County Road
[Symbol]	Proposed Highway
[Symbol]	Waterway
[Symbol]	City
[Symbol]	Town
[Symbol]	Unincorporated Community
[Symbol]	Section
[Symbol]	Range
[Symbol]	County
[Symbol]	State



**GENERAL HIGHWAY MAP
POTTER COUNTY
TEXAS**

STATE DEPARTMENT OF HIGHWAYS
AND PUBLIC TRANSPORTATION
U.S. DEPARTMENT OF TRANSPORTATION

1971
 PREPARED BY THE STATE DEPARTMENT OF HIGHWAYS AND PUBLIC TRANSPORTATION
 FROM THE 1968 GENERAL HIGHWAY MAP OF TEXAS
 AND THE 1968 GENERAL HIGHWAY MAP OF POTTER COUNTY, TEXAS



Please use black ink.
Send original copy by
certified mail to the
Texas Water Commission
P.O. Box 13087
Austin, Texas 78711

State of Texas
WATER WELL REPORT

Texas Water Well Drillers Board
P. O. Box 13087
Austin, Texas 78711

ATTENTION OWNER: Confidentiality Privilege Notice on Reverse Side

1) OWNER Robert Young Address Estates & Big Sky Amarillo, Tex
(Name) (Street or RFD) (City) (State)

2) LOCATION OF WELL:
County Potter 10 miles in Northwest direction from Amarillo
(N.E., S.W., etc.) (Town)

Legal description:
Driller must complete the legal description to the right with distance and direction from two intersecting section or survey lines, or he must locate and identify the well on an official Quarter- or Half-Scale Texas County General Highway Map and attach the map to this form.

Section No. _____ Block No. _____ Township _____
Abstract No. _____ Survey Name _____
Distance and direction from two intersecting section or survey lines _____

See attached map.

3) TYPE OF WORK (Check): New Well Deepening Reconditioning Plugging

4) PROPOSED USE (Check): Domestic Industrial Monitor Public Supply Irrigation Test Well Injection Other _____

5) DRILLING METHOD (Check): Mud Rotary Air Hammer Jetted Bored Air Rotary Cable Tool Other _____

6) WELL LOG:
Date Drilling: Started 1-14-88 19__ Completed _____ 19__

DIAMETER OF HOLE		
Dia. (in.)	From (ft.)	To (ft.)
9	Surface	460

7) BOREHOLE COMPLETION:
 Open Hole Straight Wall Underreamed
 Gravel Packed Other _____
If Gravel Packed give interval ... from 17 ft. to 460

From (ft.)	To (ft.)	Description and color of formation material
0	25	Topsoil, caliche, caprock.
25	50	Caliche, lt. brown sandy clay.
50	72	Lt. brown sandy clay.
72	94	Lt. brown sandy clay w/strks. sandstone.
94	116	Fine tight sand and sandstone, gravel @ 105'.
116	138	Gravel-hard, red clay & shale at 120'.
138	160	Red clay & shale.
160	182	Red clay & shale w/strks. gray clay.
182	204	Red clay & shale " " "
204	226	Grey & red clay w/strks. fine tight sandstone.
226	248	Grey & red clay w/strks. fine tight sandstone.
248	270	Red and grey clay & shale.
270	292	Red and grey clay & shale.
292	314	Red and grey shale, yellow clay & shale.
314	336	Yellow clay & shale.
336	358	Yellow clay & shale, red clay.
358	380	Red clay w/ shale strks.
380	402	Red clay w/ shale strks.
402	424	Red clay w/ shale strks.
424	446	Red clay w/strks. fine tight sand.

8) CASING, BLANK PIPE, AND WELL SCREEN DATA:

Dia. (in.)	New or Used	Steel, Plastic, etc. Perf., Slotted, etc. Screen Mfg., if commercial	Setting (ft.)		G. C. or S.C.
			From	To	
9	N	PVC .050 Perforations	0	260	
			260	460	

9) CEMENTING DATA [Rule 319.44(b)]
Cemented from 17 ft. to 2 ft. No. of Sacks 1
_____ ft. to _____ ft. No. of Sacks _____
Method used Mixed
Cemented by Mark Randall

10) SURFACE COMPLETION
 Specified Surface Slab Installed [Rule 319.44(c)]
 Pitless Adapter Used [Rule 319.44(d)]
 Approved Alternative Procedure Used [Rule 319.71]

11) WATER LEVEL:
Static level 240 ft. below land surface Date _____
Artesian flow _____ gpm. Date _____

12) PACKERS: 11, 15, 17 Type _____ Depth _____

13) TYPE PUMP: APR 10 1988
 Turbine Jet Submersible Cylinder
 OTHER WATER PUMP _____
Depth to pump bowls, cylinder, jet, etc., _____ ft.

15) WATER QUALITY:
Did you knowingly penetrate any strata which contained undesirable water? Yes No
If yes, submit "REPORT OF UNDESIRABLE WATER"
Type of water? _____ Depth of strata _____
Was a chemical analysis made? Yes No

14) WELL TESTS:
Type Test: Pump Bailer Jetted Estimated
Yield: _____ gpm with _____ ft. drawdown after _____ hrs.

I hereby certify that this well was drilled by me (or under my supervision) and that each and all of the statements herein are true to the best of my knowledge and belief. I understand that failure to complete items 1 thru 12 will result in the log(s) being returned for completion and resubmittal.

COMPANY NAME K-Ran Drilling, Inc, Water Well Driller's License No. 2848-W
(Type or Print)

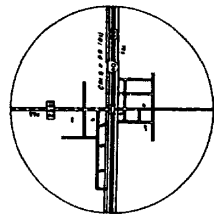
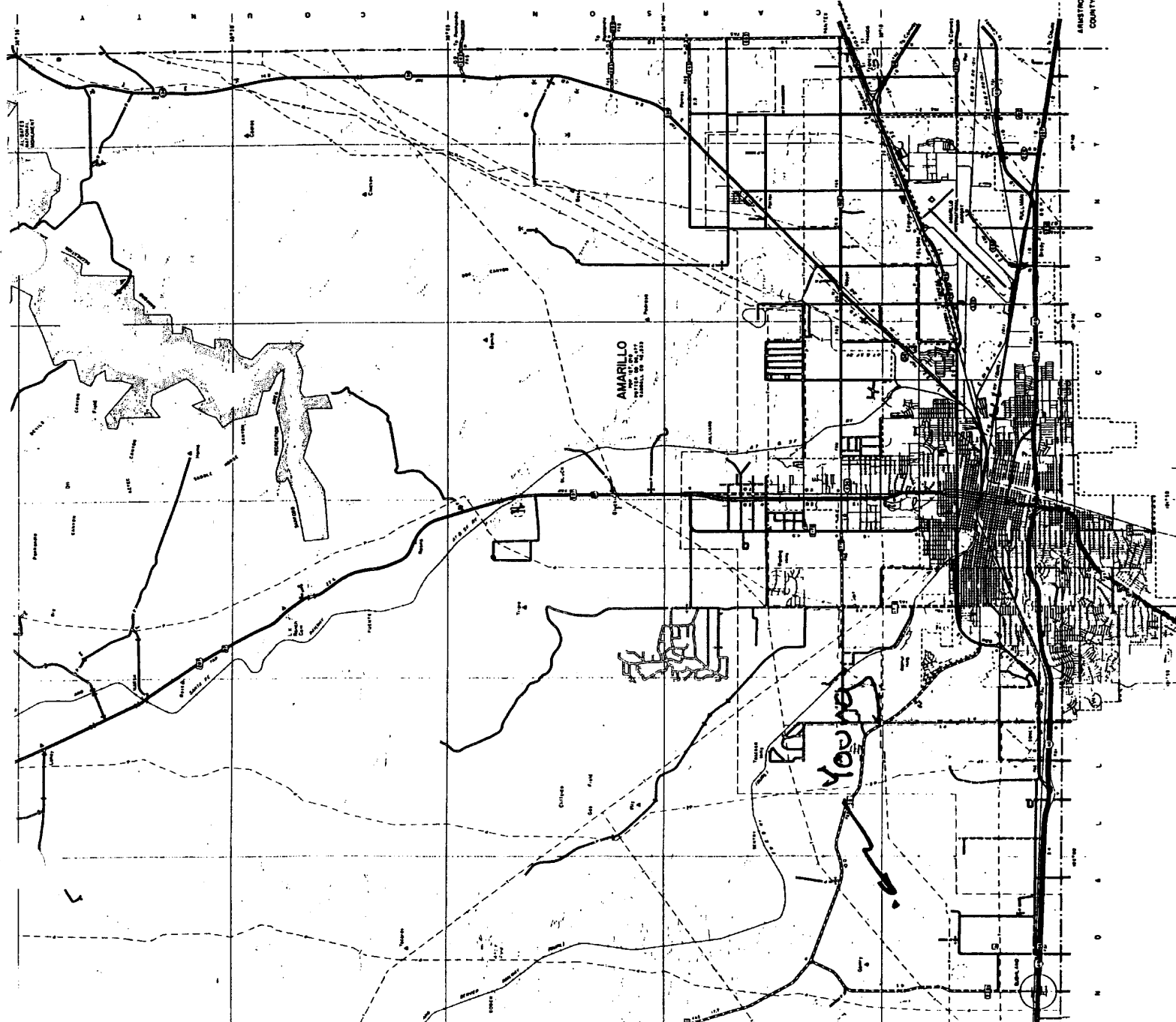
ADDRESS Rt. 6, Box 106 Amarillo, Texas 79106
(Street or RFD) (City) (State) (Zip)

(Signed) [Signature] (Signed) _____
(Licensed Water Well Driller) (Registered Driller Trainee)

Please attach electric log, chemical analysis, and other pertinent information, if available.

For TWC use only
Well No. 27-56-3
Located on map _____

1. ROAD CLASSIFICATION
 2. ROAD TYPE
 3. ROAD WIDTH
 4. ROAD SURFACE
 5. ROAD CONDITION
 6. ROAD GRADE
 7. ROAD ALIGNMENT
 8. ROAD RIGHT-OF-WAY
 9. ROAD INTERSECTION
 10. ROAD BRIDGE
 11. ROAD TUNNEL
 12. ROAD CULVERT
 13. ROAD DRAINAGE
 14. ROAD LIGHTING
 15. ROAD SIGNAGE
 16. ROAD FENCE
 17. ROAD BARRIER
 18. ROAD MEDIAN
 19. ROAD SHOULDER
 20. ROAD PAVEMENT
 21. ROAD GRADE SEPARATION
 22. ROAD CROSSING
 23. ROAD JUNCTION
 24. ROAD DIVERSION
 25. ROAD CLOSURE
 26. ROAD REPAIR
 27. ROAD CONSTRUCTION
 28. ROAD MAINTENANCE
 29. ROAD SAFETY
 30. ROAD ACCESS
 31. ROAD EGRESS
 32. ROAD ENTRANCE
 33. ROAD EXIT
 34. ROAD RAMP
 35. ROAD ON-RAMP
 36. ROAD OFF-RAMP
 37. ROAD OVERPASS
 38. ROAD UNDERPASS
 39. ROAD VIADUCT
 40. ROAD TRESTLE
 41. ROAD GALLERY
 42. ROAD BOX CULVERT
 43. ROAD ARCH CULVERT
 44. ROAD PIPE CULVERT
 45. ROAD DRAINAGE CANAL
 46. ROAD DRAINAGE DITCH
 47. ROAD DRAINAGE TRENCH
 48. ROAD DRAINAGE STRUCTURE
 49. ROAD DRAINAGE SYSTEM
 50. ROAD DRAINAGE NETWORK



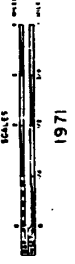
BUSHLAND



KEY TO QUANTITIES

GENERAL HIGHWAY MAP POTTER COUNTY TEXAS

PREPARED BY THE
 STATE DEPARTMENT OF HIGHWAYS
 AND PUBLIC TRANSPORTATION
 TRANSPORTATION PLANNING DIVISION
 IN COOPERATION WITH THE
 U.S. DEPARTMENT OF TRANSPORTATION
 FEDERAL HIGHWAY ADMINISTRATION

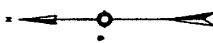


1971

HIGHWAYS REVISED TO OCTOBER 1, 1980

THIS MAP IS THE PROPERTY OF THE STATE DEPARTMENT OF HIGHWAYS AND PUBLIC TRANSPORTATION. IT IS LOANED TO YOU BY THE STATE DEPARTMENT OF HIGHWAYS AND PUBLIC TRANSPORTATION. IT IS TO BE RETURNED TO THE STATE DEPARTMENT OF HIGHWAYS AND PUBLIC TRANSPORTATION WHEN YOU RETURN IT.

FEDERAL HIGHWAY ADMINISTRATION
 U.S. DEPARTMENT OF TRANSPORTATION
 WASHINGTON, D.C. 20541



KEY TO SUPPLEMENTARY SHEETS

ATTENTION OWNER: Confidentiality
Privilege Notice on Reverse Side

State of Texas
WELL REPORT

Texas Water Well Drillers Board
P.O. Box 13087
Austin, Texas 78711

1) OWNER Steve Shamlin ADDRESS Eagletree Amarillo, Texas
(Name) (Street or RFD) (City) (State) (Z)
2) LOCATION OF WELL:
County Potter 10 miles in West direction from Amarillo
(NE, SW, etc.) (Town)

Driller must complete the legal description below with distance and direction from two intersecting section or survey lines, or he must locate and identify the well on an official Quarter- or Half-Scale Texas County General Highway Map and attach the map to this form.

LEGAL DESCRIPTION:

Section No. _____ Block No. _____ Township _____ Abstract No. _____ Survey Name _____
Distance and direction from two intersecting section or survey lines _____

SEE ATTACHED MAP

3) TYPE OF WORK (Check):
 New Well Deepening
 Reconditioning Plugging
4) PROPOSED USE (Check):
 Domestic Industrial Monitor Public Supply
 Irrigation Test Well Injection De-Watering
5) DRILLING METHOD (Check): Driven
 Mud Rotary Air Hammer Jetted Bored
 Air Rotary Cable Tool Other _____

6) WELL LOG:

Date Drilling: Started <u>12-13</u> 19 <u>93</u> Completed _____ 19____	DIAMETER OF HOLE		
	Dia. (In.)	From (ft.)	To (ft.)
	9	Surface	355

7) BOREHOLE COMPLETION:
 Open Hole Straight Wall Underreamed
 Gravel Packed Other _____
If Gravel Packed give interval ... from 17 ft. to 355 ft.

From (ft.)	To (ft.)	Description and color of formation material
0	15	Topsoil, caprock.
15	70	Caliche.
70	110	Green sandstone, conglomerate.
110	150	Red clay, shale.
150	185	Brn and gray clay, w/sandstone strks.
185	270	Red & white clay & shale w/ sandstone strks.
270	320	Reddish brn clay w/sand strks.
320	345	Red clay w/strks sand loose fast drilling.

8) CASING, BLANK PIPE, AND WELL SCREEN DATA:

Dia. (In.)	New or Used	Steel, Plastic, etc. Perf., Slotted, etc. Screen Mfg., if commercial	Setting (ft.)		Gage Casing Screen
			From	To	
5	N	Sch 40 PVC	0	225	
		.030 Perforations	225	345	
		10' blank on bottom			

13) TYPE PUMP:
 Turbine Jet Submersible Cylinder
 Other _____
Depth to pump bowls, cylinder, jet, etc., _____ ft.

9) CEMENTING DATA [Rule 287.44(1)]
Cemented from 2 ft. to 17 ft. No. of Sacks Used 4
20 1994 _____ ft. to _____ ft. No. of Sacks Used _____
Method used Cement
Cemented by Mixed

14) WELL TESTS:
Type Test: Pump Bailer Jetted Estimated
Yield: _____ gpm with _____ ft. drawdown after _____ hrs.

10) SURFACE COMPLETION
 Specified Surface Slab Installed [Rule 287.44(2)(A)]
 Specified Steel Sleeve Installed [Rule 287.44(3)(A)]
 Pitless Adapter Used [Rule 287.44(3)(B)]
 Approved Alternative Procedure Used [Rule 287.71]

15) WATER QUALITY:
Did you knowingly penetrate any strata which contained undesirable constituents?
 Yes No If yes, submit "REPORT OF UNDESIRABLE WATER"
Type of water? _____ Depth of strata _____
Was a chemical analysis made? Yes No

11) WATER LEVEL:
Static level 110 ft. below land surface Date _____
Artesian flow _____ gpm. Date _____

12) PACKERS: Type _____ Depth _____

I hereby certify that this well was drilled by me (or under my supervision) and that each and all of the statements herein are true to the best of my knowledge and belief. I understand that failure to complete Items 1 thru 15 will result in the log(s) being returned for completion and resubmittal.

COMPANY NAME K-Ran Drilling, Inc. WELL DRILLER'S LICENSE NO. 2848-WI
(Type or print)

ADDRESS Rt. 6, Box 106 Amarillo, Texas 79124-9502
(Street or RFD) (City) (State) (Zip)

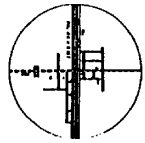
Drilled by [Signature] (Licensed Well Driller) (Signed) William M. Roberts (Registered Driller Trainee)

Please attach electric log, chemical analysis, and other pertinent information, if available.

For TWC use only: Well No. _____ Located on map _____

LEGEND

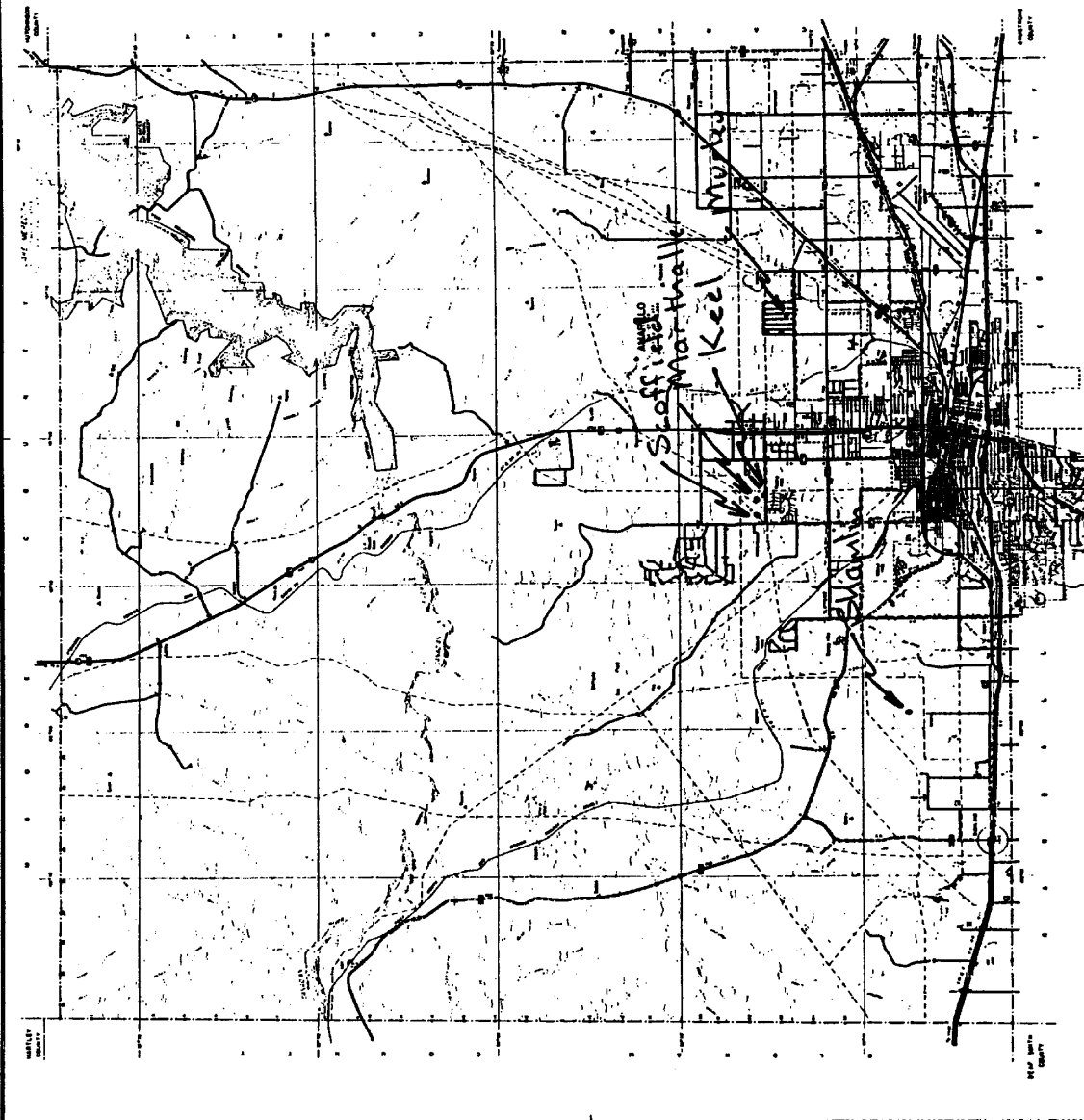
1. Interstate Highway	11. Secondary Road
2. Federal Highway	12. Unimproved Road
3. State Highway	13. Road Under Construction
4. County Road	14. Road Closed
5. Road	15. Road to be Closed
6. Road to be Closed	16. Road to be Closed
7. Road to be Closed	17. Road to be Closed
8. Road to be Closed	18. Road to be Closed
9. Road to be Closed	19. Road to be Closed
10. Road to be Closed	20. Road to be Closed



**GENERAL HIGHWAY MAP
POTTER COUNTY
TEXAS**

STATE DEPARTMENT OF HIGHWAYS
AND PUBLIC TRANSPORTATION
A DIVISION OF THE TEXAS
U.S. DEPARTMENT OF TRANSPORTATION
TEXAS DISTRICT OFFICE
AUSTIN, TEXAS

1971
REVISED TO OCTOBER 1970
REVISED TO OCTOBER 1969
REVISED TO OCTOBER 1968
REVISED TO OCTOBER 1967
REVISED TO OCTOBER 1966
REVISED TO OCTOBER 1965
REVISED TO OCTOBER 1964
REVISED TO OCTOBER 1963
REVISED TO OCTOBER 1962
REVISED TO OCTOBER 1961
REVISED TO OCTOBER 1960
REVISED TO OCTOBER 1959
REVISED TO OCTOBER 1958
REVISED TO OCTOBER 1957
REVISED TO OCTOBER 1956
REVISED TO OCTOBER 1955
REVISED TO OCTOBER 1954
REVISED TO OCTOBER 1953
REVISED TO OCTOBER 1952
REVISED TO OCTOBER 1951
REVISED TO OCTOBER 1950



Please use black ink, send original copy by certified mail to the Texas Department of Water Resources, P. O. Box 13087, Austin, Texas 78711

State of Texas
WATER WELL REPORT

Texas Water Well Drillers Board
P. O. Box 13087
Austin, Texas 78711

ATTENTION OWNER: Confidentiality Privilege Notice on Reverse Side

OWNER Harold Knight Address 8112 Coronado Amarillo, Texas 79110
(Name) (Street or RFD) (City) (State) (Zip)
LOCATION OF WELL:
County Potter miles in I-40 West direction from Amarillo, Turn North
n Dowell Rd 2 miles, 1/4 back west
(N.E., S.W., etc.) (Town)

Driller must complete the legal description to the right with distance and direction from two intersecting section or survey lines, or he must locate and identify the well on an official Quarter- or Half-Scale Texas County General Highway Map and attach the map to this form.

Legal description:
Section No. _____ Block No. _____ Township _____
Abstract No. _____ Survey Name _____
Distance and direction from two intersecting section or survey lines _____
 See attached map.

1) TYPE OF WORK (Check):
 New Well Deepening
 Reconditioning Plugging
4) PROPOSED USE (Check):
 Domestic Industrial Public Supply
 Irrigation Test Well Other _____
5) DRILLING METHOD (Check):
 Mud Rotary Air Hammer Driven Bored
 Air Rotary Cable Tool Jetted Other _____

WELL LOG:
Date drilled 4-8-1989
DIAMETER OF HOLE
Dia. (in.) From (ft.) To (ft.)
8 3/4 Surface 555

7) BOREHOLE COMPLETION:
 Open Hole Straight Wall Underreamed
 Gravel Packed Other _____
If Gravel Packed give interval ... from 15 ft. to 555 ft.

From (ft.)	To (ft.)	Description and color of formation material
- 1		Soil
- 44		Brown Sandy Clay
4- 62		White Sandy Clay & Soft Rock
2 - 105		Brown Sandy Clay
05 - 135		Brown Sandy Clay & Soft Rock
15 - 154		White & Brown Rock
4- 168		Red Clay
8 - 260		Red Clay & Blue Clay Streaks
0 - 281		Gray Clay & Soft Rock
1 - 285		Brown Clay & Soft Rock
5 - 342		Red & Gray Clay
2 - 398		Brown Clay & Soft Rock
8 - 405		Red with White Clay & Soft Rock
5 - 428		Red Clay & Soft Rock (loose)
8 - 436		Red & White Clay & Soft Rock
36 - 476		Red Clay
6- 505		Red & Gray Clay & Soft Rock
05 - 520		Yellow, Red & Gray Clay & Rock
0 - 524		Brown Sandy Clay & coarse Sand
4 - 545		Red, Yellow, Brown Clay & Rock
45 - 550		Course Sand
0 - 555		Red Bed

8) CASING, BLANK PIPE, AND WELL SCREEN DATA:

Dia. (in.)	New or Used	Steel, Plastic, etc. Perf., Slotted, etc. Screen Mfg., if commercial	Setting (ft.)		Gage Casing Screen
			From	To	
5	N	160 PVC	0	555	.020
		Perf 130 Ft			
		325-345/365-385			
		405-425/445-465			
		485-505/525-555			

9) CEMENTING DATA [Rule 319.44(b)]
Cemented from 0 ft. to 15 ft.
ft. to _____ ft.
Method used Hand Mixed
Cemented by Don DeHay

10) SURFACE COMPLETION
 Specified Surface Slab Installed [Rule 319.44(c)]
 Pitless Adapter Used [Rule 319.44(d)]
 Approved Alternative Procedure Used [Rule 319.71]

11) WATER LEVEL:
Static level 140 ft. below land surface Date 12-8-89
Artesian flow _____ gpm. Date _____

12) PACKERS: Type Depth
None None

13) TYPE PUMP:
 Turbine Jet Submersible Cylinder
 Other _____
Depth to pump bowls, cylinder, jet, etc., 540 ft.

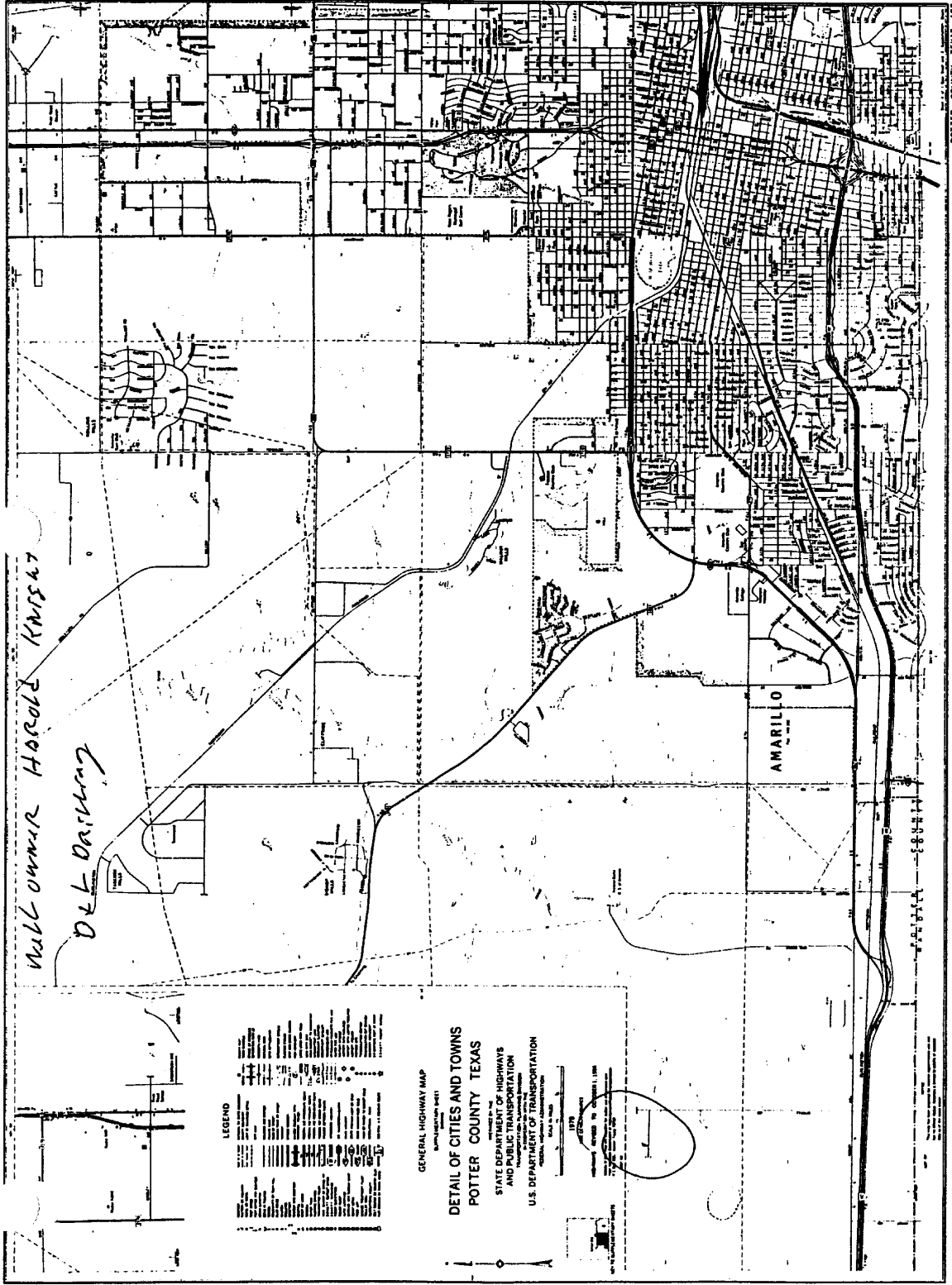
14) WELL TESTS:
Type Test: Pump Bailer Jetted Estimated
Yield: 15 gpm with 4.4 ft. drawdown after _____ hrs.

1) WATER QUALITY:
Did you knowingly penetrate any strata which contained undesirable water? Yes No
If yes, submit "REPORT OF UNDESIRABLE WATER"
Type of water? _____ Depth of strata 520
Was a chemical analysis made? Yes No

RECEIVED
DEC 20 1989

I hereby certify that this well was drilled by me (or under my supervision) and that each and all of the statements herein are true to the best of my knowledge and belief. I understand that failure to complete items 1 thru 12 will result in the log(s) being returned for completion and resubmittal.

COMPANY NAME D. & L. Drilling Water Well Driller's License No. 2558
(Type or Print)
ADDRESS 5606 McCormick Rd Amarillo, Texas 79118
(Street or RFD) (City) (State) (Zip)
Signed Don DeHay (Signed) _____ (Registered Driller Trainee)
Please attach electric log, chemical analysis, and other pertinent information, if available. For TDWR use only Well No. 06-49-1 Located on map _____



POTTER COUNTY TEXAS 188



TEXAS WATER DEVELOPMENT BOARD

Charles W. Jenness, *Chairman*
William B. Madden, *Member*
Diane E. Umstead, *Member*

Craig D. Pedersen,
Executive Administrator

Wesley E. Pittman, *Vice Chairman*
Noe Fernandez, *Member*
Othon Medina, Jr., *Member*

Telecommunications Cover Page Fax Number **(512) 445-1488**

DATE: 10/18/93

TO: Todd Lee
PERSON TO CONTACT

FROM: Phil Nordstrom
PERSON SENDING FAX

HDR
COMPANY NAME

TWDB
COMPANY NAME

TOWN _____ STATE _____

TOWN _____ STATE _____

214 960 4471
TELEFAX NUMBER

512 445 1488
TELEFAX NUMBER

COMMENTS: Requested data on located wells

Total Number of Pages Transmitting (including this cover page) 3

For Verification of telecommunications transmission, please contact the operator at (512) 445-1488.

AE: _____ OPERATOR: _____

**TEXAS WATER DEVELOPMENT BOARD
WATER LEVEL OBSERVATION WELL REPORT**

STATE WELL NUMBER: 0756307
 PREVIOUS WELL NUMBER: P276
 WELL LOCATION: LAT: 35 13 07
 LONG: 102 01 37
 WELL USE: I

CURRENT DATE: Oct 18 1993
 YEAR RECORD BEGINS: 1976
 ELEVATION OF LAND SURFACE: 3814
 DEPTH OF WELL: 295

DATE OF CURRENT MEASUREMENT MO DAY YEAR	CURRENT DEPTH TO WATER FROM LAND SURFACE	CHANGE IN LEVEL SINCE LAST STATIC MEASUREMENT	MEASUREMENT NUMBER	ELEVATION OF WATER LEVEL	MEASURING AGENCY	MEASUREMENT METHOD	REMARKS
09/13/1976	-227.48		01	3587	06	1	
01/03/1977	-232.87		01	3581	06	1	04
01/05/1978	-222.92	4.56	01	3591	06	1	
01/19/1979	-223.88	-0.96	01	3590	06	1	
12/05/1979	-225.07	-1.19	01	3589	06	1	
01/06/1981	-225.77	-0.70	01	3588	06	1	
01/19/1982	-224.64	1.13	01	3589	06	1	
02/22/1983	-223.77	0.87	01	3590	06	1	
01/03/1984	-224.45	-0.68	01	3590	06	1	
01/24/1985	-224.52	-0.07	01	3589	06	1	
02/1986	-224.78	-0.26	01	3589	06	1	
07/1987	-225.22	-0.44	01	3589	06	1	
02/10/1988	-224.53	0.69	01	3589	06	1	
01/03/1989	-224.88	-0.35	01	3589	06	1	
01/04/1990	-224.41	0.47	01	3590	06	1	
01/28/1991	-225.56	-1.15	01	3588	06	1	
01/20/1992	-226.23	-0.67	01	3588	06	1	
01/06/1993	-226.59	-0.36	01	3587	06	1	

AQUIFER: OGALLALA FORMATION
 BASIN : Red River
 COUNTY : Potter

WELL CLASS AND NUMBER: CURRENT 0756307

<u>SWN</u>	<u>USE</u>	<u>WQ</u>	<u>GPM YIELD</u>	
0649101	Domestic	Y ³¹⁹ _{TDS}	--	
0756301	Irr	N	--	
302	Irr	N	560	
303	Irr	N	800	
304	Irr	N	500	
305	Irr	N	--	
306	Irr	N	600	
*307	Irr	Y ³⁵⁰ _{TDS}	400	Current Obs.
602	Irr	N	700	
603	Irr	N	550	
604	Irr	N	500	
611	Irr	N	--	

Yield reported by driller during pump test.

0649101 Sampled in 1988 TDS=320
0756307 Sampled in 1980 TDS=350

ATTENTION-OWNER: Confidentiality
Privilege Notice on Reverse Side

State of Texas
WELL REPORT

Texas Water Well Drillers Board
P.O. Box 13087
Austin, Texas 78711

OWNER Lonnie Eaves ADDRESS _____ (Street or RFD) _____ (City) _____ (State) _____ (Zip)
(Name)

LOCATION OF WELL: County Potter _____ 9 miles in W direction from Amarillo _____
(NE, SW, etc.) (Town)

Driller must complete the legal description below with distance and direction from two intersecting section or survey lines, or he must locate and identify the well on an official Quarter- or Half-Scale Texas County General Highway Map and attach the map to this form.

LEGAL DESCRIPTION:

Section No. _____ Block No. _____ Township _____ Abstract No. _____ Survey Name _____

Distance and direction from two intersecting section or survey lines _____

SEE ATTACHED MAP

3) TYPE OF WORK (Check):

- New Well Deepening
 Reconditioning Plugging

4) PROPOSED USE (Check):

- Domestic Industrial Monitor Public Supply
 Irrigation Test Well Injection De-Watering

5) DRILLING METHOD (Check):

- Mud Rotary Air Hammer Jetted Bored
 Air Rotary Cable Tool Other _____

Driven

6) WELL LOG:

Date Drilling: 6-19-92
Started _____ 19____
Completed _____ 19____

DIAMETER OF HOLE

Dia. (in.)	From (ft.)	To (ft.)
9	Surface	336

7) BOREHOLE COMPLETION:

- Open Hole Straight Wall Underreamed

Gravel Packed Other _____

If Gravel Packed give interval ... from 17 ft. to 336 ft.

From (ft.) To (ft.) Description and color of formation material

8) CASING, BLANK PIPE, AND WELL SCREEN DATA:

From (ft.)	To (ft.)	Description and color of formation material
0	25	Topsoil, brn dirty sand w/ caliche layers.
25	50	Brn clean med sand, large broken gravel & cong @ 40'.
50	72	Conglomerate to 57', red clay.
72	94	Red clay w/shale strks.
94	116	" " " "
116	138	" " " "
138	160	" " " "
160	182	" " " "

Dia. (in.)	New or Used	Steel, Plastic, etc. Perf., Slotted, etc. Screen Mfg., if commercial	Setting (ft.)		Gage Casting Screen
			From	To	
5	N	PVC	0	154	
		.050 Perforations	154	314	
		10' blank on bottom			

(Use reverse side if necessary)

9) CEMENTING DATA [Rule 287.44(1)]

Cemented from 2 ft. to 17 ft. No. of Sacks Used 4
_____ ft. to _____ ft. No. of Sacks Used _____

Method used Mixed
Cemented by Mark Randall

10) SURFACE COMPLETION

- Specified Surface Slab Installed [Rule 287.44(2)(A)]
 Specified Steel Sleeve Installed [Rule 287.44(3)(A)]
 Pitless Adapter Used [Rule 287.44(3)(B)]
 Approved Alternative Procedure Used [Rule 287.71]

11) WATER LEVEL:

Static level 65' ft. below land surface Date _____
Artesian flow _____ gpm. Date _____

12) PACKERS:

Type _____ Depth _____

13) TYPE PUMP:

- Turbine Jet Submersible Cylinder

Other _____

Depth to pump bowls, cylinder, jet, etc., _____ ft.

14) WELL TESTS:

Type Test: Pump Bailor Jetted Estimated

Yield: _____ gpm with _____ ft drawdown after _____ Yes _____ No

15) WATER QUALITY:

Did you knowingly penetrate any strata which contained undesirable constituents? NO 11/14/1992

Yes No If yes, submit "REPORT OF UNDESIRABLE WATER"

Type of water? _____ Depth of strata _____

Was a chemical analysis made? Yes No

I hereby certify that this well was drilled by me (or under my supervision) and that each and all of the statements herein are true to the best of my knowledge and belief. I understand that failure to complete items 1 thru 15 will result in the log(s) being returned for completion and resubmittal.

COMPANY NAME K-Ran Drilling, Inc. WELL DRILLER'S LICENSE NO. 2848-W
(Type or print)

ADDRESS Rt. 6, Box 106 Amarillo, Texas 79124-9502
(Street or RFD) (City) (State) (Zip)

(Signed) [Signature] (Signed) _____
(Licensed Well Driller) (Registered Driller Trainee)

Please attach electric log, chemical analysis, and other pertinent information, if available. For TWC use only: Well No. _____ Located on map _____

ATTENTION OWNER: Confidentiality
Privilege Notice on Reverse Side

State of Texas WELL REPORT

Texas Water Well Drillers Board
P.O. Box 13087
Austin, Texas 78711

1) OWNER Charlene Barnard ADDRESS Eagle Tree Amarillo, Texas
 (Name) (Street or RFD) (City) (State) (Zip)

2) LOCATION OF WELL:
 County Potter 10 miles in West direction from Amarillo
 (NE, SW, etc.) (Town)

Driller must complete the legal description below with distance and direction from two intersecting section or survey lines, or he must locate and identify the well on an official Quarter- or Half-Scale Texas County General Highway Map and attach the map to this form.

LEGAL DESCRIPTION:

Section No. _____ Block No. _____ Township _____ Abstract No. _____ Survey Name _____

Distance and direction from two intersecting section or survey lines _____

SEE ATTACHED MAP

3) TYPE OF WORK (Check):

New Well Deepening
 Reconditioning Plugging

4) PROPOSED USE (Check):

Domestic Industrial Monitor Public Supply
 Irrigation Test Well Injection De-Watering

5) DRILLING METHOD (Check):

Mud Rotary Air Hammer Jetted Bored
 Air Rotary Cable Tool Other _____

6) WELL LOG:

Date Drilling: _____
Started 8-22 1990
Completed _____ 19____

DIAMETER OF HOLE

Dia. (in.)	From (ft.)	To (ft.)
8 3/4	Surface	338

7) BOREHOLE COMPLETION:

Open Hole Straight Wall Underreamed

Gravel Packed Other _____
If Gravel Packed give interval ... from 17 ft. to 338 ft.

From (ft.) To (ft.) Description and color of formation material

0	25	Topsoil, caliche, med. gravel.
25	50	Med gravel, red clay.
50	72	Red & grey clay.
72	94	Red & grey clay w/strks. of shale.
94	116	Red & grey clay w/strks. sandstone.
116	138	Red & grey clay w/strks. sandstone.
138	160	Red & grey clay w/strsk. sandstone.

(Use reverse side if necessary)

8) CASING, BLANK PIPE, AND WELL SCREEN DATA:

Dia. (in.)	New or Used	Steel, Plastic, etc. Perf., Slotted, etc. Screen Mfg., if commercial	Setting (ft.)		Gage Castir Scree
			From	To	
5	N	PVC	0	178	
		.050 Perforations	178	338	

9) CEMENTING DATA [Rule 287.44(1)]

Cemented from 2 ft. to 17 ft. No. of Sacks Used 4

_____ ft. to _____ ft. No. of Sacks Used _____

Method used Mixed
Cemented by Mark Randall

13) TYPE PUMP:

Turbine Jet Submersible Cylinder
 Other _____

Depth to pump bowls, cylinder, jet, etc., _____

14) WELL TESTS:

Type Test: Pump Bailer Jetted Estimated

Yield: _____ gpm with _____ ft. drawdown after _____ hrs.

15) WATER QUALITY:

Did you knowingly penetrate any strata which contained undesirable constituents?

Yes No If yes, submit "REPORT OF UNDESIRABLE WATER"

Type of water? _____ Depth of strata _____

Was a chemical analysis made? Yes No

10) SURFACE COMPLETION

Specified Surface Slab Installed [Rule 287.44(2)(A)]

Specified Steel Sleeve Installed [Rule 287.44(3)(A)]

Pitless Adapter Used [Rule 287.44(3)(B)]

Approved Alternative Procedure Used [Rule 287.71]

11) WATER LEVEL:

Static level 125 ft. below land surface Date _____

Artesian flow _____ gpm. Date _____

12) PACKERS:

Type	Depth

I hereby certify that this well was drilled by me (or under my supervision) and that each and all of the statements herein are true to the best of my knowledge and belief. I understand that failure to complete items 1 thru 15 will result in the log(s) being returned for completion and resubmittal.

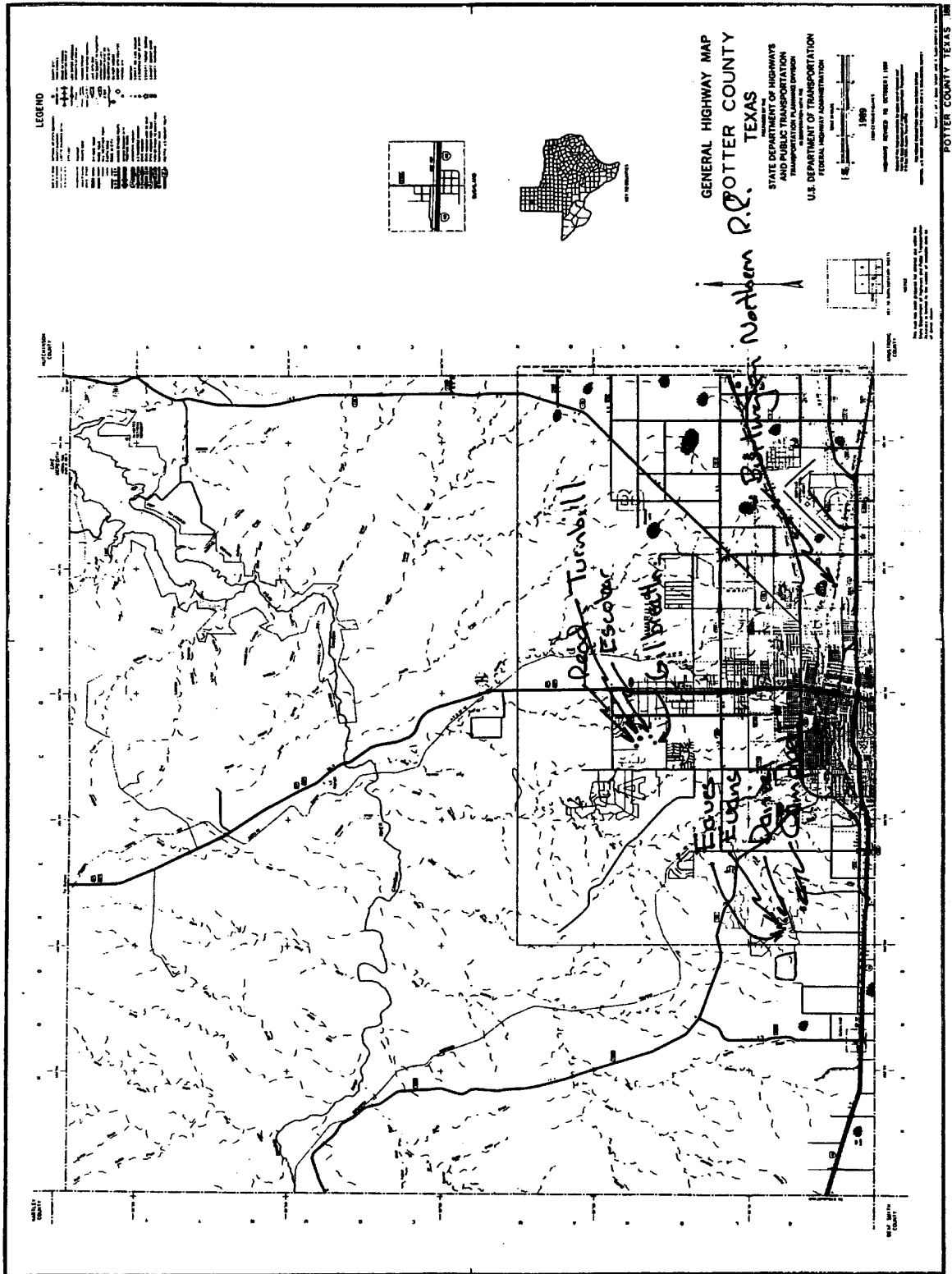
COMPANY NAME K-Ran Drilling, Inc. WELL DRILLER'S LICENSE NO. 2848-W
(Type or print)

ADDRESS Rt. 6, Box 106 Amarillo, Texas 79124-950
(Street or RFD) (City) (State) (Zip)

(Signed) [Signature] (Signed) _____
(Licensed Well-Driller) (Registered Driller Trainee)

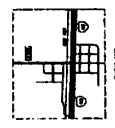
Please attach electric log, chemical analysis, and other pertinent information, if available.

For TWC use only: Well No. _____ Located on map _____



LEGEND

—	Interstate Highway
—	State Highway
—	County Road
—	Other Road
—	Waterway
—	Boundary
—	Settlement
—	Public Building
—	Religious Building
—	Government Building
—	Commercial Building
—	Industrial Building
—	Public Utility
—	Other



**GENERAL HIGHWAY MAP
POTTER COUNTY
TEXAS**

STATE DEPARTMENT OF HIGHWAYS
AND PUBLIC TRANSPORTATION
TRANSPORTATION PLANNING DIVISION
U.S. DEPARTMENT OF TRANSPORTATION
FEDERAL HIGHWAY ADMINISTRATION



POTTER COUNTY TEXAS

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ATTENTION OWNER: Confidentiality
Privilege Notice on Reverse Side

State of Texas
WELL REPORT

Texas Water Well Drillers Board
P.O. Box 13087
Austin, Texas 78711

1) OWNER Evan Evans ADDRESS Eagle Tree
(Name) (Street or RFD) (City) (State)
2) LOCATION OF WELL:
County Potter _____ 9 _____ miles in W direction from Amarillo
(NE, SW, etc.) (Town)

Driller must complete the legal description below with distance and direction from two intersecting section or survey lines, or he must locate and identify the well on an official Quarter- or Half-Scale Texas County General Highway Map and attach the map to this form.

LEGAL DESCRIPTION:

Section No. _____ Block No. _____ Township _____ Abstract No. _____ Survey Name _____

Distance and direction from two intersecting section or survey lines _____

SEE ATTACHED MAP

3) TYPE OF WORK (Check):

New Well Deepening
 Reconditioning Plugging

4) PROPOSED USE (Check):

Domestic Industrial Monitor Public Supply
 Irrigation Test Well Injection De-Watering

5) DRILLING METHOD (Check):

Mud Rotary Air Hammer Jetted Bored
 Air Rotary Cable Tool Other _____

6) WELL LOG:

Date Drilling:
Started 6-17-92 19__
Completed _____ 19__

DIAMETER OF HOLE

Dia. (in.)	From (ft.)	To (ft.)
9	Surface	370

7) BOREHOLE COMPLETION:

Open Hole Straight Wall Underreamed

Gravel Packed Other _____
If Gravel Packed give interval ... from 17 ft. to 370 ft.

From (ft.) To (ft.) Description and color of formation material

8) CASING, BLANK PIPE, AND WELL SCREEN DATA:

From (ft.)	To (ft.)	Description and color of formation material	Dia. (in.)	New or Used	Steel, Plastic, etc. Perf., Slotted, etc. Screen Mfg., if commercial	Setting (ft.)		Gage Casting Screen
						From	To	
0	25	Topsoil, fine brn sand.						
25	50	Fine brn sand, coarse sand & gravel @ 40'.	5	N	PVC	0	162	
50	72	Red & grey clay @ 51'.			PVC	302	342	
72	94	Red clay, grn shale & s/s @ 82			.050 Perforations	162	302	
94	116	Red clay w/shale strks.			.050 Perforations	342	362	
116	138	" " " "						
138	160	" " " "						
160	182	Red clay w/sand strks.						
182	204	Blue shale cemented brn sand.						

9) CEMENTING DATA [Rule 287.44(1)]

Cemented from 2 ft. to 17 ft. No. of Sacks Used 4
_____ ft. to _____ ft. No. of Sacks Used _____

Method used Mixed
Cemented by Mark Randall

10) SURFACE COMPLETION

Specified Surface Slab Installed [Rule 287.44(2)(A)]
 Specified Steel Sleeve Installed [Rule 287.44(3)(A)]
 Pitless Adapter Used [Rule 287.44(3)(B)]
 Approved Alternative Procedure Used [Rule 287.71]

11) WATER LEVEL:

Static level 60' ft. below land surface Date _____
Artesian flow _____ gpm. Date _____

12) PACKERS:

Type _____ Depth _____

13) TYPE PUMP:

Turbine Jet Submersible Cylinder
 Other _____

Depth to pump bowls, cylinder, jet, etc., _____

14) WELL TESTS:

Type Test: Pump Bailer Jetted Estimated
Yield: _____ gpm with _____ ft. drawdown after 14 hrs.

15) WATER QUALITY:

Did you knowingly penetrate any strata which contained undesirable constituents?
 Yes No If yes, submit "REPORT OF UNDESIRABLE WATER"
Type of water? _____ Depth of strata _____
Was a chemical analysis made? Yes No

I hereby certify that this well was drilled by me (or under my supervision) and that each and all of the statements herein are true to the best of my knowledge and belief. I understand that failure to complete items 1 thru 15 will result in the log(s) being returned for completion and resubmittal.

COMPANY NAME K-Ran Drilling, Inc. WELL DRILLER'S LICENSE NO. 2848-W
(Type or print)

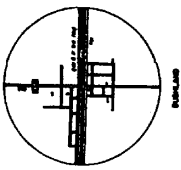
ADDRESS Rt. 6, Box 106 Amarillo, Texas 79124-9502
(Street or RFD) (City) (State) (Zip)

(Signed) [Signature] (Signed) _____
(Licensed Well Driller) (Registered Driller Trainee)

Please attach electric log, chemical analysis, and other pertinent information, if available. For TWC use only: Well No. _____ Located on map _____

LEGEND

Interstate Highway	State Highway	County Road	Local Road
Expressway	Trunk Road	Branch Road	Access Road
Proposed Interstate	Proposed State	Proposed County	Proposed Local
Waterway	Railroad	Power Line	Telephone Line
City	Village	Hamlet	Unincorporated Area
Water	Marsh	Swamp	Woods
Public Building	Religious Building	Commercial Building	Industrial Building
Government Building	Educational Building	Medical Building	Recreational Building
Public Utility	Transportation	Communication	Defense
Other			

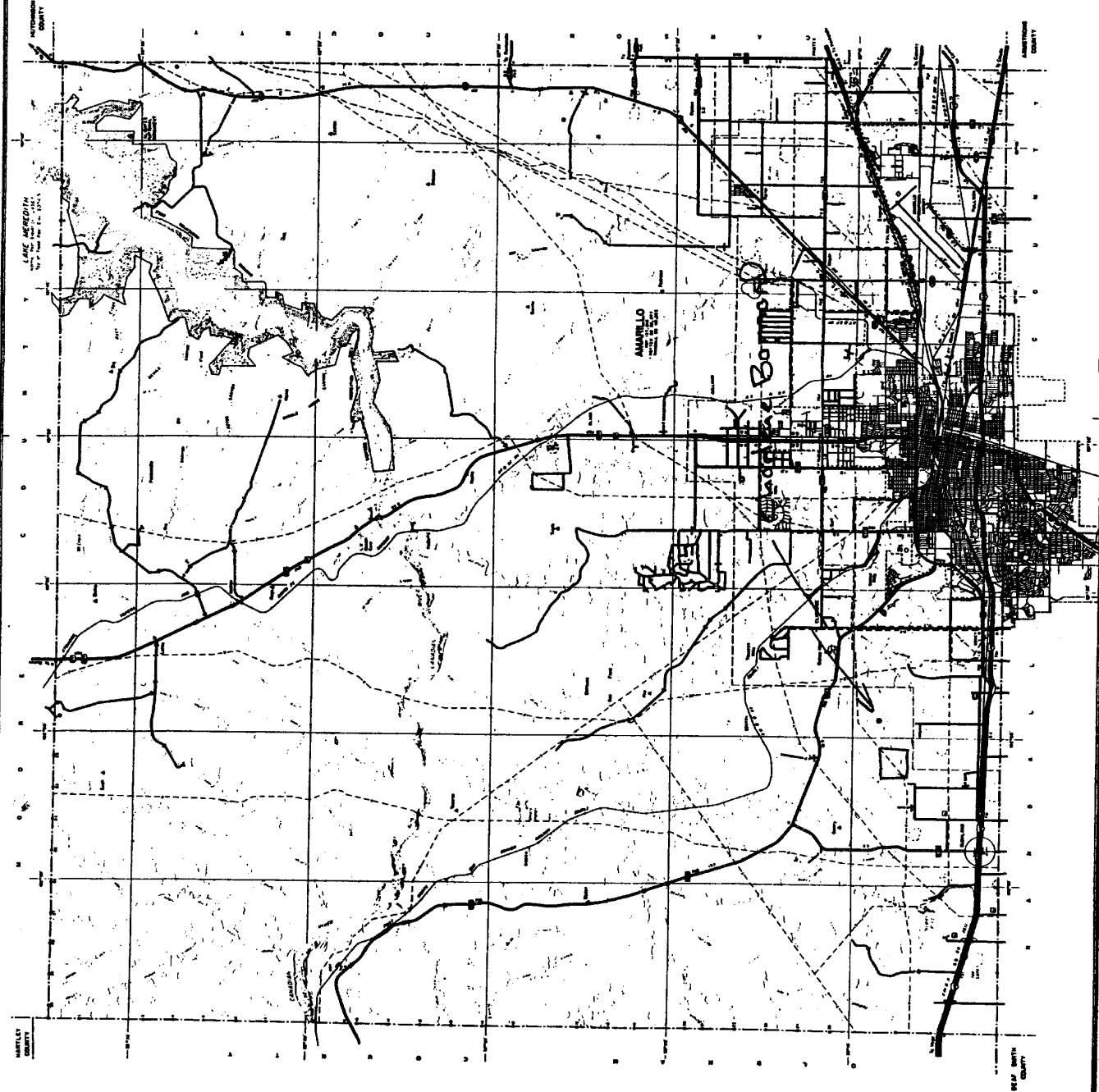


GENERAL HIGHWAY MAP POTTER COUNTY TEXAS

PREPARED BY THE
STATE DEPARTMENT OF HIGHWAYS
AND PUBLIC TRANSPORTATION
TRANSPORTATION ENGINEERING DIVISION
IN COOPERATION WITH THE
U.S. DEPARTMENT OF TRANSPORTATION
FEDERAL HIGHWAY ADMINISTRATION

SCALE
MILES
1971

REVISED TO OCTOBER 1, 1968
BASED ON THE 1967 GENERAL HIGHWAY MAP OF TEXAS
AND THE 1967 GENERAL HIGHWAY MAP OF POTTER COUNTY, TEXAS
FOR FURTHER INFORMATION CONTACT THE STATE DEPARTMENT OF HIGHWAYS AND PUBLIC TRANSPORTATION, TRANSPORTATION ENGINEERING DIVISION, 1000 WEST 11TH AVENUE, AUSTIN, TEXAS 78701



7-56-3(A-J)

and original copy by State of Texas
 Texas Water Development Board
 1001 North Loop West, Suite 1000
 Austin, Texas 78711

WATER WELL REPORT

1) OWNER:
 Person having well drilled: Bush Estate
 Landowner: Sam G. Bush
 Address: Box 1270 Amarillo, Texas
 (Street or RFD) (City) (State)

2) LOCATION OF WELL:
 County: COLLETT
 Labor: Victor Plunk Farm
 Block No.: 0
 Section: 127
 (Corner or survey as on town)
 miles in NE, SW, etc. direction from Amarillo (Town)
 (City) (State)

3) TYPE OF WELL (Check):
 New Well Despensing
 Reconditioning Plugging
 Irrigation Test Well Other
 4) PURPOSE USE (Check):
 Domestic Industrial Municipal
 Irrigation Test Well Other
 5) TYPE OF WELL (Check):
 Rotary Driven Bored
 Cable Jetted Bored
 AMA

6) WELL LOG:
 Diameter of hole 2 in. Depth drilled 200 ft. Depth of completed well 200 ft. Date drilled Dec. 68
 All measurements made from 0 ft. above ground level.

From (ft.)	To (ft.)	Description and color of formation material
0	2	BLK clay topsoil
2	80	Yellow clay
80	120	sandy caliche
120	141	sand, sandstone stringers
140	17	soft sand
170	218	sandstone
218	225	rock
225	275	Opallala sand

7) COMPLETION (Check):
 Straight well Gravel packed Other
 Underreamed Open hole

8) CASING:
 Type: old New Steel Plastic Other
 Cased from 0 ft. to 5 ft.

Diameter (inches)	SETTING		Slot size
	From (ft.)	To (ft.)	
6 5/8	0	200	1 7/16

9) WATER LEVEL: 100 ft. below land surface Date Dec. 68
 Static level 100 ft. below land surface Date Dec. 68
 Artesian pressure 0 lbs. per square inch Date 0

10) SCREEN:
 Type: March cut gauze
 Perforated Slotted

11) PUMP DATA:
 Manufacturer's Name: Armatron
 Type: Submersible H.P. 1
 Designed pumping rate 10 gpm gph
 Type power unit: Electric
 Depth to bowl, cylinder, jet, etc., 0 ft. below land surface.

12) WELL TESTS:
 Has a pump test made? Yes No If yes by whom?
 Yield: 0 gpm with 0 ft. drawdown after 0 hrs
 Better test 30 gpm with 1 ft. drawdown after 7 hrs
 Artesian flow 0 gpm Date 0
 Temperature of water 0
 Has a chemical analysis made? Yes No
 Did any strata contain undrinkable water? Yes No
 Type of water: potable depth of strata 190-237

I hereby certify that this well was drilled by me (or under my supervision) and that each and all of the statements herein are true to the best of my knowledge and belief.

Signature: C. A. Biggers (Type or Print)
 Address: 700 Valley Ave. Amarillo, Texas 79102
 (Street or RFD) (City) (State)

Water Well Drillers Registration No. 286
 (Company Name)

For TWDs use only
Well No. 07-26-24
Located on map
Received: 12/1/67

State of Texas
WATER WELL REPORT

OWNER:
Person having well drilled: W.M.H. BUSH CAT (Name)
Address: AMARILLO TEX (City) (State)

Landowner: SAMUELS ABRAHAM (Name)
Address: (Street or RFD) (City) (State)

LOCATION OF WELL:
County: ROBERTS (Name)
Mileage in (N.E., S.W., etc.) direction from: BUSHLAND (Town)

Locate by sketch map showing landmarks, roads, creeks, highway number, etc.
Give legal location with distances and directions from nearest section of survey lines.
Block: 9 League: East
Abstract No. (Mag. Net. S&T. Sec.) of Section: _____

PROPOSED USE (Check):
 Domestic
 Industrial
 Test Well
 Irrigation
 Municipal
 Other
 Dug
 Bored

WELL LOG:
Diameter of hole: 18" in. Depth of completed well: 356 ft. Date drilled: 12-20-67
All measurements made from _____ ft. above ground level.

From (ft.)	To (ft.)	Description and color of formation material	Casing Type: Old	New	Steel	Plastic	Other
0-14	301c	YCALICENE					
11-60		SANDY CLAY					
10-85		SHALE + CLAY					
13-95		CAP ROCK					
15-130		TIGHT SANDSHALE					
30-275		FINE SAND					
25-305		COURSE SAND					
205-345		ROCK + SAND STAS					
11-356		Red Bed					

11) WELL TESTS:
 (Use reverse side if necessary)
 Completion (Check):
 Sight well
 Cased packed
 Open hole
 Underreamed
 Other: _____
 Yield: _____ gpm with _____ ft. drawdown after _____ hrs.
 Boiler test: _____ gpm with _____ ft. drawdown after _____ hrs.
 Artesian flow: _____ gpm
 Temperature of water: _____

12) WATER QUALITY:
 Was a chemical analysis made? Yes No
 Did any strata contain undesirable water? Yes No
 Type of water? _____ depth of strata: _____

I hereby certify that this well was drilled by me (or under my supervision) and that each and all of the statements herein are true to the best of my knowledge and belief.
 Water Well Drillers Registration No. 306

NAME: W.G. GOYNE (Type or Print)
 ADDRESS: 1306 MOLIPAY DR (Street or RFD) PLAINVIEW TEX (City) (State)
 (Signed) W.G. Goyne (Under Well Driller) (Company Name)

1) OWNER: Person having well drilled W. H. Bush Estate (Name) Address Box 1220, Ams, Texas, 70105 (City) (State) (Zip)
 Landowner Same (Name) Address Same (City) (State) (Zip)
 County Tarrant (Name) Labor 9 (Type or Firm) Abstract No. BS&P (Name)
 Well No. 54 S&W Sec. of Section 13 Block No. 9
 6 miles in NW direction from Amarillo, Texas. In Northwest corner of the S.W. 1/4 quarter of section 13 of range 7E, T. 20N.

2) LOCATION: 4520 (Name) 240 (Name) 220 (Name)
 3) TYPE OF WORK (Check):
 New Well Deepening
 Reconditioning Plugging
 4) PROPOSED USE (Check):
 Domestic Industrial Municipal Irrigation Test Well Other Stock
 5) TYPE OF WELL (Check):
 Rotary Driven Dug Cable Jetted Bored
 6) WELL LOG:
 Diameter of hole 9 in. depth drilled 350 ft. Depth of completed well 350 ft. Date drilled Sept. 78
 All measurements made from 0 ft. above ground level.

From (ft.)	To (ft.)	Description and color of formation material
0	3	sandy brown top soil
3	40	yellow sandy clay
40	70	limestone w caliche & sandst.
70	140	sandy clay w sandstone st.
140	162	gravel
162	220	hard & soft str. red & grey shale
220	225	grey sandy shale w sandstone

7) COMPLETION (Check):
 Straight well Gravel packed Other
 Under reamed Open hole
 8) WATER LEVEL:
 Static level 210 ft. below land surface Date Sept. 78
 Artesian pressure --- lbs. per square inch Date ---
 9) CASING:
 Type: old New Steel Plastic Other
 Cemented from 0 ft. to 5 ft.
 10) SCREEN:
 Type Torch cut perforation
 Perforated Slotted
 Diameter (inches) From (ft.) Setting To (ft.) Slot size
5 5/8 2' above 350 188 350 1/16
 12) PUMP DATA:
 Manufacturer's Name Aeromotor windmill
 Type 10 Ft H.P.
 Designed pumping rate 3 gpm gph
 Type power unit ---
 Depth to bowls, cylinder, jet, etc., 343 ft. below land surface.
 Yield: --- gpm with --- ft. drawdown after --- hrs
 Boiler test --- gpm with 100 ft. drawdown after 7 hrs
 Artesian flow --- gpm Date Sept. 78
 Temperature of water ---
 Was a chemical analysis made? Yes No
 Did any strata contain undesirable water? Yes No
 Type of water? Potable sweet with strata 320-342

I hereby certify that this well was drilled by me (or under my supervision) and that each and all of the statements herein are true to the best of my knowledge and belief.
 W. H. Bush Estate (Type or Firm) Amarillo (City) Texas (State) (Zip)
 address 700 Valley Ave.
 Signed) Clifford Suggen (Name)
 C. A. Biggers, Drilling & Repair Serv. (Company Name)

OWNER Robert Jackson (Name) Address _____ (Street or RFD) (City) Amarillo (State) TX (Zip)
 LOCATION OF WELL: 7 miles in N.M. direction from _____ (Town)
 County Potter (N.E., S.W., etc.)

Legal description: Section No. 111 Block No. 9 Township _____
 Abstract No. _____ Survey Name Jimmy Neil (Bishop Estates)
 Distance and direction from two intersecting section or survey lines B.S.+F.
 See attached map.

4) PROPOSED USE (Check):
 Domestic Industrial Public Supply
 Reconditioning Irrigation Test Well Other

5) DRILLING METHOD (Check):
 Mud Rotary Air Hammer Driven Bored
 Air Rotary Cable Tool Jetted Other

6) BOREHOLE COMPLETION:
 Open Hole Straight Wall Undreamed
 Gravel Packed Other
 If Gravel Packed give interval... from 0 ft. to 230 ft.

8) CASING, BLANK PIPE, AND WELL SCREEN DATA:

From (ft.)	To (ft.)	Description and color of formation material	Dis. (in.)	New or Used	Steel, Plastic, etc. Part. Size, if commercial	Setting (ft.)	Gage Spring Screen
10	160	Surface Red Clay	5	N	Plastic	0	230
60	180	Sandstone w/ Clay Strips				120	220
80	200	Hard Sandstone & Red Clay					
80	220	Red & Brown Clay					
80	220	Red & Blue Clay w/ Sandstone Strips					
20	230	Red Clay					

9) WATER LEVEL:
 Static level 3-15-80 ft. below land surface Date 3-15-80
 Artesian flow _____ gam. Date _____

10) PACKERS:
 Type _____ Depth _____

11) TYPE PUMP:
 Turbine Jet Submersible Cylinder
 Other _____
 Depth to pump bowls, cylinder, jet, etc., _____ ft.

12) WELL TESTS:
 Type Test Pump Bailer Jetted Estimated
 Yield: 3 gpm with _____ ft. drawdown after _____ hr.

WATER QUALITY:
 (Use reverse side if necessary)
 Did you knowingly penetrate any strata which contained undesirable water? Yes No
 If yes, submit "REPORT OF UNDESIRABLE WATER"
 Type of water? _____ Depth of strata _____
 Was a chemical analysis made? Yes No

I hereby certify that this well was drilled by me (or under my supervision) and that each and all of the statements herein are true to the best of my knowledge and belief.

ME Lester J. Taylor (Type or Print) Water Well Driller Registration No. 1849
 ADDRESS Box 781 (Street or RFD) SURRAY (City) Texas (State) 79086 (Zip)
 (print) Lester J. Taylor (Water Well Driller) Les Taylor Drilling Co. (Company Name)

1) OWNER Martin Birken Field (Name) Address 3811 A Washington (Street or RD) Amarillo (City) Texas (State) 79003 (Zip)
 County Potter miles in 7 (N.E., S.W., etc.) direction from Amarillo (Town)

2) LOCATION OF WELL:
 Section No. 111 Block No. 9 Township
 Abstract No. Jimmy Neal Survey Name B.S.+F
 Distance and direction from two intersecting section or survey lines:
 See attached map.

3) TYPE OF WORK (Check):
 New Well Deepening Domestic Industrial Public Supply
 Reconditioning Plugging Irrigation Test Well Other

4) PROPOSED USE (Check):
 Domestic Industrial Public Supply
 Irrigation Test Well Other

5) DRILLING METHOD (Check):
 Mud Rotary Air Hammer Driven Bored
 Air Rotary Cable Tool Jetted Other

6) WELL LOG:
 Date drilled 3-11-80
 DIAMETER OF HOLE: Dis. (in.) From (ft.) To (ft.) Surface 180
 Description and color of formation material:
 0 100 Surface Red & Blue Clay w/ Sand & stone
 100 120 Sandstone w/ Blue Clay Strips
 120 140 Sandstone w/ Red & Blue Clay Strips
 140 160 Red & Blue Shale w/ sand & sandstone strips
 160 180 Red & Yellow Clay

7) BOREHOLE COMPLETION:
 Open Hole Straight Wall Underreamed
 Gravel Packed Other
 If Gravel Packed give interval . . . from 0 ft. to 180 ft.

8) CASING, BLANK PIPE, AND WELL SCREEN DATA:

New or Used	Dis. (in.)	Setting (ft.)	Casing	
			From	To
			0	180
			90	170

9) WATER LEVEL:
 Cemented from _____ ft. to _____ ft.
 Method used _____
 Cemented by _____ (Company or Individual)
 Static level 98 ft. below land surface Date 3-11-80
 Artesian flow _____ gpm.

10) PACKERS:

Type	Depth

11) TYPE PUMP:
 Turbine Jet Submersible Cylinder
 Other _____
 Depth to pump bowl, cylinder, jet, etc., _____ ft.

12) WELL TESTS:
 Type Test: Pump Boiler Jetted Estimated
 Yield: 12 gpm with _____ ft. drawdown after _____ hrs.

13) WATER QUALITY:
 (Use reverse side if necessary)
 Did you knowingly penetrate any strata which contained undesirable water? Yes No
 If yes, submit "REPORT OF UNDESIRABLE WATER"
 Type of water? _____ Depth of strata _____
 Was a chemical analysis made? Yes No

I hereby certify that this well was drilled by me (or under my supervision) and that each and all of the statements herein are true to the best of my knowledge and belief.

NAME Lester J. Taylor (Type or Print) Water Well Drillers Registration No. 1849
 ADDRESS Box (Type or Print) Subway (City) Texas (State) 79986
 Signed Lester J. Taylor (Signature) Las Taylor Drilling Co.

JAN 1 1973
For TDWR use only
Well No. 00-56-3D
Located on map. Yes
Received: JAC

OWNER: GARY ALEXANDER
Address: BOX 3502
City: AARMOCK TEX 79006
County: BASTER
miles in N.W. direction from AARMOCK (Town)

2) LOCATION OF WELL:
Section No. 114 Block No. 9
Survey Name: JIMMY EARLE HARIS
Distance and direction from two intersecting section or survey lines

3) TYPE OF WORK (Check):
 New Well
 Deepening
 Plugging
 Reconditioning
 Industrial
 Public Supply
 Irrigation
 Test Well
 Other

4) PROPOSED USE (Check):
 Domestic
 Air Hammer
 Bored
 Mud Rotary
 Cable Tool
 Driven
 Air Rotary
 Jetted
 Other

5) DRILLING METHOD (Check):
 Straight Well
 Underreamed
 Open Hole
 Gravel Packed
 Other
If Gravel Packed give interval... from 0 ft. to 177 ft.

6) WELL LOG:
Date drilled: 12-2-71
DIA. (in.) From (ft.) To (ft.)
9 3/4" Surface 177'
Description and color of formation material

7) BOREHOLE COMPLETION:
8) CASING, BLANK PIPE, AND WELL SCREEN DATA:
New or Used: Plastic, etc. Setting (ft.) From To
5' N PLASTIC 0 177
5' N PLASTIC AND SLATS 100 177

9) WATER LEVEL:
Static level: 85' ft. below land surface Date
Artesian flow: gm. Date

10) PACKERS:
Type Depth

11) TYPE PUMP:
 Turbin
 Jet
 Submersible
 Cylinder
 Other
Depth to pump bows, cylinder, jet, etc., ft.

12) WELL TESTS:
Type Test: Pump Bailer Jetted Estimated
Yield: 15 gpm with ft. drawdown after hrs.

WATER QUALITY:
Did you knowingly penetrate any strata which contained undesirable water? Yes No
If yes, submit "REPORT OF UNDESIRABLE WATER"
Type of water? Depth of strata?
Was a chemical analysis made? Yes No

I hereby certify that this well was drilled by me (or under my supervision) and that each and all of the statements herein are true to the best of my knowledge and belief.

NAME: GUY J. TAYLOR
Type or Print
Water Well Drillers Registration No. 1849

ADDRESS: BOX 984
City: SEWERY TEX 79086
Zip: 79086

Company Name: See Taylor Drilling Co.

See attach electric for chemical analysis and...

State of Texas
WATER WELL REPORT
 ATTENTION OWNER: Confidentiality Privilege Notice on Reverse Side

For TDWR use only
 Well No. 07-1030
 Located on map RS
 Received: CRS

and original copy by certified mail to the Texas Department of Water Resources, P.O. Box 13087, Austin, Texas 78711

OWNER: William A. Bowers (Name)
 Address: 2 Cambridge (Street or RFD) Amarillo, Tx. 79106 (City) (State) (Zip)
 County: Potter (County) 10 miles in W direction from Amarillo (Town) (N.E., S.W., etc.)

LOCATION OF WELL:
 Legal description:
 Section No. 114 Block No. 9 Township 856F
 Abstract No. _____ Survey Name _____
 Distance and direction from two intersecting section or survey lines
Unit 1, Track 80, Bishop Estates

1) TYPE OF WORK (Check):
 New Well Deepening Reconditioning Plugging Public Supply
 2) PROPOSED USE (Check):
 Domestic Industrial Irrigation Test Well Other

3) WATER QUALITY:
 Did you knowingly penetrate any strata which contained undesirable water? Yes No
 If yes, submit "REPORT OF UNDESIRABLE WATER"
 Type of water? _____ Depth of strata _____
 Was a chemical analysis made? Yes No

4) DRILLING METHOD (Check):
 Mud Rotary Air Hammer Driven Bored
 Air Rotary Cable Tool Jetted Other

5) BOREHOLE COMPLETION:
 Open Hole Straight Well Underreamed
 Gravel Packed Other _____
 If Gravel Packed give interval... from top ft. to bottom ft.

6) CASING, BLANK PIPE, AND WELL SCREEN DATA:

From (ft.)	To (ft.)	Description and color of formation material	New or Used	Steel, Plastic, etc. Screen Mfg., if commercial	Setting (ft.)	Gage Casing Screen
					From	To
0	3	top soil				
3	64	Caliche				
64	80	Clay & hard rock				
80	187	Red clay				
187	190	Blue clay				
190	196	Sandy clay & sandstone				
196	210	Blue clay				
210	231	Speckled caly w/ sandstone				
231	253	Hard gray rock				
253	318	Hard gray rock & clay				
318	332	Red clay & rock				
332	352	Sand & sandstone				
352		Yellow clay & rock				

7) WATER LEVEL:
 Static level 217 ft. below land surface Date 6/22/80
 Artesian flow _____ gpm. Date _____

8) TYPE PUMP:
 Turbine Jet Submersible Cylinder
 Other _____
 Depth to pump bowl, cylinder, jet, etc., _____ 320 _____ ft.

9) WELL TESTS:
 Type Test Pump Seiler Jetted Estimated
 Yield: 12 gpm with _____ 0 _____ ft. drawdown after _____ 3 _____ hrs.

10) PACKERS:
 Type _____ Depth _____

11) CEMENTING DATA:
 Cemented from _____ ft. to _____ ft.
 Method used _____
 Cemented by _____ (Company or Individual)

12) I HEREBY CERTIFY THAT THIS WELL WAS DRILLED BY ME (OR UNDER MY SUPERVISION) AND THAT EACH AND ALL OF THE STATEMENTS HEREIN ARE TRUE TO THE BEST OF MY KNOWLEDGE AND BELIEF.
 A.M.E. Charles Hookey (Type or Print) Water Well Driller Registration No. 674
 ADDRESS Box 17 (Street or P.O. Box) Miami (City) Tx. (State) 79059 (Zip)
 Signed Charles Hookey Miami Water Well Service

Well No. 01-36-36
 Located on map YCS
 Received: G.F.S.

WATER WELL REPORT
 ATTENTION OWNER: Confidentiality Privilege Notice on Reverse Side

OWNER John Portee (Name)
 Address Box 162 (Street or RFD)
 City Cactus (City) State Texas Zip 79013
 County Folsom (County) Direction from NW (Direction)
 Well Location Bishop Hills Estate (Town)

Block No. _____ Township _____
 Abstract No. _____ Survey Name _____
 Distance and direction from two intersecting section or survey lines _____

Legal description:
 Section No. _____
 Distance and direction from two intersecting section or survey lines _____

4) PROPOSED USE (Check):
 New Well Deepening Industrial Public Supply
 Reconditioning Plugging Irrigation Text Well Other _____

5) DRILLING METHOD (Check):
 Mud Rotary Air Hammer Driven Bored
 Air Rotary Cable Tool Jetted Other _____

6) DIAMETER OF HOLE:
 Dia. (in.) From (ft.) To (ft.)
 8 3/4 Surface 350

7) BOREHOLE COMPLETION:
 Open Hole Straight Well Underreamed
 Gravel Packed Other _____
 If Gravel Packed give interval . . . from 0 ft. to 350 ft.

8) CASING, BLANK PIPE, AND WELL SCREEN DATA:
 New or Used _____ Setting (ft.)
 Dia. (in.) _____ From _____ To _____
 Screen Mfg.: If commercial _____
 5 New Steel, Perf. 250 350

WATER QUALITY:
 Did you knowingly penetrate any strata which contained undesirable water? Yes No
 If yes, submit "REPORT OF UNDESIRABLE WATER"
 Type of water? _____ Depth of strata _____
 Was a chemical analysis made? Yes No
 (Use reverse side if necessary)

9) WATER LEVEL:
 Static level 250 ft. below land surface Date 3-19-81
 Artesian flow _____ gpm. Date _____

10) PACKERS:
 Type _____ Depth _____

11) TYPE PUMP:
 Turbine Jet Submersible Cylinder
 Other _____
 Depth to pump bowls, cylinder, jet, etc., 315 ft.

12) WELL TESTS:
 Type Test Pump Seiler Jetted Estimated
 Yield: 23 gpm with 25 ft. drawdown after 3 hrs.

CEMENTING DATA
 Cemented from _____ ft. to _____ ft.
 Method used _____
 Cemented by _____ (Company or Individual)

WELL LOG:
 Date drilled March 19, 1981

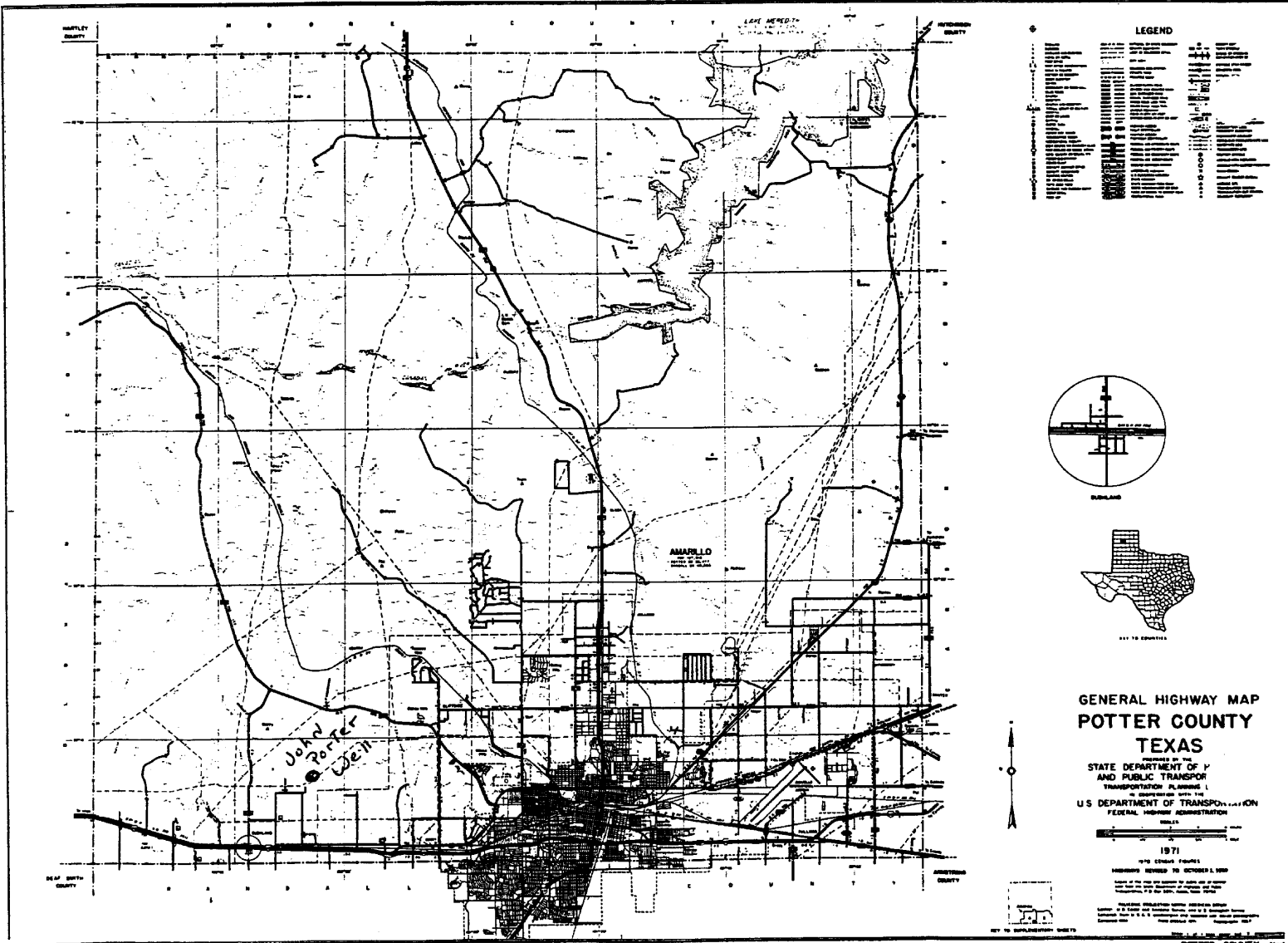
From (ft.) To (ft.) Description and color of formation material

0 28 Topsoil & Caliche
 28 48 Catclay & silt
 48 92 Rock & clay
 92 136 White Clay & Sand
 136 180 Sand & Gravel
 180 202 Sand & Gray clay
 202 246 Gray & white clay
 246 268 White, gray, & red clay
 268 290 Gray & red clay
 290 312 Red clay & gravel
 312 334 Red clay
 334 350 Red clay
 350 TD

AME Jimmy McGaskill (Type or Print)
 Water Well Drillers Registration No. 1771
 ADDRESS 8018 River Road (Street or RFD) Amarillo (City) Texas (State) 79108 (Zip)
 signed Jimmy McGaskill (Water Well Driller) A & A Drilling Company (Company Name)

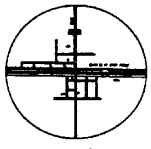
1981-36-36
 Dumas

John Porter's Well



LEGEND

[Symbol]	Interstate Highway
[Symbol]	State Highway
[Symbol]	County Road
[Symbol]	Local Road
[Symbol]	Waterway
[Symbol]	City
[Symbol]	County Seat
[Symbol]	Well
[Symbol]	Other



**GENERAL HIGHWAY MAP
POTTER COUNTY
TEXAS**

PREPARED BY THE
STATE DEPARTMENT OF
TRANSPORTATION PLANNING
AND PUBLIC TRANSPORT

UNDER THE
U.S. DEPARTMENT OF TRANSPORTATION
FEDERAL HIGHWAY ADMINISTRATION

1971

1:250,000 Scale

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OWNER: J. L. Bragg (Name) Address: 3534 Bragg (Street or RFD) direction from Garfield (City) Texas (State) 79109 (Zip)
 County: Potter miles in N.W. (N.E., S.W., etc.) direction from Garfield (Town) 110 (Town)

LEGAL DESCRIPTION: Section No. _____ Block No. _____ Township _____
 Abstract No. _____ Survey Name _____
 Distance and direction from two intersecting section or survey lines _____

1) TYPE OF WORK (Check):
 New Well Deepening Reconditioning Plugging Industrial Public Supply
 4) PROPOSED USE (Check):
 Domestic Irrigation Test Well Other _____

2) WELL LOG:
 Date drilled 4-14-81
 5) DRILLING METHOD (Check):
 Mud Rotary Air Hammer Driven Bored
 Air Rotary Cable Tool Jetted Other _____
 7) BOREHOLE COMPLETION:
 Open Hole Straight Well Underreamed
 Gravel Packed Other _____
 If Gravel Packed give interval... from Surface ft. to 350 ft.

8) CASING, BLANK PIPE, AND WELL SCREEN DATA:

From (ft.)	To (ft.)	Description and color of formation material	Dia. (in.)	New or Used	Steel, Plastic, etc. Screen Mgt., if commercial	Setting (ft.)	Gap Casing Screen
						From	To
0	15	Top soil + white + rock					
15	30	caliche + rock					
30	45	Red clay + rock	5	N	P.V.C.	Surface	350
45	60	Red clay + rock					40
60	75	" " " "					
75	90	Red clay + silts blue shale					
90	105	" " " "					
105	120	" " " "					
120	135	Red clay + rock					
135	150	" " " "					
150	165	Red + blue clay + silts rock					
165	180	" " " "					
180	195	Blue shale + silts lime stone					
195	210	" " " "					
210	225	" " " "					
225	240	Red + blue shale + silts limestone					
240	255	" " " "					
255	270	" " " "					
270	285	Yellow clay					
285	300	" " " "					
300	315	" " " "					
315	330	" " " "					
330	345	Yellow clay					

9) WATER LEVEL:
 Static level 135 ft. below land surface Date 4-14-81
 Artesian flow _____ gpm. Date _____
 Cemented from _____ ft. to _____ ft.
 Method used _____
 Cemented by _____ (Company or Individual)

10) PACKERS:
 Type _____ Depth _____

11) TYPE PUMP:
 Turbine Jet Submersible Cylinder
 Other _____
 Depth to pump bowls, cylinder, jet, etc., _____ ft.

12) WELL TESTS:
 Type Test: Pump Boiler Jetted Estimated
 Yield: 6 gpm with 90 ft. drawdown after 2 hrs.

3) WATER QUALITY:
 (Use reverse side if necessary)
 Did you knowingly penetrate any strata which contained undesirable water? Yes No
 If yes, submit "REPORT OF UNDESIRABLE WATER"
 Type of water: _____ Depth of strata _____
 Was a chemical analysis made? Yes No

I hereby certify that this well was drilled by me (or under my supervision) and that each and all of the statements herein are true to the best of my knowledge and belief.
 NAME: Joe Allen (Type or Print) Water Well Drillers Registration No. 2053
 ADDRESS: Rt 5 Box 22 E (Street or RFD) Garfield (City) Texas (State) 79118 (Zip)
 signed: Joe Allen (Water Well Driller) T & A Drilling Co. (Company Name)

1) OWNER LEWIS WHEATLEY (Name) Address 103 PATON (City) AMARILLO (State) (Zip)
 2) LOCATION OF WELL: County ROTTER (Name) 6 miles in N.W. direction from AMARILLO (Town)
 (N.E., S.W., etc.)

Driller must complete the legal description to the right
 (Section and direction from two intersecting sec-
 tions of the General Land Office Survey, or from
 well on an official Course or Half-Section Course
 General Highway Map and attach the map to this form.)

Legal description: Section No. _____ Township _____
 Abstract No. _____ Survey Name _____
 Distance and direction from two intersecting section or survey lines _____

See attached map. 07-S&36

3) TYPE OF WORK (Check):
 New Well Deepening
 Reconditioning Plugging

4) PROPOSED USE (Check):
 Domestic Industrial Public Supply
 Irrigation Test Well Other _____

5) DRILLING METHOD (Check):
 Mud Rotary Air Hammer Driven Bond
 Air Rotary Cable Tool Jetted Other _____

6) WELL LOG:
 Date drilled 12-11-84
 Dia. (in.) From (ft.) To (ft.)
8 3/4" Surface 290

7) BOREHOLE COMPLETION:
 Open Hole Straight Wall Underreamed
 Gravel Packed Other _____
 If Gravel Packed give interval . . . from 10 ft. to 290 ft.

8) CASING, BLANK PIPE, AND WELL SCREEN DATA:

From (ft.)	To (ft.)	Description and color of formation material	Dia. (in.)	New or Used	Steel, Plastic, etc. Perf., Slotted, etc. Screen Mfg., if commercial	Setting (ft.) From To	Gap Casing Screen
0-15	Top Soil + Gravel						
15-30	Caliche w/ Brown Shale + Sand Clay				PVC Plastic	0-190	
30-40	Brown Shale + Sand Clay				PVC	190-280	
40-120	Sand Clay w/ Red + Gray Shale						
120-150	Hard Gray Shale w/ Red + Gray Gravel						

9) WATER LEVEL:
 Static level 130 ft. below land surface Date 12-13-84
 Artesian flow _____ gpm. Date _____

10) PACKERS:
 Type _____ Depth _____

11) TYPE PUMP:
 Turbine Jet Submersible Cylinder
 Other _____
 Depth to pump bowl, cylinder, jet, etc., 260 ft.

12) WELL TESTS:
 Type Test: Pump Bailor Jetted Estimated
 Yield: 12 gpm with 280 ft. drawdown after 2 hrs.

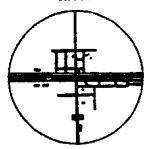
13) WATER QUALITY:
 Did you knowingly penetrate any strata which contained undesirable water? Yes No
 If yes, submit "REPORT OF UNDESIRABLE WATER"
 Type of water? FRESH Depth of strata 160'
 Was a chemical analysis made? Yes No

I hereby certify that this well was drilled by me (or under my supervision) and that each and all of the statements herein are true to the best of my knowledge and belief.

COMPANY NAME A-1 BAPTIST WELL SERV. Water Well Driller's License No. 2119

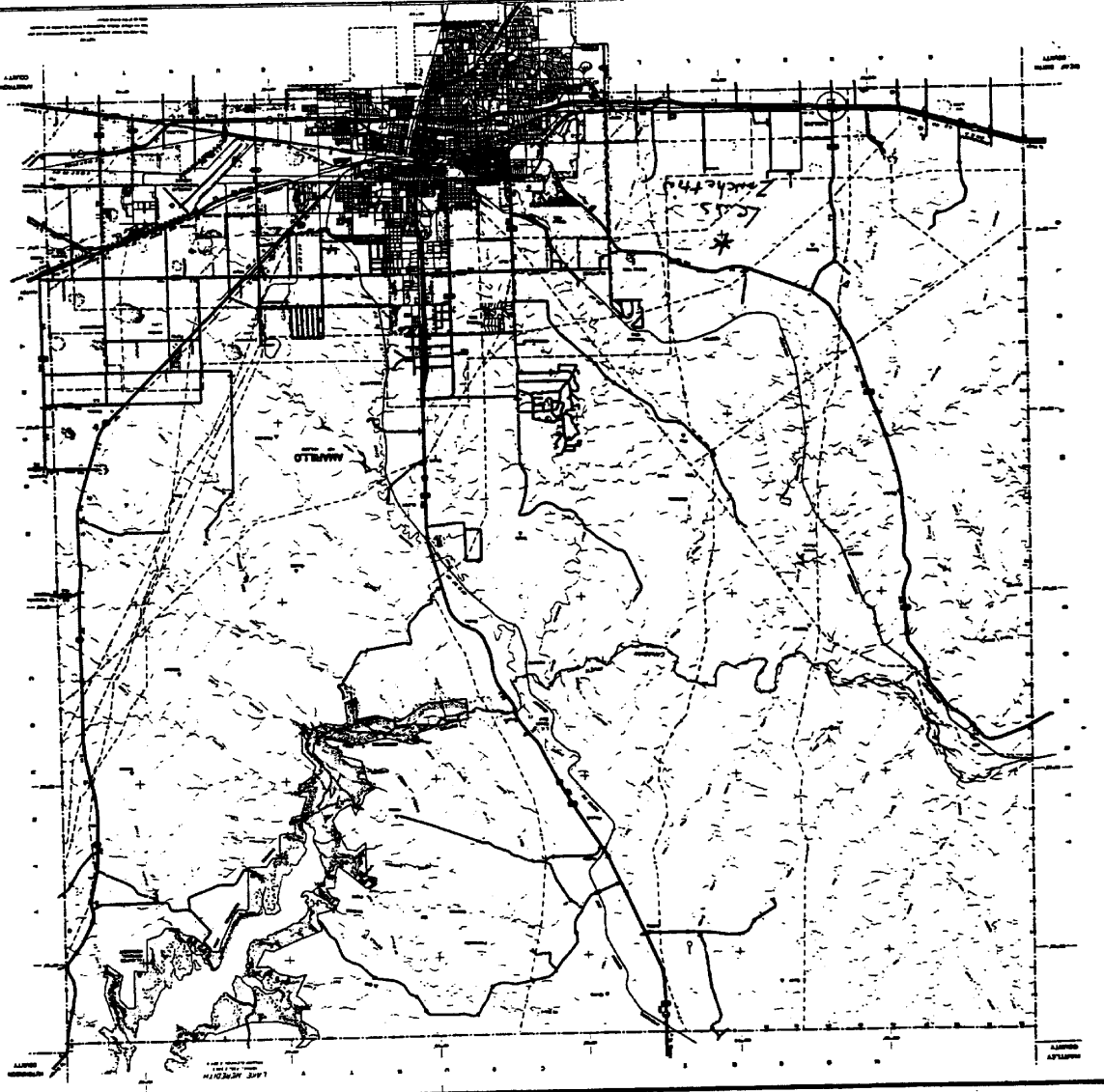
ADDRESS RT 2 Box 54-6 (Type or Print) AMARILLO TX
 (Street or RFD) (City) (State) (Zip)
 Signed) Andy D. Powell (Licensed Water Well Driller) (Signed) Ray E. Bell (Registered Driller - Licensed)
 For TDWR use only: Well No. 0256-36

POTTER COUNTY MAP
TEXAS
STATE DEPARTMENT OF HIGHWAYS
AND PUBLIC TRANSPORTATION
TRANSPORTATION PLANNING DIVISION
U.S. DEPARTMENT OF TRANSPORTATION
FEDERAL HIGHWAY ADMINISTRATION
1971



LEGEND

—	Interstate Highway
—	State Highway
—	County Road
—	Other Road
—	Proposed Road
—	Waterway
—	Boundary
—	City
—	Township
—	Section
—	Other



1) OWNER Chuck Aley (Name) Address 2807 S Spring (City) Amario TX (State) 7910 (Zip)
 2) LOCATION OF WELL: Potter (Name) 6 miles in N.W. (Street or RFD) direction from Amario (Town)
 County Potter (N.E., S.W., etc.) (Town)

Driller must complete the legal description to the right with distance and direction from two intersecting section or survey lines, or the must locate and identify the well on an official Quarter- or Half-Section Texas County General Highway Map and attach the map to this form.
 Legal description: Section No. _____ Block No. _____ Township _____
 Abstract No. _____ Survey Name _____
 Distance and direction from two intersecting section or survey lines _____

3) TYPE OF WORK (Check):
 New Well Deepening
 Reconditioning Plugging
 Proposed Use (Check):
 Domestic Industrial Public Supply
 Irrigation Test Well Other _____

6) WELL LOG:
 Date drilled 11-2-84
 DIAMETER OF HOLE
 From (ft.) _____ To (ft.) _____
 Dis. (in.) _____ From (ft.) _____ To (ft.) _____
 Surface _____ 350

7) BOREHOLE COMPLETION:
 Open Hole Straight Well Undrilled
 Gravel Packed Other _____
 If Gravel Packed give interval ... from 0 ft. to 350 ft.

8) CASING, BLANK PIPE, AND WELL SCREEN DATA:

From (ft.)	To (ft.)	Description and color of formation (meter)	Dia. (in.)	New or Used	Steel, Plastic, etc. Perf., Slotted, etc. Screen Mfg., if commercial	Setting (ft.) From To	Gate Closing Screen
0-15		Top soil & caliche					
15-30		Sandy Clay w/ caliche & fine sand	4 1/2" N		Plastic	0	265
30-60		Fine sand w/ cemented sand & siltstone	4 1/2" N		P.V.C. Rerouted	150	350
60-145		Fine to med sand w/ cemented sand & siltstone					
105-165		Med. to coarse sand w/ siltstone					
165-210		Med to coarse sand w/ siltstone & red shale					
210-285		Red shale w/ siltstone & sandstone & red clay					
285-350		Red shale w/ siltstone & red w/ gray clay					

9) WATER LEVEL:
 Cased from 0 ft. to 10' ft.
 Method used A-1 Rammer Well Service
 Cemented by _____ (Company or Individual)

10) PACKERS:
 Type _____ Depth _____

11) TYPE PUMP:
 Turbine Jet Submersible Cylinder
 Other _____
 Depth to pump bowl, cylinder, jet, etc. 340' ft.

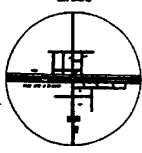
12) WELL TESTS:
 Type Test: Pump Bailor Jetted Estimated
 Yield: 10 gpm with 140 ft. drawdown after 2 hrs.

13) WATER QUALITY:
 Did you knowingly penetrate any strata which contained undrinkable water? Yes No
 If yes, submit "REPORT OF UNDESIRABLE WATER"
 Type of water? EC55 Depth of strata 200' ±
 Was a chemical analysis made? Yes No

I hereby certify that this well was drilled by me (or under my supervision) and that each and all of the statements herein are true to the best of my knowledge and belief.

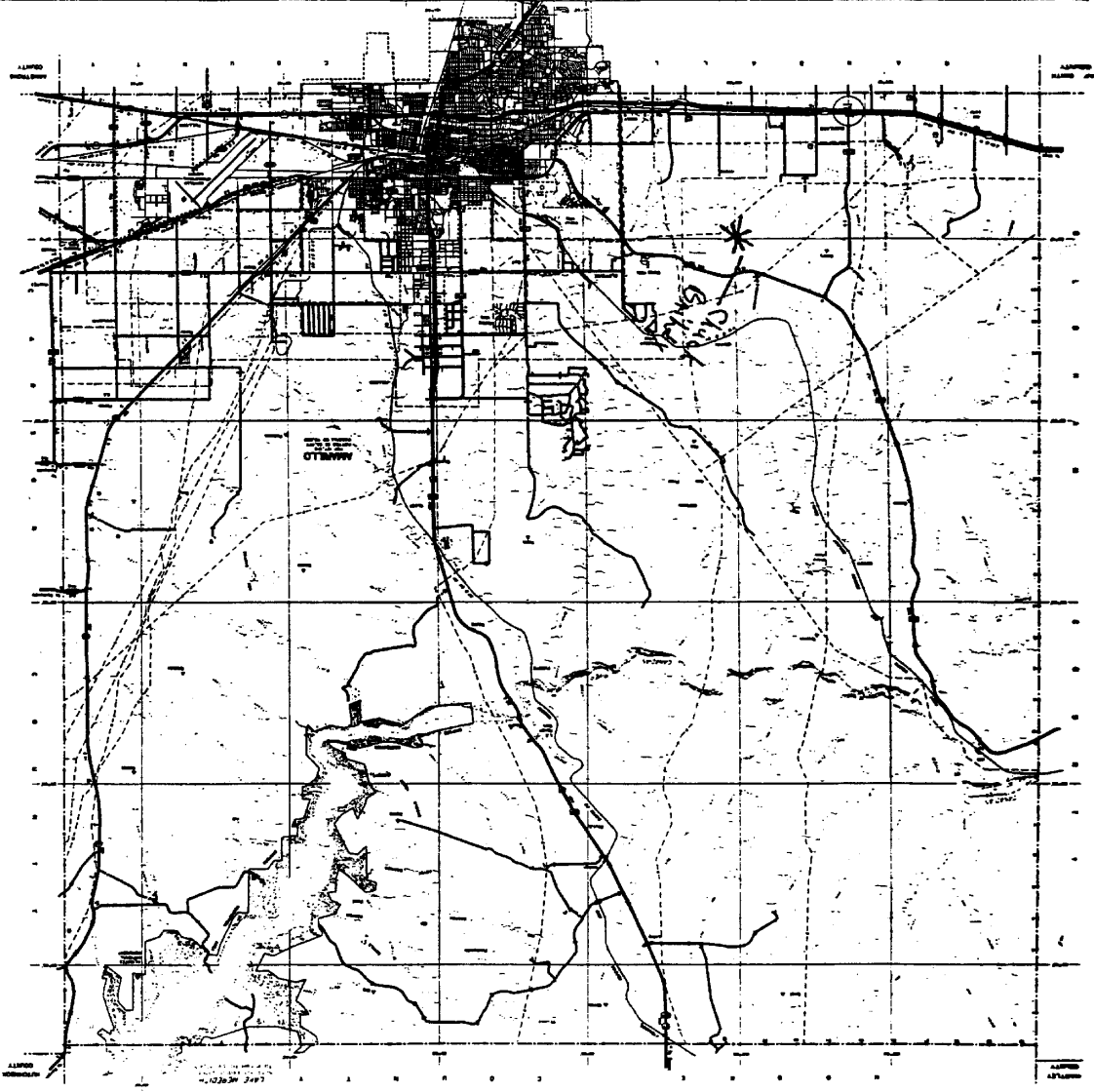
COMPANY NAME A-1 Rammer Well Service Water Well Driller's License No. 2119
 ADDRESS Rt 3 Box 54-G (Type of Firm) Amario (City) TX. (State) 7910 (Zip)
 (Signed) Ray D Bork (Signed) Ray D Bork (Registered Driller)
 Please attach electric log, chemical analysis, and other pertinent information, if available.

GENERAL HIGHWAY MAP
 POTTER COUNTY
 TEXAS
 STATE DEPARTMENT OF HIGHWAYS
 AND PUBLIC TRANSPORTATION
 TRANSPORTATION PLANNING DIVISION
 U.S. DEPARTMENT OF TRANSPORTATION
 FEDERAL HIGHWAY ADMINISTRATION
 1971
 THIS MAP WAS PREPARED BY THE
 STATE DEPARTMENT OF HIGHWAYS
 AND PUBLIC TRANSPORTATION
 TRANSPORTATION PLANNING DIVISION
 IN COOPERATION WITH THE
 U.S. DEPARTMENT OF TRANSPORTATION
 FEDERAL HIGHWAY ADMINISTRATION
 IN ACCORDANCE WITH THE
 FEDERAL AID TO HIGHWAY ACT
 OF OCTOBER 3, 1966



LEGEND

	Interstate Highway
	Federal Highway
	State Highway
	County Road
	Unimproved Road
	Railroad
	Waterway
	Airport
	City
	Town
	Village
	School
	Church
	Cemetery
	Public Building
	Industrial Building
	Residential Building
	Power Line
	Telephone Line
	Gas Line
	Water Line
	Sewer Line
	Elevation Contour
	Spot Elevation
	Section Corner
	Township and Range Corner
	Section Number
	Township and Range Number



OWNER: DAY & OR (Name) Address: 6300 B. Todd Lane Lakewood, Texas 79013 (City) (State) (Zip)
 LOCATION OF WELL: Potter (Street or RFD) direction from AAW-110 (Town)
 County: Potter (N.E., S.W., etc.)

Driller must complete the legal description to the right
 Legal description: Section No. 113 Block No. 9 Township _____
 Abstract No. _____ Survey Name B & P
 Distance and direction from two intersecting section or survey lines _____

TYPE OF WORK (Check):
 New Well Deepening Reconditioning Plugging
 PROPOSED USE (Check):
 Domestic Industrial Public Supply
 Irrigation Test Well Other _____
 See attached map.

WELL LOG:
 Date drilled: 1-6-85
 DIAMETER OF HOLE:
 Dia. (in.) From (ft.) To (ft.)
8 3/4 Surface 295

From (ft.)	To (ft.)	Description and color of formation material	8) CASING, BLANK PIPE, AND WELL SCREEN DATA:
0	115	SUBSURFACE CALIBER GRAY & SAND	
115	155	Red clay & gravel	
155	195	Red clay	
195	235	Red clay w/ sandstone strata	
235	275	Red & green clay w/ sandstone strata	
275	295	Blue clay	

9) CEMENTING DATA (Rule 319.44(b))
 Cemented from: Pipe 1 ft. to 15 ft.
 Method used: Hand-Mixed
 Cemented by: Lee Taylor Drilling

10) SURFACE COMPLETION
 Specified surface slab installed (Rule 319.44(c))
 Piles Adapter Used (Rule 319.44(d))
 Approved Alternative Procedure Used (Rule 319.71)

11) WATER LEVEL:
 Static level: _____ ft. below land surface Date _____
 Artesian flow: _____ gpm. Date _____
 PACKERS: _____ Type _____ Depth _____

DEPT. OF WATER RESOURCES
 REC-141985
 13) TYPE PUMP:
 Turbine Jet Submersible Cylinder
 Other _____
 Depth to pump bowl, cylinder, jet, etc.: _____ ft.

14) WELL TESTS:
 Type Test: Pump Bailor Jetted Estimated
 Yield: 2-5 gpm with _____ ft. drawdown after _____ hrs.
 Was a chemical analysis made? Yes No

WATER QUALITY:
 Did you knowingly penetrate any strata which contained undesirable water? Yes No
 If yes, submit "REPORT OF UNDESIRABLE WATER"
 Type of water? _____ Depth of strata? _____
 Was a chemical analysis made? Yes No

COMPANY NAME: LEE TAYLOR DRILLING Water Well Driller's License No. 2366
 ADDRESS: P.O. Box 781, Survey, Texas 79086
 (Street or RFD) (City) (State) (Zip)
 Signed: Lee Taylor (Registered Driller Trainee) Well No. 07-51634
 Date: 1/6/85

OWNER Day and Company Address 6309 S. Indiana Lubbock TX 79413
 (City or RFD) (City) (State) (Zip)
 LOCATION OF WELL Pitter 6 miles in W. N. W. direction from Amosillo (Town)
 County Pitter (N.E., S.W., sec)

Driller must complete the legal description to the right with distance and direction from two intersecting sections or survey lines, or he must locate and identify the well on an official Quarter- or Half-Scale Texas County General Highway Map and attach the map to this form.

Legal description: Section No. _____ Township _____
 Block No. _____
 Abstract No. _____ Survey Name _____
 Distance and direction from two intersecting section or survey lines _____

See attached map: W-8-8-01-56-31

1) TYPE OF WORK (Check):
 New Well Deepening Reconditioning Plugging

4) PROPOSED USE (Check):
 Domestic Industrial Public Supply Irrigation Test Well Other _____

5) DRILLING METHOD (Check):
 Mud Rotary Air Hammer Driven Bored Air Rotary Cable Tool Jetted Other _____

WELL LOG:
 DIAMETER OF HOLE
 Dia. (in.) From (ft.) To (ft.)
8 3/4 Surface 300
 Date drilled 3/14/85

7) BOREHOLE COMPLETION:
 Open Hole Straight Wall Undrained
 Gravel Packed Other _____
 If Gravel Packed give interval . . . from 10 ft. to 300 ft.

8) CASINO, BLANK PIPE, AND WELL SCREEN DATA:

Dia. (in.)	New or Used	Steel, Plastic, etc. Perf., Slotted, etc. Screen Mfg., if commercial	Setting (ft.)		Gage Casing Screen
			From	To	
<u>4 1/2</u>	<u>N</u>	<u>Plastic</u>	<u>0</u>	<u>185</u>	
<u>4 1/2</u>	<u>N</u>	<u>RUS. Reinforced</u>	<u>180</u>	<u>300</u>	

9) WATER LEVEL:
 Static level 170 ft. below land surface Date 3/15/85
 Artesian flow _____ gpm. Date _____

10) PACKERS:
 Type _____ Depth _____

11) TYPE PUMP:
 Turbine Jet Submersible Cylinder
 Depth to pump bowl, cylinder, jet, etc., 240 ft.

3) WATER QUALITY: (Use reverse side if necessary) DEF. OF WATER RESOURCES
 Did you knowingly penetrate any strata which contained underground water? Yes No
 If yes, submit "REPORT OF UNDERGROUND WATER" Type of water? fresh Depth of strata _____
 Was a chemical analysis made? Yes No

I hereby certify that this well was drilled by me (or under my supervision) and that each and all of the statements herein are true to the best of my knowledge and belief.

COMPANY NAME A-1 Pump & Well Services Water Well Driller's License No. 2119
 (Type & Print)
 ADDRESS Pt. Box 54-G Amosillo TX 79101
 (City or RFD) (City) (State) (Zip)
 (Signed) Wally H. Hanks (Registered Driller) Wally H. Hanks (Signature)
 (Signed) Wally H. Hanks (Registered Driller) Wally H. Hanks (Signature)
 For TDWP 07-56-31 Well No. 07-56-31 Located on map X65 C.F.S.

LAREN
 (806) 622-0852

1) OWNER DAVE Emery Address 6309 Bridlewood Lubbock Tx. 79413
 County Petro City W.N.W. direction from Aberville (Town)
 (N.E., S.W., etc.)

Driller must complete the legal description to the right with distance and direction from two intersecting sections or survey lines, or he must locate and identify the well on an official Quarter- or Half-Scale Texas County General Highway Map and attach the map to this form.

Legal description:
 Section No. _____ Block No. _____ Township _____
 Abstract No. _____ Survey Name _____
 Distance and direction from two intersecting sections or survey lines _____

3) TYPE OF WORK (check):
 New Well Deepening
 Reconditioning Plugging

4) PROPOSED USE (check):
 Domestic Industrial Public Supply
 Irrigation Test Well Other _____

5) DRILLING METHOD (check):
 Mud Rotary Air Hammer Driven Bond
 Air Rotary Cable Tool Jetted Other _____

6) WELL LOG:
 Date drilled 3/12/85

From (ft.)	To (ft.)	Description and color of formation material
0-15		Top soil w/ sandy caliche
5-60		Caliche w/ caliche east
0-75		Caliche w/ sandy clay
5-105		Mod. to coarse sand w/ sandstone
05-120		Fine to med sand w/ cemented sand
20-135		Fine sand
35-210		Fine to med sand w/ gts. cemented sand
40-255		Fine to med sand w/ fine gravel
65-270		Gray sandy clay w/ sand stripes
70-285		Red wgray clay w/ sandstone & gravel sand
85-300		Red to gray clay w/ sandstone & gravel sand
300		Red clay

7) BOREHOLE COMPLETION:
 Open Hole Straight Wall Undrilled
 Gravel Packed Other _____
 If Gravel Packed give interval ... from 10 ft. to 300 ft.

8) CASING, BLANK PIPE, AND WELL SCREEN DATA:

Dia. (in.)	New or Used	Steel, Plastic, etc. Perf., Slotted, etc. Screen Mfg., if commercial	Setting (ft.) From To	Gravel Packing Screen
4 1/2"	N	Plastic	0	180'
4 1/2"	N	RVC. Perforated	180'	300'

9) WATER LEVEL:
 Static level 170 ft. below land surface Date 3/14/85
 Artesian flow _____ gm. Date _____

CEMENTING DATA
 Cemented from 0 ft. to 10 ft.
 Method used _____
 Cemented by A-1 Pump & Well Service (Company or Individual)

10) PACKERS:
 Type _____ Depth _____

11) TYPE PUMP:
 Turbine Jet Submersible Cylinder
 Depth to pump bowl, cylinder, jet, etc., 246' ft.

12) WELL TESTS:
 Type Test: Pump Baller Jetted Estimated
 Yield: 12 gpm with 16' ft. drawdown after 2 hrs.

13) WATER QUALITY:
 Did you knowingly penetrate any areas which contain hazardous substances or water? Yes No
 If yes, submit "REPORT OF UNDESIRABLE WATER" 130' ft.
 Type of water? SEAS Depth of strata _____
 Was a chemical analysis made? Yes No

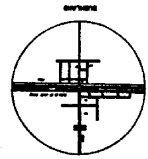
I hereby certify that this well was drilled by me (or under my supervision) and that each and all of the statements herein are true to the best of my knowledge and belief.

COMPANY NAME A-1 Pump & Well Services Water Well Driller's License No. 2119
 (Type or Print)
 ADDRESS Pt. A Box 54-G Aberville TX 79101
 (City) (State) (Zip)
 (Signed) Andy D. Bostick (Signed) Andy D. Bostick
 (Licensed Water Well Driller) (Registered Driller)
 For TDWR use only
 Well No. 2119-36-31
 Located on map 233 C.F. 5

GENERAL HIGHWAY MAP
1971

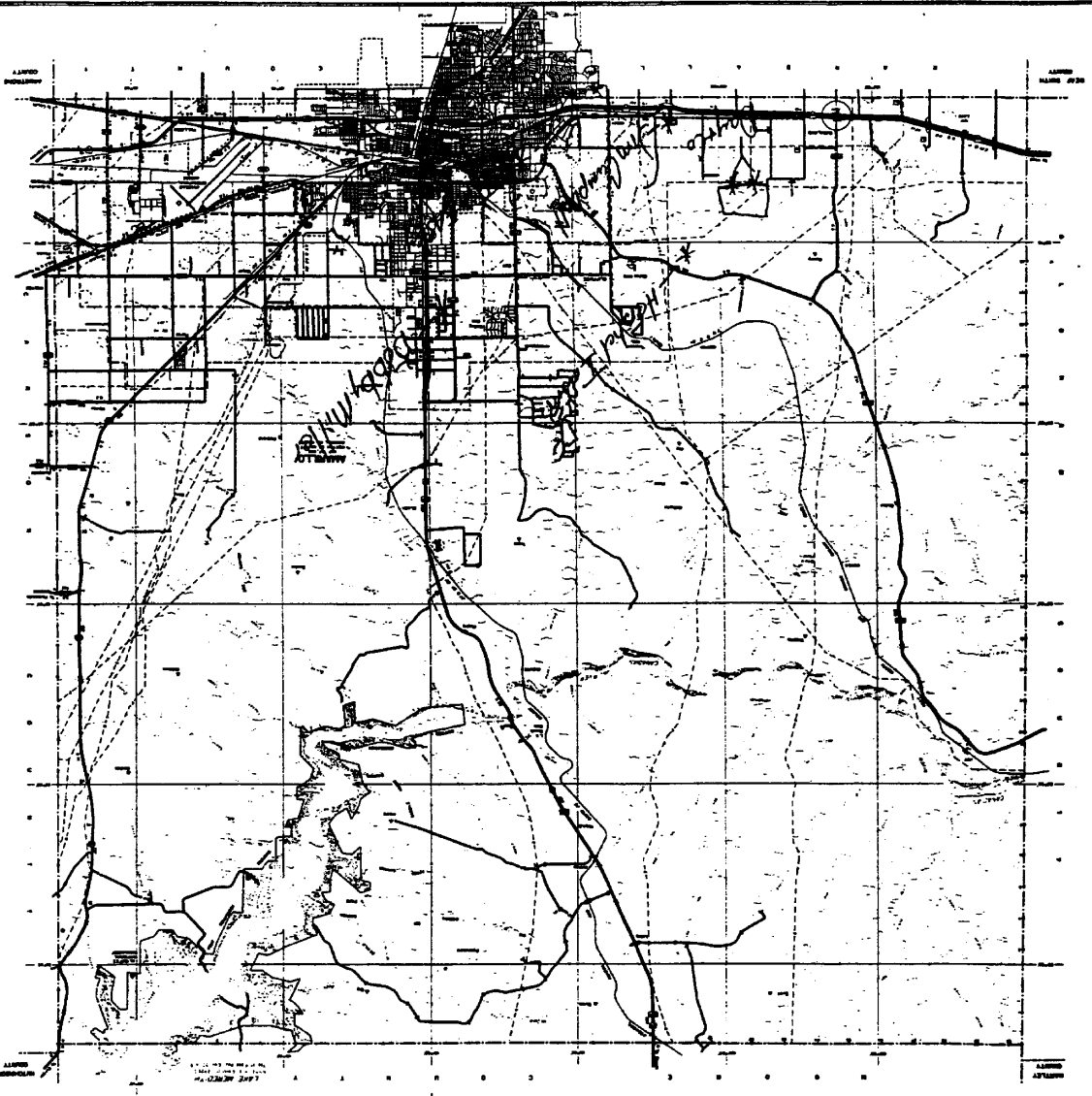
STATE DEPARTMENT OF HIGHWAY AND PUBLIC TRANSPORTATION
TRANSPORTATION PLANNING DIVISION
U.S. DEPARTMENT OF TRANSPORTATION
FEDERAL HIGHWAY ADMINISTRATION

GENERAL HIGHWAY MAP
POTTER COUNTY
TEXAS



LEGEND

—	Interstate Highway
—	State Highway
—	County Road
—	Other Road
—	Waterway
—	Boundary
—	Settlement
—	Other



TEXAS WATER DEVELOPMENT BOARD
WELL SCHEDULE

Aquifer: _____ Field No. _____ State Well No. 111 07-56301
Owner's Well No. _____ County Potter

1. Location: SW 1/4 SW 1/4 Sec. 126, Block 9, Survey B.S. & E.

2. Owner: J.W. Hill Address: _____
Tenant: _____ Address: _____
Driller: _____ Address: _____

3. Elevation of LSD is 3816 ft. above mal, determined by 7 1/2 min. topo

4. Drilled: 19 ft., Dug, Cable Tool, Rotary,
5. Depth: Rept. _____ ft. Meas. _____ ft.

6. Completion: Open Hole, Straight Wall, Underreamed, Gravel Packed

7. Pump: Mfg. Pomona Type Turbine
No. Stages _____, Bools Diam. _____ in., Setting _____ ft.
Column Diam. 6 in., Length Tailpipe _____ ft.

8. Motor: Fuel Elec. Make & Model _____ MP. SDGH

9. Yield: Flow _____ gpm, Pump _____ gpm, Meas., Rept., Est. _____

10. Performance Test: Date _____ Length of Test _____ Made by _____
Static Level _____ ft. Pumping Level _____ ft. Drawdown _____ ft.
Production _____ gpm Specific Capacity _____ gpm/ft.

11. Water Level: _____ ft. rept. _____ 19 above _____ which is _____ ft. above surface.
_____ ft. meas. _____ below _____ which is _____ ft. below surface.
_____ ft. rept. _____ 19 above _____ which is _____ ft. above surface.
_____ ft. meas. _____ below _____ which is _____ ft. below surface.
_____ ft. rept. _____ 19 above _____ which is _____ ft. above surface.
_____ ft. meas. _____ below _____ which is _____ ft. below surface.

12. Use: Dom., Stock, Public Supply, Ind., Irr. Waterflooding, Observation, Not Used.

13. Quality: (Remarks on taste, odor, color, etc.) _____
Temp. _____ °F, Date sampled for analysis _____ Laboratory _____
Temp. _____ °F, Date sampled for analysis _____ Laboratory _____
Temp. _____ °F, Date sampled for analysis _____ Laboratory _____

14. Other data available as circled: Driller's Log, Radioactivity Log, Electric Log, Formation Samples, Pumping Test,

15. Record by: D. Müller Date 3-7-1972
Source of Data Obs

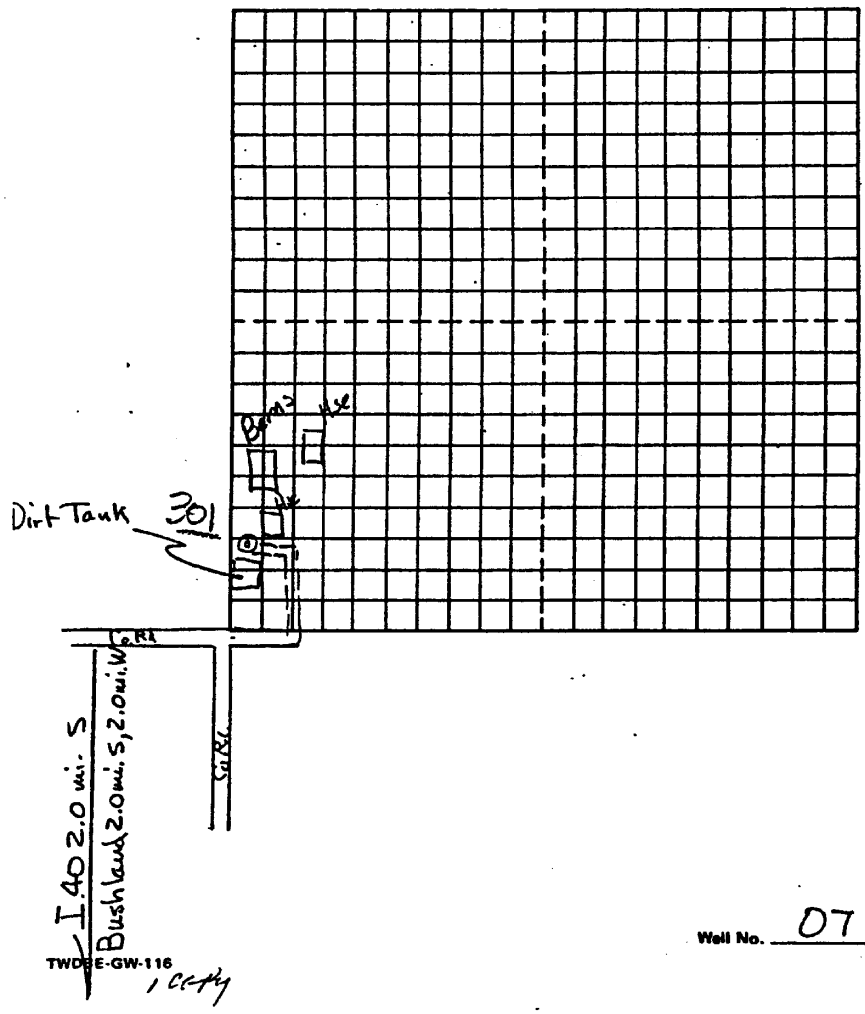
16. Remarks: Access E-side pump base

CASINO & BLANK PIPE			
Cemented From		ft. to	
Diam. (in.)	Type	Setting, ft.	
		From	To

WELL SCREEN			
Screen Openings			
Diam. (in.)	Type	Setting, ft.	
		From	To

WATER WELL LOCATION SKETCH
TEXAS WATER DEVELOPMENT BOARD
GROUND WATER DIVISION

Section 126 in Block 9
Potter County
2 1/2-minute Quadrangle 3 in
7 1/2-minute Quadrangle 56
Sketch by D. Müller Date 3-7-72



Well No. 07 . 56 . 301

TEXAS WATER DEVELOPMENT BOARD
WELL SCHEDULE

Permit No. 252

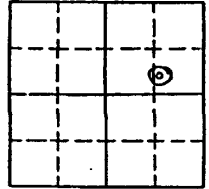
Aquifer _____

Field No. _____

State Well No. 07-56-302
County Potter

Owner's Well No. _____

1. Location: SE 1/4, NE 1/4 Sec. 127, Block 9 Survey BS & F



2. Owner: Caroline B. Emery Address: _____

Tenant: _____ Address: _____

Driller: W.G. Gayne Address: Hainview, Texas

3. Elevation of LSD is 3801 ft. above mal, determined by 7 1/2 min topo.

4. Drilled: 5-15-69, Dug, Cable Tool, Rotary

5. Depth: Rept. 317 ft. Meas. _____ ft.

6. Completion: Open Hole, Straight Wall, Underreamed, Gravel Packed

7. Pump: Mfr. Peerless Type Turbine

No. Stages 7, Bore Dia. 10 in., Setting 270 ft.

Column Dia. 6 in., Length Tailpipe _____ ft.

8. Motor: Fuel NG Make & Model Minn. Moline HP. 406H

9. Yield: Flow _____ gpm, Pump 500 gpm, Meas. Rept., Est. _____

10. Performance Test: Date 5-15-69 Length of Test _____ Made by DRILLER

Static Level 190 ft. Pumping Level 255 ft. Drawdown _____ ft.

Production 500 gpm Specific Capacity _____ gpm/ft.

11. Water Level: 190 ft. Rept. 5-15-69 above _____ ft. above surface.
 _____ ft. rept. _____ below _____ ft. below surface.
 _____ ft. meas. _____ above _____ ft. above surface.
 _____ ft. rept. _____ below _____ ft. below surface.
 _____ ft. meas. _____ above _____ ft. above surface.
 _____ ft. rept. _____ below _____ ft. below surface.
 _____ ft. meas. _____ above _____ ft. above surface.

12. Use: Dom., Stock, Public Supply, Ind., Irr. Waterflooding, Observation, Not Used,

13. Quality: (Remarks on taste, odor, color, etc.) _____

Temp. _____ °F, Date sampled for analysis _____ Laboratory _____

Temp. _____ °F, Date sampled for analysis _____ Laboratory _____

Temp. _____ °F, Date sampled for analysis _____ Laboratory _____

14. Other data available as circled: Driller's Log, Radioactivity Log, Electric Log,

Formation Samples, Pumping Test,

15. Record by: D. Miller Date 3-8-1972

Source of Data DL, Tenant

16. Remarks: Access W-side pump base
Base of Ogallala 280' (LW)

CASINO & BLANK PIPE			
Diam. (in.)	Type	Setting, ft.	
		from	to
16		0	317

WELL SCREEN			
Screen Openings			
Diam. (in.)	Type	Setting, ft.	
		from	to
16	Perf.	290	317

Quadruplicate--Applicant's Copy

High Plains Underground Water Conservation District No. 1

REGISTRATION and LOG OF WELL

INSTRUCTIONS: Fill out in quadruplet. Submit all copies to County Committee for recommendation. (PLEASE TYPE OR PRINT)

FOR USE OF COMMITTEEMEN	
Field Well No.	253
Date Received	4-29-69
Permit Size	Maximum
of Pump	6 in Yield 600 GPM

1. Land Owner Caroline B. Finney Address P.O. Box 1220 Amarillo, Texas

2. Well located 1 miles N, 2 miles E, _____ miles S, _____ miles W of town of Bushland

3. County Potter Labor _____ League _____ Abstract No. _____

4. NW¼ NE¼ SW¼ SE¼ Section 127 Block 9 Survey BS & F

MARK OUT THOSE THAT DO NOT APPLY

670 N
400 E

DRILLER'S LOG OF WELL

Method of Drilling: Rotary _____ Spudder _____ Diameter of Well: 18 inches.

MARK OUT ONE THAT DOES NOT APPLY

FROM (FEET)	TO (FEET)	DESCRIPTION OF FORMATION MATERIAL	FROM (FEET)	TO (FEET)	DESCRIPTION OF FORMATION MATERIAL
0	12	Soil & Caliche			
12	60	Sdy Cly			
60	90	Red Cly			
90	98	Cap Rk			
98	150	Fn Sl (Tight)			
150	170	Brkn Rk			
170	225	Tight Sl & Rk Strks			
225	265	Fn Sl			
265	280	Coarse Sl.			
280	317	Red Bed			

REMARKS:

I hereby certify that this well was drilled by me (or under my supervision), and that each and all of the statements herein are true to the best of my knowledge and belief.

Driller W.G. Grayne Address Plainville, Texas Date Drilled 5-15-1969

DESCRIPTION OF WELL AND PRODUCTION EQUIPMENT

(This Does Not Mean Testing or Development Pump)

6. Casing: new, used, gas line, or shop made. Diameter 16 in Total casing length 288 ft.

7. Casing perforations: from 280 ft. to 317 ft. Size 3/16 X 10" Number of rows 6

8. Pump Column: Size 6 in. Column, shaft length 270 ft. Suction pipe size 6 in. Suction pipe length 3 ft.

9. Pump bowls: Size 10 Number of stages 7 Pump discharge pipe: Size 6 in.

10. Depth to water level 190 ft. Pump yield 560 GPM. Pumping level: 255 ft.

11. Power Unit: Electrical, Natural Gas, Butane, Other _____ Horsepower 60

Signature _____ TITLE _____ ADDRESS _____

LANDOWNER OR AGENT

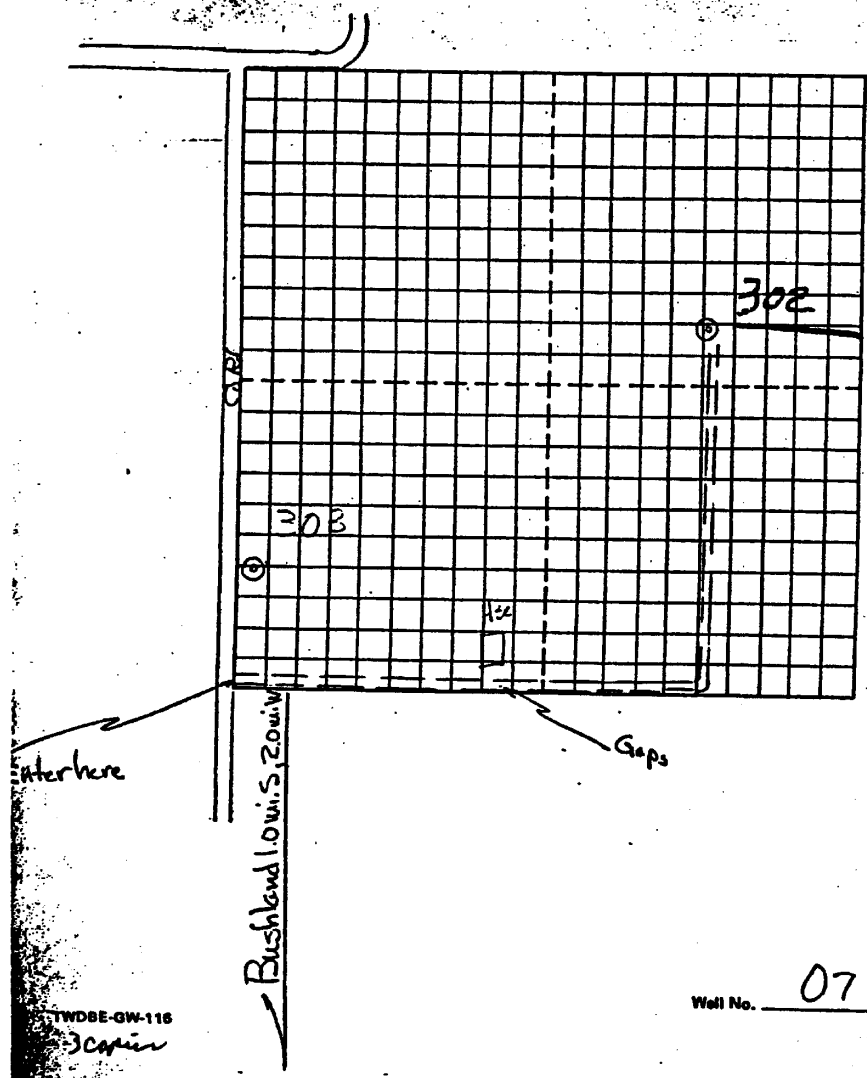
TITLE

ADDRESS

WATER WELL LOCATION SKETCH
TEXAS WATER DEVELOPMENT BOARD
GROUND WATER DIVISION

Section 127 in Block 9
Potter County
2 1/2-minute Quadrangle 3 1/6 in
7 1/2-minute Quadrangle 56
Sketch by D. Mueller Date 3-7-72

1 Mile



TWDBE-GW-116
3 Copies

Well No. 07 56 302

TEXAS WATER DEVELOPMENT BOARD

WELL SCHEDULE

Permit No. 242

UU 07.56.303

Aquifer: _____

Field No. _____

State Well No. _____

Owner's Well No. _____

County: Potter

1. Location: SW 1/4, SW 1/4 Sec. 127, Block 9 Survey B.S. & F
 2. Owner: Caroline B. Emery Address: _____
 Tenant: _____ Address: _____
 3. Driller: Dirks Ddg Co. Address: Hereford, Texas
 4. Elevation of LSD is 3804 ft. above mal, determined by 7 1/2 min. topo

5. Depth: Rept. 305 ft. Mess. _____ ft.
 6. Completion: Open Hole, Straight Wall, Underreamed, Gravel Packed
 7. Pump: Mfr. Deming Type Turbine
 No. Stages 6, Bore Dia. 12 in., Setting 290 ft.
 Column Dia. 8 in., Length Tailpipe _____ ft.
 8. Motor: Fuel NG Make & Model Minn-Moline HP. _____
 9. Yield: Flow _____ gpm, Pump 800 gpm, Mess. (R) gpm, Est. _____
 10. Performance Test: Date 5-25-66 Length of Test _____ Made by DRILLER

CASINO & BLANK PIPE			
Cemented From		ft. to	
Diam. (in.)	Type	Setting, ft.	
		from	to
16		0	305

Static Level 181 ft. Pumping Level 262 ft. Drawdown _____ ft.
 Production 800 gpm Specific Capacity _____ gpm/ft.
 11. Water Level: 181 ft. Cap. 5-25-1966 above
 mess. below
 ft. rept. 19 above which is ft. above surface.
 mean. below which is ft. below surface.
 ft. rept. 19 above which is ft. above surface.
 mess. below which is ft. below surface.
 ft. rept. 19 above which is ft. above surface.
 mess. below which is ft. below surface.
 12. Use: Dom., Stock, Public Supply, Ind., (R) Waterflooding, Observation, Not Used.
 13. Quality: (Remarks on taste, odor, color, etc.)

Temp. _____ °F, Date sampled for analysis _____ Laboratory _____
 Temp. _____ °F, Date sampled for analysis _____ Laboratory _____
 Temp. _____ °F, Date sampled for analysis _____ Laboratory _____

WELL SCREEN			
Screen Openings			
Diam. (in.)	Type	Setting, ft.	
		from	to
16	Perf	210	305

14. Other data available as circled: Driller's Log, Radioactivity Log, Electric Log, Formation Samples, Pumping Test.
 15. Record by: D. Müller Date 3-7-1972
 Source of Data Obs. DL
 16. Remarks: No access
 Base of Ogallala 295' (LW)

3804
 295

 3509

Triplicate County Committee

High Plains Underground Water Conservation District No. 1

REGISTRATION and LOG OF WELL

INSTRUCTIONS: Fill out in quadruplet. Submit all copies to County Committee for recommendation. (PLEASE TYPE OR PRINT)

FOR USE OF COMMITTEEMEN

Field Well No. _____

Date _____

Received _____

Permit Size _____ Maximum _____

of Pump _____ In Yield _____ GPM

1. Land Owner Pugh Estate Address Amarillo, Texas

2. Well located 1/4 miles N, _____ miles S, 2 miles E, _____ miles W of town of Parland, Texas

3. County Potter Labor _____ League _____ Abstract No. _____

4. NW $\frac{1}{4}$ NE $\frac{1}{4}$ SW $\frac{1}{4}$ SE $\frac{1}{4}$ Section 127 Block 9 Survey P.S. & F

MARK OUT THOSE THAT DO NOT APPLY

360 3
10 W

DRILLER'S LOG OF WELL

Method of Drilling: Rotary _____ Spudder _____ Diameter of Well: _____ inches.

MARK OUT ONE THAT DOES NOT APPLY

FROM (FEET)	TO (FEET)	DESCRIPTION OF FORMATION MATERIAL	FROM (FEET)	TO (FEET)	DESCRIPTION OF FORMATION MATERIAL
0	4	Top Soil	218	220	Hd wh sd rk
4	86	Caliche and clay	220	224	Sd rk
86	89	Hd caliche rk	224	295	Med. coarse Lt. Br. sd & sd rk layers
89	105	Soft caliche rk	295	305	Red soil
105	122	Sd rk, clay and caliche			
122	145	Sd, sd rk and caliche			
145	147	Hd sd rk			
147	158	Sd and sd rk			
158	181	Fine Lt. Br. sd.			
181	218				

REMARKS:

I hereby certify that this well was drilled by me (or under my supervision), and that each and all of the statements herein are true to the best of my knowledge and belief.

Driller Dirks Drilling Co. Address Hersford, Texas Date Drilled 5-25-19 66

DESCRIPTION OF WELL AND PRODUCTION EQUIPMENT

(This Does Not Mean Testing or Development Pump)

6. Casing new used gas line, or shop made. Diameter 16 in Total casing length 305 ft.

7. Casing perforations: from 210 ft. to 305 ft. Size 1/4 - 3/8 Number of rows 12-8

8. Pump Column: Size 8 in. Column, shaft length 250 ft. Suction pipe size 8 in. Suction pipe length 1 ft.

9. Pump bowls: Size 12 Number of stages 6 Pump discharge pipe: Size 8 in.

10. Depth to water level 181 ft. Pump yield 800 GPM. Pumping level: 262 ft.

11. Power Unit: Electrical, Natural Gas, Butane, Other _____ Horsepower _____

Signature _____

LANDOWNER OR AGENT TITLE ADDRESS

07-56-303

TEXAS WATER DEVELOPMENT BOARD

WELL SCHEDULE

Permit No. 241
 Field No. _____ State Well No. UU 07-56-304
 Owner's Well No. _____ County Potter

1. Location: NW 1/4, NE 1/4, Sec. 146, Block 9, Survey B.S. & F.

2. Owner: R. D. Durratt Address: _____
 Tenant: Leo Beener Address: _____
 Driller: Dirks Drilling Co Address: Hereford Texas

3. Elevation of LSD is 3821 ft. above sea level, determined by 7/23/66 topog.

4. Drilled: 4-6-1966; Dug, Cable Tool Rotary

5. Depth: Rept. 286 ft. Meas. _____ ft.

6. Completion: Open Hole, Straight Wall, Underreamed, Gravel Packed

7. Pump: Mfr. U.S. Always Type Turbine
 No. Stages 7, Bore Dia. 10 in., Setting 280 ft.
 Column Dia. 5 in., Length Tailpipe _____ ft.

8. Motor: Fuel NG Make & Model Mini-Moline HP 50GH

9. Yield: Flow _____ gpm, Pump 500 gpm, Meas. Rept., Est. _____

10. Performance Test: Date 4-6-66 Length of Test _____ Made by DELLER
 Static Level 200 ft. Pumping Level 250 ft. Drawdown 56 ft.
 Production 500 gpm Specific Capacity _____ gpm/ft.

11. Water Level: 200 ft. Rept. 4-6-1966 above surface.
 _____ ft. _____ 19 below surface.
 _____ ft. _____ 19 above surface.
 _____ ft. _____ 19 below surface.
 _____ ft. _____ 19 above surface.
 _____ ft. _____ 19 below surface.

12. Use: Dom., Stock, Public Supply, Ind. Irr. Waterflooding, Observation, Not Used.

13. Quality: (Remarks on tests, odor, color, etc.) _____
 Temp. _____ °F, Date sampled for analysis _____ Laboratory _____
 Temp. _____ °F, Date sampled for analysis _____ Laboratory _____
 Temp. _____ °F, Date sampled for analysis _____ Laboratory _____

14. Other data available as circled: Driller's Log Radioactivity Log, Electric Log, Formation Samples, Pumping Test.

15. Record by: D. Müller Date 2-7-1972
 Source of Data Obs., DL

16. Remarks: Access top cone N-side
Base of Ogallala 284' (K.W.)

CASINO & BLANK PIPE			
Cemented From Diam. (in.)	Type	ft. to	
		Setting, ft. from	to
16		0	286

WELL SCREEN			
Diam. (in.)	Type	Setting, ft.	
		from	to
16	Perf.	206	286

3821
 284

 3537

Original--District Office Copy

High Plains Underground Water Conservation District No. 1
REGISTRATION and LOG OF WELL

INSTRUCTIONS: Fill out in quadruplet. Submit all copies to County Committee for recommendation. (PLEASE TYPE OR PRINT)

FOR USE OF COMMITTEEMEN	
Field Well No.	771
Date Received	5-10-66
Permit Size	Maximum
of Pump	6 in Yield 600 GPM

1. Land Owner Delmar Durrett Address Amelia

2. Well located 2 miles N, 1 1/2 miles E, _____ miles W of town of Buckhorn

3. County Hottel Labor _____ League _____ Abstract No. _____

4. NW 1/4 SW 1/4 _____ SE 1/4 _____ Section 146 Block 9 Survey BC & F

MARK OUT THOSE THAT DO NOT APPLY

324 N

626 W

DRILLER'S LOG OF WELL

Method of Drilling: Rotary ~~Spudger~~ _____ Diameter of Well: 19 inches.

MARK OUT ONE THAT DOES NOT APPLY

FROM (FEET)	TO (FEET)	DESCRIPTION OF FORMATION MATERIAL	FROM (FEET)	TO (FEET)	DESCRIPTION OF FORMATION MATERIAL
0	4	Top Soil			
4	91	caliche & clay			
91	93	caliche rk			
93	103	caliche, clay & caliche rk			
103	121	Mel course lt br sil.			
121	225	Mel course sd & caliche bed rd			
225	280	Mel lt br sil & sd rk lens			
280	284	Course sd & gravel			
284	286	Rel Bed			

REMARKS:

I hereby certify that this well was drilled by me (or under my supervision), and that each and all of the statements herein are true to the best of my knowledge and belief.

Driller Dirks Drilling Co Address Harvard Date Drilled 4-6-1966

DESCRIPTION OF WELL AND PRODUCTION EQUIPMENT

(This Does Not Mean Testing or Development Pump)

6. Casing: new, used, gas line, or shop made. Diameter 16 in Total casing length 286 ft.

7. Casing perforations: from 206 ft. to 286 ft. Size 1/4-3/16 Number of rows 8-10

8. Pump Column: Size 6 in. Column, shaft length 200 ft. Suction pipe size 6 in. Suction pipe length 1 ft.

9. Pump bowls: Size 10 Number of stages 7 Pump discharge pipe: Size 6 in.

10. Depth to water level 200 ft. Pump yield 500 GPM. Pumping level: 286 ft.

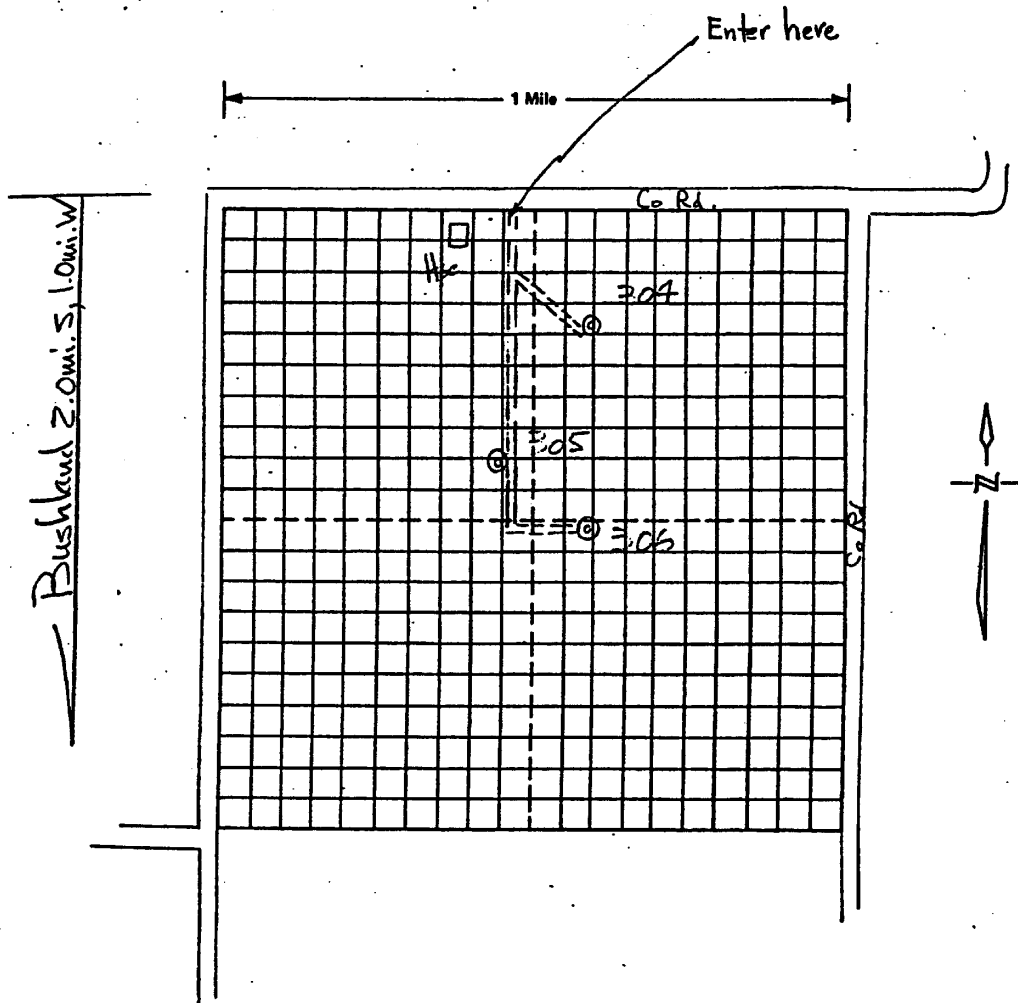
11. Power Unit: Electrical, Natural Gas, Butane, Other _____ Horsepower 70

Signature _____

LANDOWNER OR AGENT TITLE ADDRESS

WATER WELL LOCATION SKETCH
TEXAS WATER DEVELOPMENT BOARD
GROUND WATER DIVISION

Section 146 in Block 9
Potter County
2 1/2-minute Quadrangle 2,3,5,6 in
7 1/2-minute Quadrangle 56
Sketch by D. Müller Date 3-7-72



TWDBE-GW-116
Scapion

Well No. 07 56 304

TEXAS WATER DEVELOPMENT BOARD
WELL SCHEDULE

Permit No. 246

State Well No. 07-56-305

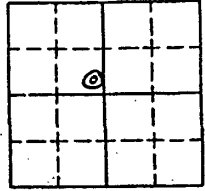
Aquifer _____

Field No. _____

County Potter

Owner's Well No. _____

1. Location: SE 1/4 NW 1/4 Sec. 146, Block 9, Survey B.S. 2 F



2. Owner: Leo Bezyer Address: _____

Tenant: _____ Address: _____

Driller: _____ Address: _____

3. Elevation of LSD is 3815 ft. above sea level, determined by 1/2 W.W. Lope

4. Drilled: 19 ft. Dug, Cable Tool, Rotary, _____

5. Depth Rept. _____ ft. Mess. _____ ft.

6. Completion: Open Hole, Straight Wall, Underreamed, Gravel Packed

7. Pump: Mfg. Wiestroeth Type Turbine

No. Stages _____, Bore Dia. _____ in., Setting _____ ft.

Column Dia. 6 in., Length Tailpipe _____ ft.

8. Motor: Fuel NG Make & Model Minn. Moline No. 75GH

9. Yield: Flow _____ gpm, Pump _____ gpm, Mess., Rept., Est. _____

10. Performance Test: Date _____ Length of Test _____ Note by _____

Static Level _____ ft. Pumping Level _____ ft. Drawdown _____ ft.

Production _____ gpm Specific Capacity _____ gpm/ft.

11. Water Level: _____ ft. reft. _____ 19 above _____ which is _____ ft. above surface.
 _____ ft. reft. _____ 19 below _____ which is _____ ft. above surface.
 _____ ft. reft. _____ 19 below _____ which is _____ ft. above surface.
 _____ ft. reft. _____ 19 below _____ which is _____ ft. above surface.

12. Use: Dom., Stock, Public Supply, Ind., Irr. Waterflooding, Observation, Not Used,

13. Quality: (Remarks on taste, odor, color, etc.) _____

Temp. _____ °F, Date sampled for analysis _____ Laboratory _____

Temp. _____ °F, Date sampled for analysis _____ Laboratory _____

Temp. _____ °F, Date sampled for analysis _____ Laboratory _____

14. Other data available as circled: Driller's Log, Radioactivity Log, Electric Log,

Formation Samples, Pumping Test.

15. Record by: D. Müller Date 3-7-1972

Source of Data Obs., DL

16. Remarks: Access top of cone blk.

CASTING & BLANK PIPE			
Cemented From		ft. to	
Diam. (in.)	Type	Setting, ft.	
		from	to

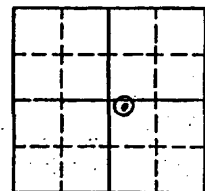
WELL SCREEN			
Screen Openings		Setting, ft.	
Diam. (in.)	Type	from	

TEXAS WATER DEVELOPMENT BOARD

WELL SCHEDULE

Permit No. 207
 Field No. _____
 Owner's Well No. _____
 State Well No. UU 07-56-306
 County Pettit

1. Location: NW 1/4, SE 1/4 Sec. 146, Block 9, Survey B.S. & F.
 2. Owner: R.D. Durrett Address: _____
 Tenant: Leo Beazer Address: _____
 Driller: J.H. Fish Address: Hereford, Texas
 3. Elevation of LSD is 3814 ft. above sea, determined by 7 1/2 min. topo.



4. Drilled: 11-9-1954, Dug, Cable Tool, Rotary
 5. Depth: 305 ft. Meas. _____ ft.
 6. Completion: Open Hole, Straight Wall, Underreamed, Gravel Packed
 7. Pump: Mfg. Pomona Type Turbine
 No. Stages 6, Bowls Diam. 12 in., Setting 270 ft.
 Column Diam. 6 in., Length Tailpipe _____ ft.
 8. Motor: Powl NG Make & Model Minn-Moline HP. 75GH.
 9. Yield: Flow _____ gpm, Pump 600 gpm, Meas. Sept., Est. _____
 10. Performance Test: Date 11-9-54 Length of Test _____ Made by DELLER
 Static Level 185 ft. Pumping Level 250 ft. Drawdown _____ ft.
 Production 600 gpm Specific Capacity _____ gpm/ft.

CASING & BULK PIPE			
Cemented From		ft. to _____ ft.	
Diam. (in.)	Type	Setting, ft.	
		from	to
16		0	305

11. Water Level: 185 ft. Sept. 11-9-1954 above _____ ft. below surface.
 _____ ft. rept. 19 above _____ ft. below surface.
 _____ ft. rept. 19 above _____ ft. below surface.
 _____ ft. rept. 19 above _____ ft. below surface.
 _____ ft. rept. 19 above _____ ft. below surface.

12. Use: Dom., Stock, Public Supply, Ind. Irr. Waterflooding, Observation, Not Used.
 13. Quality: (Remarks on taste, odor, color, etc.) _____

Temp. _____ °F, Date sampled for analysis _____ Laboratory _____
 Temp. _____ °F, Date sampled for analysis _____ Laboratory _____
 Temp. _____ °F, Date sampled for analysis _____ Laboratory _____

14. Other data available as circled: Driller's Log Radioactivity Log, Electric Log,
 Formation Samples, Pumping Test,

15. Record by: D. Muller Date 3-7-1972
 Source of Data Obs. DL

16. Remarks: Access N-side pump base
Base of Ogallala 302' (TW)

WELL SCREEN			
Screen Openings		Setting, ft.	
Diam. (in.)	Type	from	to
16	Perf.	215	305

REGISTRATION and LOG OF WELL

INSTRUCTIONS: Fill out in quadruplet. Submit all copies to County Committee for recommendation. (PLEASE TYPE OR PRINT)

Field Well No.	207
Date Received	1-11-55
Permit Size	Maximum
of Pump	6 in Yield 700 GPM

1. Land Owner Delmar Durrett Address Amarillo

2. Well located 1 1/2 miles N, _____ miles S, 1 1/2 miles E, _____ miles W of town of Bushkauf

3. County Potter Labor _____ League _____ Abstract No. _____

4. NW 1/4 NE 1/4 SW 1/4 SE 1/4 Section 146 Block 9 Survey BS & F

MARK OUT THOSE THAT DO NOT APPLY

880 N
740 E

DRILLER'S LOG OF WELL

Method of Drilling: Rotary Spudder _____ Diameter of Well: _____ inches.

MARK OUT ONE THAT DOES NOT APPLY

FROM (FEET)	TO (FEET)	DESCRIPTION OF FORMATION MATERIAL	FROM (FEET)	TO (FEET)	DESCRIPTION OF FORMATION MATERIAL
0	4	Caliche			
4	60	Clay			
60	160	Sd 1/2 cly			
160	161	RK			
161	220	Cly			
220	267	Fu sd			
267	302	Sd 1/2 gravel			
302	305	Red Bed			

REMARKS:

I hereby certify that this well was drilled by me (or under my supervision), and that each and all of the statements herein are true to the best of my knowledge and belief.

Driller J.H. Fish Address Hereford Date Drilled 11-9-1954

DESCRIPTION OF WELL AND PRODUCTION EQUIPMENT

(This Does Not Mean Testing or Development Pump)

6. Casing: new, used, gas line, or shop made. Diameter 16 in Total casing length _____ ft.

7. Casing perforations: from 215 ft. to 305 ft. Size 1/4 X 12 Number of rows 8

8. Pump Column: Size 6 in. Column, shaft length 270 ft. Suction pipe size 6 in. Suction pipe length 10 ft.

9. Pump bowls: Size 12 Number of stages 6 Pump discharge pipe: Size 6 in.

10. Depth to water level 185 ft. Pump yield 600 GPM. Pumping level: 250 ft.

11. Power Unit: Electrical, Natural Gas, Outage, Other _____ Horsepower: 75

Signature _____ TITLE _____ ADDRESS _____

LANDOWNER OR AGENT

TEXAS WATER DEVELOPMENT BOARD
WELL SCHEDULE

Aquifer Ogallala

Field No. Perm. # 276

State Well No. 07-56-307

Owner's Well No. _____

County Potter

1. Location: NW 1/4, NW 1/4 Sec. 127, Block B-9, Survey B.S. & F

2. Owner: Caroline B. Emery Address: Box 1230, Amarillo, Tx.
 Tenant: Victor Plusk Address: Rt 1, Box 544, Amarillo, Tx.
 Driller: Bud Gibbens Address: Plainview, TX

3. Elevation of _____ is 3814 ft. above sea level, determined by _____

4. Drilled: 3-8-74; Log, Cable Tool Rotary

5. Depth: Rept. 295 ft. Meas. _____ ft. Red Bed Reported @ 287.5 ft.

6. Completion: Open Hole (Straight Wall) Underreamed, Gravel Packed

7. Pump: Mgr. Johnson p.b. Amarillo Co. Type Turbine
 No. Stages 7, Bowl Diam. 10 in., Setting 290 ft.
 Column Diam. 6 in., Length Tailpipe 10 ft.

8. Motor: Fuel NAT GAS Make & Model M.M. 6 cyl. HP.

9. Yield: Flow _____ gpm, Pump 400 gpm, Meas. Rept. Est. Driller

10. Performance Test: Date _____ Length of Test _____ Made by _____

Static Level _____ ft. Pumping Level _____ ft. Drawdown _____ ft.
Production _____ gpm Specific Capacity _____ gpm/ft.

11. Water Level: 227.98 ft. 9/13 1976 above See MP Below

ft. rpt. _____	19	above	which is <u>+0.50</u> ft. above surface.
ft. rpt. _____	19	below	which is _____ ft. below surface.
ft. meas. _____	19	above	which is _____ ft. above surface.
ft. rpt. _____	19	below	which is _____ ft. below surface.
ft. meas. _____	19	above	which is _____ ft. above surface.
ft. rpt. _____	19	below	which is _____ ft. below surface.

12. Use: Dom., Stock, Public Supply, Ind. Irr. Waterflooding, Observation Not Used.

13. Quality: (Remarks on taste, odor, color, etc.) _____

Temp. _____ °F, Date sampled for analysis _____ Laboratory _____

Temp. _____ °F, Date sampled for analysis _____ Laboratory _____

Temp. _____ °F, Date sampled for analysis _____ Laboratory _____

14. Other data available as circled: Driller's Log Radioactivity Log, Electric Log, Formation Samples, Pumping Test.

15. Record by: DAN SEALE Date 9/13 1976

Source of Data Field & H.P.U.W.C.D. Records

16. Remarks: Permission from Mr. F. E. Colwell III, Manager to enter this well into the program

CASING & BLANK PIPE			
Cemented From		ft. to	
Diam. (in.)	Type	Setting, ft.	
		from	to
14	Steel	Surface	295

WELL SCREEN			
Screen Openings			
Diam. (in.)	Type	Setting, ft.	
		from	to
14	Perforated	197	295
Casing Re-lined with 3/8" slits			
4 row pattern.			

Obs Well

3814
38289
3525

M.P. - Edge of Air-line Hole
inside pump port
S. side = +0.50 ft

(Sketch)

07-56-307

Typewrite (black ribbon) or print plainly
(soft, pencil or black ink)
Do not use ball point pen

Texas Department of Health Laboratories
1100 West 49th Street
Austin, Texas 78756

TDWR ONLY

Organization No. _____ Lab No.

Work No. _____

CHEMICAL WATER ANALYSIS REPORT

Send report to:
Data Collection and Evaluation Section
Texas Department of Water Resources
P.O. Box 13087
Austin, Texas 78711

S. R. S.
SEP 19 1980

County 188 Bottle

State Well No. 07 56 3d7

Well No. 276

Date Collected 08 01 80

Location NW 1/4, NW 1/4, Sec. 127, Blk B-9, B&F Survey Sample No. By HPAWCD #1 B5

Source (type of well) turbine Owner Caroline Embry

Date Drilled 3-8-74 Depth 295 ft. WBF Ogallala

Producing intervals _____ Water level _____ ft. Sample depth _____ ft.

Sampled after pumping cont hrs. Yield _____ GPM °F °C

Point of collection tadcet on discharge Appearance clear turbid colored other

Use irr. Remarks _____

(FOR LABORATORY USE)

CHEMICAL ANALYSIS

Laboratory No. CO15975 Date Received AUG 18 1980 Date Reported SEP 17 1980

	MG/L	ME/L
Silica . . . 00955 . . .	57	
Calcium . . . 00915 . . .	47	2.36
Magnesium . . . 00925 . . .	26	2.11
Sodium . . . 00929 . . .	29	1.26
	Total	5.73
<input type="checkbox"/> Potassium . . . 00937 . . .		
<input type="checkbox"/> Manganese . . . 01055 . . .		XNa _____
<input type="checkbox"/> Boron . . . 01022 . . .		SAR _____
<input type="checkbox"/> Total Iron . . . 01045 . . .		RSC _____

(other) _____ MG/L

Specific Conductance (micromhos/cm³) . . . 00095 . . . 490

Diluted Conductance (micromhos/cm³) 4 x 144 = 576

Items will be analyzed if checked.

¹The bicarbonate reported in this analysis can be converted by computation (multiplying by 0.4917) to an equivalent amount of carbonate, and the carbonate figure used in the computation of dissolved solids.
²Nitrogen cycle requires separate sample.
³Total Iron and Manganese require separate sample.

TDWR-0148 (Rev. 1-8-80)

	MG/L	ME/L
Carbonate . . . 00445 . . .	0	
¹⁴⁴ Bicarbonate . . . 00440 . . .	293	4.80
Sulfate . . . 00945 . . .	30	0.62
Chloride . . . 00940 . . .	7	0.20
Fluoride . . . 00951 . . .	2.4	0.1
Nitrate . . . 71850 . . .	2.9	
pH . . . 00403 . . .	8.2	
	Total	5.75
¹ Dissolved Solids (residue at 180°C) . . . 70300 . . .		250
Phenolphthalein Alkalinity as CaCO ₃ . . . 00415 . . .		0
Total Alkalinity as CaCO ₃ (<u>4.80</u>) . . . 00410 . . .		240
Total Hardness as CaCO ₃ (<u>4.47</u>) . . . 00900 . . .		224
Ammonia - N . . . ² Nitrogen Cycle . . . 00610 . . .		
Nitrite - N . . . RE . . . 00615 . . .		
Nitrate - N . . . JUL-25-1981 . . . 00620 . . .		
Organic Nitrogen . . . (CH ₂ O) _n . . . 00605 . . .		

Analyst _____ Checked By _____

1) OWNER: Person having well drilled Caroline B. Emney Address Box 1230 Amarillo Texas
 (Name) (Street or RFD) (City) (State)
 Landowner Same Address Same
 (Name) (Street or RFD) (City) (State)

2) LOCATION OF WELL: County Potter 3/4-N & 2-E miles in NE direction from Bushland, Texas
 (Name) (Section, S.E., etc.) (Town)
 Locate by sketch map showing landmarks, roads, creeks, highway number, etc.
 Give legal location with distances and directions from adjacent sections or survey lines.
 Labor _____ League _____
 Block 9 Survey BS & F
 Abstract No. _____
 (WATER WELL) of Section 127
 (Use reverse side if necessary)

3) TYPE OF WELL (Check): New Well Reconditioning Deepening Flugging
 4) PROPOSED USE (Check): Domestic Industrial Municipal Irrigation Test Well Other
 5) TYPE OF WELL (Check): Rotary Cable Driven Jetted Dog Bored

6) WELL LOG: Diameter of hole 1 1/2" in. Depth drilled 295' ft. Depth of completed well _____ ft. Date drilled 3-8-74
 All measurements made from _____ ft. above ground level.

From (ft.)	To (ft.)	Description and color of formation material	9) Casing: Type: Old _____ New <input checked="" type="checkbox"/> Steel <input checked="" type="checkbox"/> Plastic _____ Other _____
0	4	Top Soil	Commented from _____ ft. to _____
4	82	Caliche Clay	Diameter (inches) _____ Setting From (ft.) _____ To (ft.) _____ Casing _____
82	153	Clay Sand Beck & Sand	<u>1 1/2" OD.</u> <u>0</u> <u>295</u> <u>.188 Wall</u>
153	259	Clay and Layers Sand	<u>(197' - 2 95' - 4 row Perforation</u>
259	279	Fine sand	
279	289	Course Sand	10) SCREENS: Type _____ Perforated _____ slotted _____
289	295	Blue Clay and Red Bed	Diameter (inches) _____ Setting From (ft.) _____ To (ft.) _____ Slot Size _____

7) COMPLETION (Check): Straight well Gravel packed _____ Other _____ Under reamed _____ Open Hole _____
 8) WATER LEVEL: Static level _____ ft. below land surface Date _____ Artesian pressure _____ lbs. per square inch Date _____ Depth to pump bowls, cylinder, jet, etc., _____ ft. below land surface.
 11) WELL TESTS: Was a pump test made? Yes _____ No If yes, by whom _____ Yield: _____ gpm with _____ ft. drawdown after _____ Bailor test _____ gpm with _____ ft. drawdown after _____ Artesian flow _____ gpm Temperature of water _____
 12) WATER QUALITY: Was a chemical analysis made? Yes _____ No Did any strata contain undesirable water? Yes _____ No _____ Type of water? _____ depth of strata _____

I hereby certify that this well was drilled by me (or under my supervision) and that each and all of the statements herein are true to the best of my knowledge and belief.
 NAME Bud Gibbons Water Well Drillers Registration No. 299
 (Type or Print)
 ADDRESS 1004 E. 5th, P.O. Box 1972 Plainview Texas
 (Street or RFD) (City) (State)
 (Signed) Bud Gibbons Bud Gibbons Drilling Contractor
 (Water Well Driller) (Company Name)

Please attach electric log, chemical analysis, and other pertinent information, if available. 44-07-56-307
 Additional instructions on reverse side.

TEXAS WATER DEVELOPMENT BOARD

WELL SCHEDULE

Aquifer -----
 Permit No. 248
 Field No. -----
 State Well No. 44 07-56-603
 Owner's Well No. -----
 County Patterson

1. Location: NE 1/4, NW 1/4 Sec. 128, Block 9, Survey B.S. & F.
 2. Owner: Fritz Menke Address: -----
 Tenant: ----- Address: -----
 Driller: Bud Gibbons Address: Plainview, Texas
 3. Elevation of LSD is 3797 ft. above sea, determined by 7 1/2 min. tops.

4. Drilled: 4-5-1969, Dug, Cable Tool, Rotary
 5. Depth: Rept. 314 ft. Meas. ----- ft.
 6. Completion: Open Hole; Straight Wall, Underreamed, Gravel Packed
 7. Pump: Mfg. Western Type Turbine
 No. Stages 7, Bowls Diam. 10 in., Setting ----- ft.
 Column Diam. 6 in., Length Tailpipe ----- ft.
 8. Motor: Fuel NG Make & Model Chrysler Ind. HP. 50GH
 9. Yields: Flow ----- gpm, Pump 550 gpm, Meas. Rept., Est. -----
 10. Performance Test: Date 4-5-69 Length of Test ----- Made by DRILLER
 Static Level 200 ft. Pumping Level 250 ft. Drawdown 50 ft.
 Production 550 gpm Specific Capacity ----- gpm/ft.

CASING & BLANK PIPE			
Cemented From		ft. to	
Diam. (in.)	Type	Setting, ft.	
		from	to
16		0	314

11. Water Level: 200 ft. Rept. 4-5-1969 above ----- ft. above surface.
 ----- ft. meas. ----- below ----- ft. below surface.
 ----- ft. rept. 19 above ----- ft. below surface.
 ----- ft. meas. ----- below ----- ft. below surface.
 ----- ft. rept. 19 above ----- ft. below surface.
 ----- ft. meas. ----- below ----- ft. below surface.

12. Use: Dom., Stock, Public Supply, Ind., Irr., Waterflooding, Observation, Not Used.
 13. Quality: (Remarks on taste, odor, color, etc.) -----
 Temp. ----- °F, Date sampled for analysis ----- Laboratory -----
 Temp. ----- °F, Date sampled for analysis ----- Laboratory -----
 Temp. ----- °F, Date sampled for analysis ----- Laboratory -----

WELL SCREEN			
Screen Openings		Setting, ft.	
Diam. (in.)	Type	from	to
16	Perf.	250	305

14. Other data available as circled: Driller's Log, Radioactivity Log, Electric Log, Formation Samples, Pumping Test.
 15. Record by: D. Müller Date 3-7-1972
 Source of Data Obs., DL
 16. Remarks: Access S-side pump base
Base of Ogallala 306' (est)

Triplicate County Committee

High Plains Underground Water Conservation District No. 1

REGISTRATION and LOG OF WELL

INSTRUCTIONS: Fill out in quadruplet. Submit all copies to County Committee for recommendation. (PLEASE TYPE OR PRINT)

FOR USE OF COMMITTEEMEN	
Field Well No.	248
Date	
Received	
Permit Size	Maximum
of Pump 6	In Yield 560 GPM

1. Land Owner Fritz Menke Address Amarillo

2. Well located _____ miles N, 1 miles S, _____ miles E, 2 3/4 miles W of town of Bushland

3. County Potter Labor _____ League _____ Abstract No. _____

Section 12B Block 9 Survey BS & F

NW 1/4 NE 1/4 SW 1/4 SE 1/4
 MARK OUT THOSE THAT DO NOT APPLY

10 N
 530 W

DRILLER'S LOG OF WELL

Method of Drilling: Rotary Spudger Diameter of Well: 18 inches

FROM (FEET)	TO (FEET)	DESCRIPTION OF FORMATION MATERIAL	FROM (FEET)	TO (FEET)	DESCRIPTION OF FORMATION MATERIAL
0	4	Top Soil	295	306	12s
4	12	Caliche	306	314	Red bed
12	70	Sdy Cly			
70	85	RK			
85	220	Ss			
220	228	RK			
228	240	Ss			
240	255	Sd			
255	258	RK			
258	295	Sd Gravel			

REMARKS:

I hereby certify that this well was drilled by me (or under my supervision), and that each and all of the statements herein are true to the best of my knowledge and belief.

Driller Bud Gibbons Address Plainview, Texas Date Drilled 4-5-1969

DESCRIPTION OF WELL AND PRODUCTION EQUIPMENT

(This Does Not Mean Testing or Development Pump)

6. Casing: new, used gas line, or shop made. Diameter 16 in Total casing length 314 ft.

7. Casing perforations: from 250 ft. to 305 ft. Size 1/4 Number of rows 6

8. Pump Column: Size 6 in. Column, shaft length 2 ft. Suction pipe size _____ in. Suction pipe length _____ ft.

9. Pump bowls: Size 10 Number of stages 7 Pump discharge pipe: Size 6 in.

10. Depth to water level 200 ft. Pump yield 550 GPM. Pumping level: 250 ft.

11. Power Unit: Electrical Natural Gas, Butane, Other _____ Horsepower 55

Signature _____
 LANDOWNER OR AGENT TITLE ADDRESS

07-56-603

TEXAS WATER DEVELOPMENT BOARD

WELL SCHEDULE

Permit No. 224
 Aquifer ----- Field No. ----- State Well No. 111 07-56-602
 Owner's Well No. ----- County Potter

1. Location: NW 1/4, NW 1/4 Sec. 128, Block 9, Survey BS & F.

⊙		

2. Owner: Fritz Menke Address: -----
 Tenant: ----- Address: -----
 Driller: Charlie McCaskill Address: Amarillo, Texas

3. Elevation of LSD is 3803 ft. above sea, determined by 1/2 mile topo

4. Drilled: 4-10-1963, Dug, Cable Tool, Rotary,

5. Depth: Rept. ----- ft. Meas. ----- ft.

6. Completion: Open Hole, Straight Wall, Underreamed, Gravel Packed

7. Pump: Mfg. Western Type Turbine
 No. Stages 5, Bore Dia. 12 in., Setting 280 ft.
 Column Dia. 6 in., Length Tailpipe ----- ft.

8. Motor: Fuel NG Make & Model Chrysler Ind. HP. 50GH

9. Yields: Flow ----- gpm, Pump 700 gpm, Meas. (Rept. Est.) -----

10. Performance Test: Date 9-10-63 Length of Test ----- Made by DRILLER
 Static Level 190 ft. Pumping Level 280 ft. Drawdown 90 ft.
 Production 280 gpm Specific Capacity ----- gpm/ft.

CASING & BLANK PIPE			
Cemented From		ft. to	
Diam. (in.)	Type	Setting, ft.	
		From	to

11. Water Level: 190 ft. rept. 4-10-1963 above surface, which is ----- ft. above surface.
 ----- ft. rept. ----- below surface, which is ----- ft. above surface.
 ----- ft. rept. ----- below surface, which is ----- ft. above surface.
 ----- ft. rept. ----- below surface, which is ----- ft. above surface.

12. Use: Dom., Stock, Public Supply, Ind., Irr. Waterflooding, Observation, Not Used.

13. Quality: (Remarks on taste, odor, color, etc.) -----

Temp. ----- °F, Date sampled for analysis ----- Laboratory -----
 Temp. ----- °F, Date sampled for analysis ----- Laboratory -----
 Temp. ----- °F, Date sampled for analysis ----- Laboratory -----

14. Other data available as circled: Driller's Log, Radioactivity Log, Electric Log, Formation Samples, Pumping Test.

15. Record by: D. Müller Date 3-7-1972
 Source of Data Obs., DL

16. Remarks: Access S-side dump base
Base of Ogallala 300' (HW)

WELL SCREEN			
Screen Openings			
Diam. (in.)	Type	Setting, ft.	
		From	to

Quadruplicate - Applicant's Copy

07-56-60

FOR USE OF COMMITTEEMEN

High Plains Underground Water Conservation District No. 1
REGISTRATION and LOG OF WELL

INSTRUCTIONS: Fill out in quadruplet. Submit all copies to County Committee for recommendation. (PLEASE TYPE OR PRINT)

Field Well No. 229
 Date Received 7-30-63
 Permit Size Maximum
 of Pump 6 in Yield 65 GPM

1. Land Owner Fritz Menke Address Artesville
 2. Well located 1 miles N, _____ miles S, _____ miles E, 2 miles W of town of Puckett
 3. County Potter Labor _____ League _____ Abstract No. _____
 4. NW¼ NE¼ SW¼ SE¼ Section 128 Block 9 Survey B5 3 F
MARK OUT THOSE THAT DO NOT APPLY

10 N
200 W

DRILLER'S LOG OF WELL

Method of Drilling: Rotary _____ Spudder _____ Diameter of Well: _____ inches.
MARK OUT ONE THAT DOES NOT APPLY

FROM (FEET)	TO (FEET)	DESCRIPTION OF FORMATION MATERIAL	FROM (FEET)	TO (FEET)	DESCRIPTION OF FORMATION MATERIAL
0	5	Top Soil	267	285	Coarse Sd
5	85	Caliche	285	300	Sd & Gravel
85	115	Sd & Clay	200	305	Red Pcl
115	119	Wh Rk			
119	145	Sd & Chy			
145	180	Coarse Sd			
180	240	Sd & Chy			
240	243	Hd Rk			
243	265	Coarse Sd			
265	267	Hd Rk			

REMARKS:

I hereby certify that this well was drilled by me (or under my supervision), and that each and all of the statements herein are true to the best of my knowledge and belief.

Driller Charlie McCeskill Address Artesville Date Drilled 7-10-1963

DESCRIPTION OF WELL AND PRODUCTION EQUIPMENT

(This Does Not Mean Testing or Development Pump)

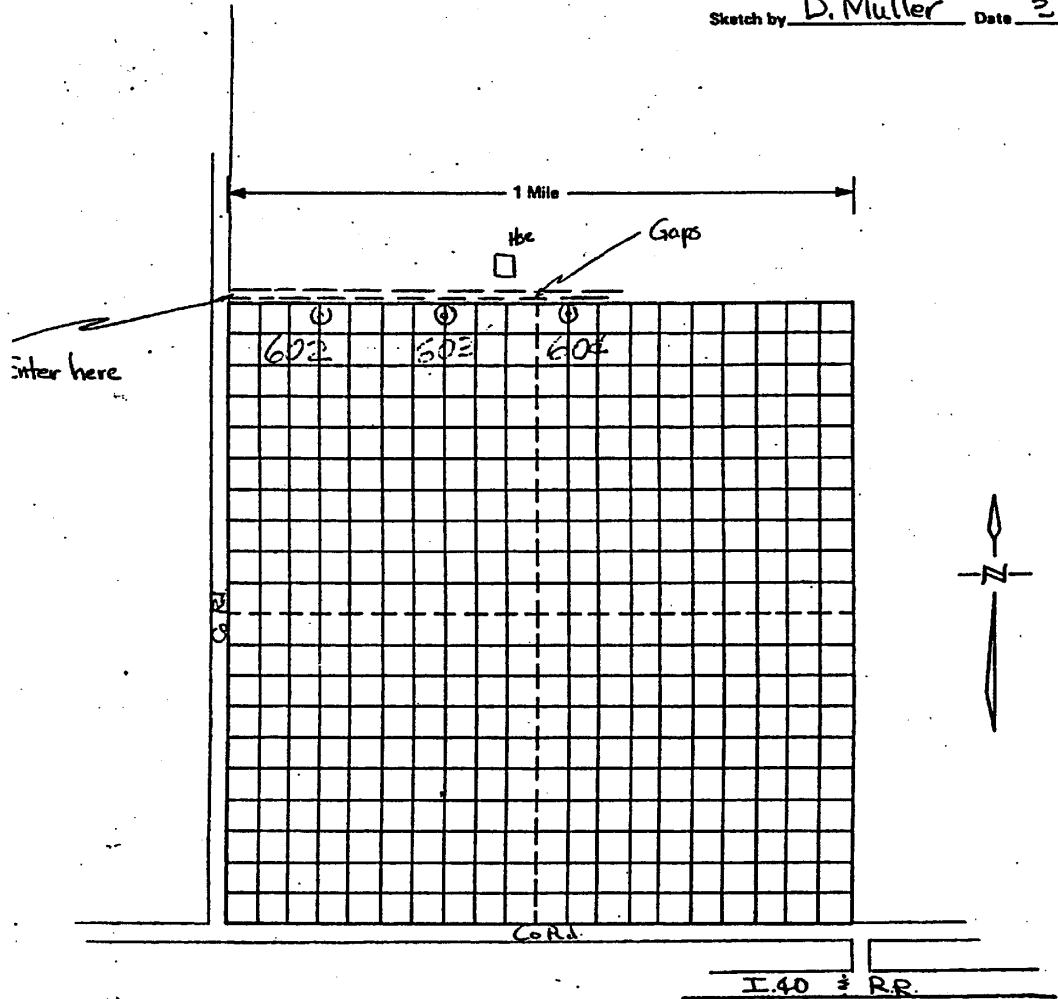
6. Casing new used, gas line, or shop made. Diameter 16 in Total casing length 305 ft.
 7. Casing perforations: from 202 ft. to 305 ft. Size 1/8 Number of rows 14
 8. Pump Column: Size 6 in. Column, shaft length 280 ft. Suction pipe size _____ in. Suction pipe length _____ ft.
 9. Pump bowls: Size 12 Number of stages 5 Pump discharge pipe: Size 6 in.
 10. Depth to water level 190 ft. Pump yield 700 GPM. Pumping level: 280 ft.
 11. Power Unit: Electrical, Natural Gas, Butane, Other _____ Horsepower _____

Signature _____ TITLE _____ ADDRESS _____

07-56-602

WATER WELL LOCATION SKETCH
TEXAS WATER DEVELOPMENT BOARD
GROUND WATER DIVISION

Section 128 In Block 9
Potter County
2 1/2-minute Quadrangle 6 in
7 1/2-minute Quadrangle 56
Sketch by D. Müller Date 2-7-72



TWDBE-GW-118
S. Capron

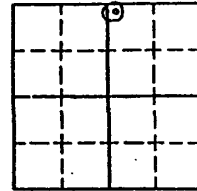
Well No. 07 . 56 . 602

TEXAS WATER DEVELOPMENT BOARD

WELL SCHEDULE

Permit No. 247
 State Well No. 07-56604
 County Potter

Location: NW 1/4, NE 1/4 Sec. 128, Block 9, Survey B.S. 3 E.
 Owner: Fritz Meuke, Address: Amarillo, Texas
 Tenant: _____, Address: _____
 Driller: Bud Gibbons, Address: Plainview, Texas
 Elevation of LSD is 3791 ft. above sea, determined by 7 1/2 Min. Topo.



Drilled: 4-3-1969, Dug, Cable Tool (Rotary)
 Depth: Rept. _____ ft. Meas. _____ ft.
 Completion: Open Hole, Straight Wall, Underscreened, Gravel Packed
 Pump: Mfg. A & C, Type Turbine
 No. Stages 7, Bore Dia. 10 in., Setting 284 ft.
 Column Dia. 6 in., Length Tailpipe _____ ft.
 Motor: Fuel NG, Make & Model Chrysler Ind. HP. 50GH
 Yield: Flow _____ gpm, Pump 500 gpm, Meas. (Rept.) Est.
 Performance Test: Date 4-3-69, Length of Test _____, Made by DRILLER
 Static Level 200 ft., Pumping Level 265 ft., Drawdown 65 ft.
 Production 500 gpm, Specific Capacity _____ gpm/ft.

CASING & BLANK PIPE			
Cemented From		ft. to	
Diam. (in.)	Type	Setting, ft.	
		from	to
16		0	312

- Water Level: 200 ft. (LSD) 4-3-1969 above/below surface.
 - ft. meas. 19 above/below surface.
 - ft. meas. 19 above/below surface.
 - ft. meas. 19 above/below surface.
 - ft. meas. 19 above/below surface.
- Use: Dom., Stock, Public Supply, Ind. (irr.) Waterflooding, Observation, Not Used.
- Quality: (Remarks on taste, odor, color, etc.)

Temp. _____ °F, Date sampled for analysis _____, Laboratory _____
 Temp. _____ °F, Date sampled for analysis _____, Laboratory _____
 Temp. _____ °F, Date sampled for analysis _____, Laboratory _____

4. Other data available as circled: Driller's Log, Radioactivity Log, Electric Log, Formation Samples, Pumping Test.
 5. Record by: D. Müller, Date 2-8-1972
 Source of Data Obs., DL

6. Remarks: Access S-side pump base
 Base of Ogallala 30.5' (hor.)

WELL SCREEN			
Screen Openings		Setting, ft.	
Diam. (in.)	Type	from	to
16	Perf.	250	305

Duplicate File Copy

07-56-60

FOR USE OF COMMITTEEMEN

High Plains Underground Water Conservation District No. 1

REGISTRATION and LOG OF WELL

INSTRUCTIONS: Fill out in quadruplet. Submit all copies to County Committee for recommendation. (PLEASE TYPE OR PRINT)

Field Well No. 247
 Date _____
 Received _____
 Permit Size _____ Maximum _____
 of Pump 6 in Yield 560 GPM

- Land Owner Fritz Meuke Address El Amarillo Texas
- Well located _____ miles N, 1 miles S, _____ miles E, 2 1/2 miles W of town of Bushland
- County Potter Labor _____ League _____ Abstract No. _____
- NW¼ NE¼ SW¼ SE¼ Section 128 Block 9 Survey BS&F

MARK OUT THOSE THAT DO NOT APPLY
 18 N
 870 W

DRILLER'S LOG OF WELL

Method of Drilling: Rotary _____ Spudder _____ Diameter of Well: 18 inches.
 MARK OUT ONE THAT DOES NOT APPLY

FROM (FEET)	TO (FEET)	DESCRIPTION OF FORMATION MATERIAL	FROM (FEET)	TO (FEET)	DESCRIPTION OF FORMATION MATERIAL
0	4	Top Soil			
4	15	Caliche			
15	90	Sdy Cly			
90	220	Ss			
220	250	Rk			
250	295	Sd Gravel			
295	305	Ss			
305	312	Red Bed			

REMARKS:

I hereby certify that this well was drilled by me (or under my supervision), and that each and all of the statements herein are true to the best of my knowledge and belief.

Driller Bud Gibbons Address Plainview Texas Date Drilled 4-3-1969

DESCRIPTION OF WELL AND PRODUCTION EQUIPMENT

(This Does Not Mean Testing or Development Pump)

- Casing: new, used, gas line or shop made. Diameter 16 in Total casing length 313 ft.
- Casing perforations: from 250 ft. to 305 ft. Size 1/4 Number of rows 6
- Pump Column: Size 6 in. Column, shaft length 234 ft. Suction pipe size 6 in. Suction pipe length 2 ft.
- Pump bowls: Size 10" Number of stages 7 Pump discharge pipe: Size 6" in.
- Depth to water level 200 ft. Pump yield 500 GPM. Pumping level: 265 ft.
- Power Unit: Electrical, Natural Gas, Butane, Other _____ Horsepower 56

Signature _____ LANDOWNER OR AGENT TITLE ADDRESS

07-56-604

TEXAS WATER DEVELOPMENT BOARD
WELL SCHEDULE

Aquifer _____ Field No. _____
Owner's Well No. _____

UU 07 56 611
State Well No. Potter
County _____

1. Location: NE 1/4 NE 1/4 Sec. 14S, Block 9, Survey B.S. & F.

			6

2. Owner: Georgianne Menke Address: Amarillo, Texas

Tenant: _____ Address: _____

Driller: _____ Address: _____

3. Elevation of LSD is 3805 ft. above msl, determined by 7 1/2 Min. Taps

4. Drilled: 19 ft. Mess. _____ Dug, Cable Tool, Rotary, _____

5. Depth: Rept. _____ ft. Mess. _____ ft.

6. Completion: Open Hole, Straight Wall, Underreamed, Gravel Packed _____

7. Pump: Mfr. Wintroath Type Turbine
No. Stages _____, Bore Dia. _____ in., Setting _____ ft.
Column Dia. 6 in., Length Tailpipe _____ ft.

8. Motor: Fuel NG Make & Model Chrysler Ind. HP. 70 Gh

9. Yield: Flow _____ gpm, Pump _____ gpm, Mess., Rept., Est. _____

10. Performance Test: Date _____ Length of Test _____ Made by _____

Static Level _____ ft. Pumping Level _____ ft. Drawdown _____ ft.

Production _____ gpm Specific Capacity _____ gpm/ft.

11. Water Level: _____ ft. rept. _____ 19 above _____ which is _____ ft. above surface.
_____ ft. rept. _____ 19 above _____ which is _____ ft. above surface.
_____ ft. rept. _____ 19 above _____ which is _____ ft. above surface.
_____ ft. rept. _____ 19 above _____ which is _____ ft. above surface.

12. Use: Dow., Stock, Public Supply, Ind. Irr. Waterflooding, Observation, Not Used.

13. Quality: (Remarks on taste, odor, color, etc.) _____

Temp. _____ °F, Date sampled for analysis _____ Laboratory _____

Temp. _____ °F, Date sampled for analysis _____ Laboratory _____

Temp. _____ °F, Date sampled for analysis _____ Laboratory _____

14. Other data available as circled: Driller's Log, Radioactivity Log, Electric Log,
Formation Samples, Pumping Test,

15. Record by: D. Müller Date 3-7-1972

Source of Data Obs

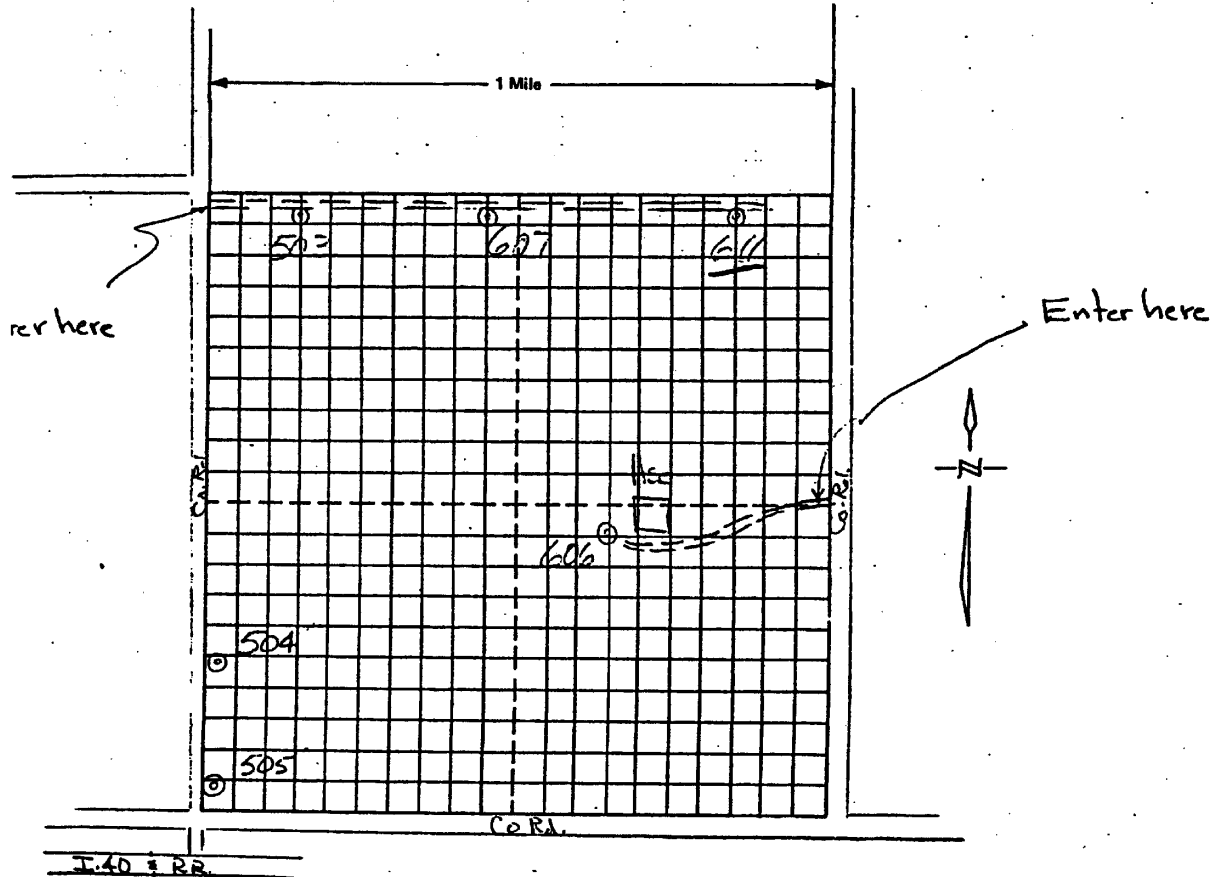
16. Remarks: Access W-side Top conc. blk

CASING & BLANK PIPE			
Cemented From		ft. to	
Diam. (in.)	Type	Setting, ft.	
		from	to

WELL SCREEN			
Screen Openings			
Diam. (in.)	Type	Setting, ft.	
		from	to

WATER WELL LOCATION SKETCH
TEXAS WATER DEVELOPMENT BOARD
GROUND WATER DIVISION

Section 145 in Block 9
Potter County
2 1/2-minute Quadrangle 5 E 6 in
7 1/2-minute Quadrangle 56
Sketch by D. Müller Date 3-7-72



shknd 1.0 mi. W

TWDBE-GW-116
11 Copies

Well No. 07 . 56 . 611

APPENDIX B

SLUG TESTING DATA AND CALCULATIONS

HDR Engineering, Inc.

HDR

Project	City of Amarillo MSWLF	Computed	BAm	Date	10/19/11
Subject	In-situ Permeability Calculations	Checked		Date	
Task	Summary	Sheet	1	Of	1

	<u>B:R</u>	<u>Hurstler</u>	<u>Equilibrium Value</u>
MW-2	6.58×10^{-4} cm/sec	1.32×10^{-3} cm/sec	3.34×10^{-3} cm
MW-3	7.24×10^{-4} cm/sec	1.80×10^{-4} cm/sec	4.4×10^{-4} cm
MW-6	1.35×10^{-3} cm/sec	1.33×10^{-3} cm/sec	3.3×10^{-3} cm/sec
P-1	1.47×10^{-3} cm/sec	3.77×10^{-2} cm/sec	--
P-2	1.25×10^{-3} cm/sec	1.03×10^{-3} cm/sec	--
P-3	1.09×10^{-3} cm/sec	4.28×10^{-3} cm/sec	3.77×10^{-3} cm

Average of B:R and Hurstler

MW-2	9.89×10^{-4} cm/sec
MW-3	4.52×10^{-4} cm/sec
MW-6	1.34×10^{-3} cm/sec
P-1	1.96×10^{-2} cm/sec
P-2	1.14×10^{-3} cm/sec
P-3	2.69×10^{-3} cm/sec

HDR Engineering, Inc.



Project	City of Amarillo MSWLF	Computed	BAM	Date	10/19/92
Subject	In-situ Permeability Calculations	Checked		Date	
Task	Bouwer and Rice Method	Sheet	1	Of	2

Static W.L. 219.1

MW-2

$$K = \frac{r_c^2 \ln(R_e/r_w)}{2Lt} \ln \frac{y_0}{y_t}$$

- K = hydraulic conductivity, cm/sec
- r_c = radius of well casing, cm
- R_e = effective radius of influence
- r_w = radius of Boring, cm
- L = length of screen or saturated thickness if entire screen is not saturated, cm
- t = selected time from time/drawdown semi-log plot
- y₀ = initial drawdown at time t = 0, sec
- y_t = drawdown at time t, sec

- R_w = 5-inches = 0.417 12.7 cm/sec
- r_c = 8-inches = 0.417 12.7 cm/sec
- L = 40ft = 1219.2 cm
- y₀ = 4.90 ft =
- y_t = 7.95 ft =
- t = 60 sec

$$\ln \frac{R_e}{r_w} = \left[\frac{1.1}{\ln(H/r_w)} + \frac{C}{L/r_w} \right]^{-1}$$

$$\frac{1.1}{\ln(26/0.417)} + \frac{3.9}{40/0.417}$$

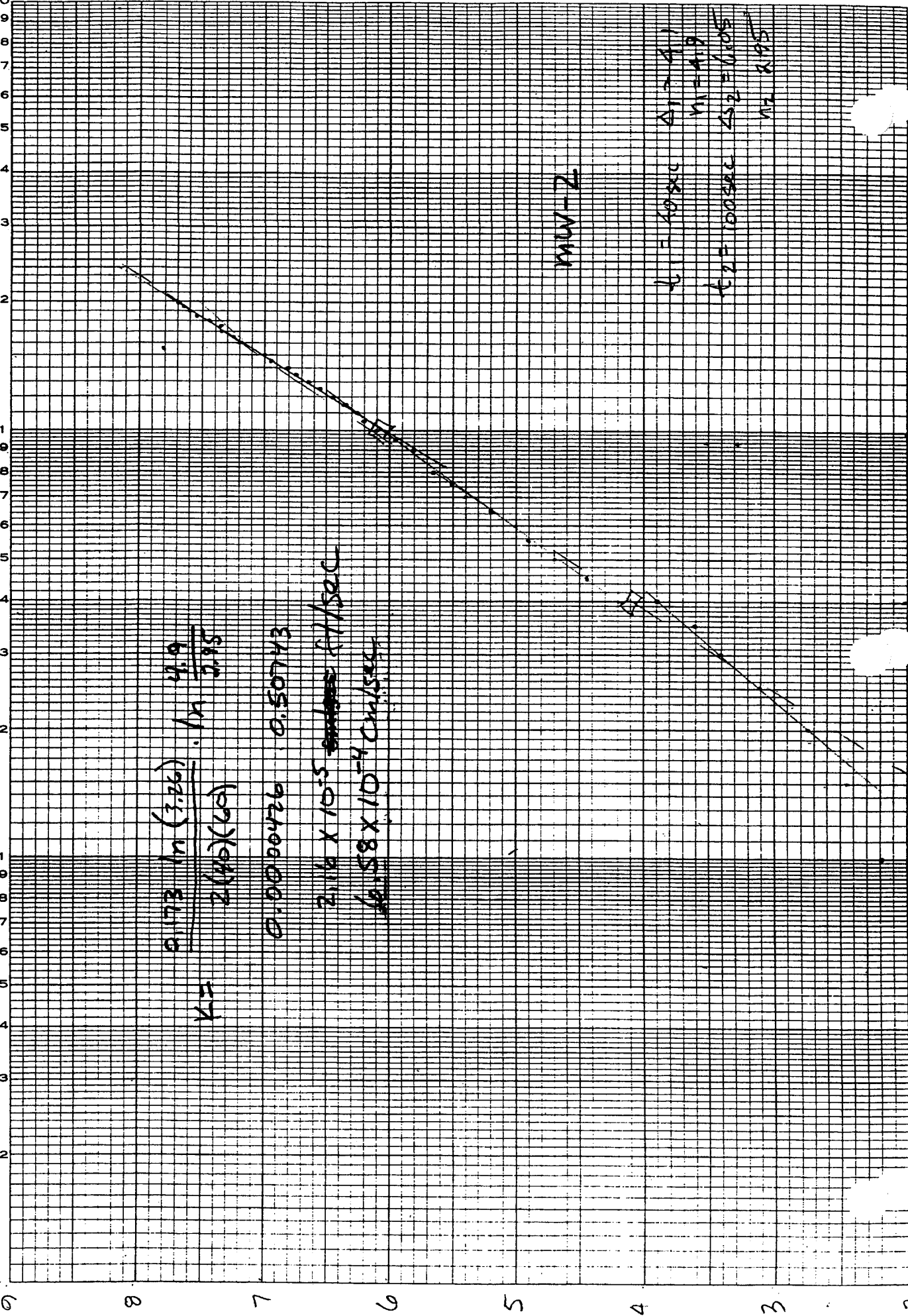
$$\frac{1.1}{12.7} + \frac{3.9}{1219.2/12.7}$$

$$= \frac{0.266}{1.535} + 0.041$$

$$= 3.26$$

log time sec

1000
900
800
700
600
500
400
300
200
100
10
1



CITY OF AMARILLO
MUNICIPAL SOLID WASTE LANDFILL
PERMIT NO. 73

SLUG TEST
RECOVERY

WELL NO.	STATIC WATER ELEV.,FT	TIME SEC	WATER LEVEL, FT	H/Ho	WATER ELEV.,FT	TIME SEC	WATER LEVEL, FT	H/Ho	WATER ELEV.,FT
			217.15						
MW-2	3590.64	0	228.00		3581.89	215	220.20	7.80	3589.69
		5	226.20	1.80	3583.69	220	220.15	7.85	3589.74
		10	225.80	2.20	3584.09	225	220.15	7.85	3589.74
		15	225.55	2.45	3584.34	230	220.10	7.90	3589.79
		20	225.25	2.75	3584.64	235	220.05	7.95	3589.84
		25	224.90	3.10	3584.99	240	220.00	8.00	3589.89
		30	224.60	3.40	3585.29	245	220.00	8.00	3589.89
		35	224.40	3.60	3585.49	250	219.95	8.05	3589.94
		40	224.10	3.90	3585.79	255	219.95	8.05	3589.94
		45	223.55	4.45	3586.34	260	219.90	8.10	3589.99
		55	223.30	4.70	3586.59	265	219.90	8.10	3589.99
		60	223.10	4.90	3586.79	270	219.85	8.15	3590.04
		65	223.00	5.00	3586.89	275	219.80	8.20	3590.09
		70	222.80	5.20	3587.09	280	219.80	8.20	3590.09
		75	222.60	5.40	3587.29	285	219.80	8.20	3590.09
		80	222.50	5.50	3587.39	290	219.80	8.20	3590.09
		85	222.35	5.65	3587.54	295	219.80	8.20	3590.09
		90	222.20	5.80	3587.69	300	219.75	8.25	3590.14
		95	222.05	5.95	3587.84	305	219.75	8.25	3590.14
		100	221.90	6.10	3587.99	310	219.70	8.30	3590.19
		105	221.80	6.20	3588.09	315	219.70	8.30	3590.19
		110	221.75	6.25	3588.14	320	219.70	8.30	3590.19
		115	221.65	6.35	3588.24	325	219.70	8.30	3590.19
		120	221.55	6.45	3588.34	330	219.65	8.35	3590.24
		125	221.45	6.55	3588.44	335	219.65	8.35	3590.24
		130	221.35	6.65	3588.54	340	219.65	8.35	3590.24
		135	221.25	6.75	3588.64	345	219.65	8.35	3590.24
		140	221.20	6.80	3588.69	350	219.60	8.40	3590.29
		145	221.05	6.95	3588.84	355	219.60	8.40	3590.29
		150	221.00	7.00	3588.89	360	219.60	8.40	3590.29
		155	220.19	7.81	3589.7	365	219.60	8.40	3590.29
		160	220.80	7.20	3589.09	370	219.60	8.40	3590.29
		165	220.75	7.25	3589.14	375	219.55	8.45	3590.34
		170	220.65	7.35	3589.24	380	219.55	8.45	3590.34
		175	220.65	7.35	3589.24	385	219.55	8.45	3590.34
		180	220.55	7.45	3589.34	390	219.55	8.45	3590.34
		185	220.45	7.55	3589.44	395	219.55	8.45	3590.34
		190	220.40	7.60	3589.49	400	219.55	8.45	3590.34
		195	220.35	7.65	3589.54	405	219.55	8.45	3590.34
		200	220.30	7.70	3589.59	410	219.55	8.45	3590.34
		205	220.30	7.70	3589.59	415	219.55	8.45	3590.34
		210	220.20	7.80	3589.69	420	219.55	8.45	3590.34

HDR Engineering, Inc.

HDR

Project	City of Amarillo MSWLF	Computed	BAM	Date	10/11/17
Subject	In-Situ Permeability Calculations	Checked		Date	
Task	Bowser and Rice Method	Sheet	1	Of	3

MW-3

$$K = \frac{r_c^2 \ln(R_e/R_w)}{2Lt} \ln \frac{Y_0}{Y_t}$$

$$R_w = 0.417$$

$$r_c = 0.417$$

$$L = 40 \text{ ft}$$

$$Y_0 = 11.10 \text{ ft}$$

$$Y_t = 4.70 \text{ ft}$$

$$t = 100 \text{ sec}$$

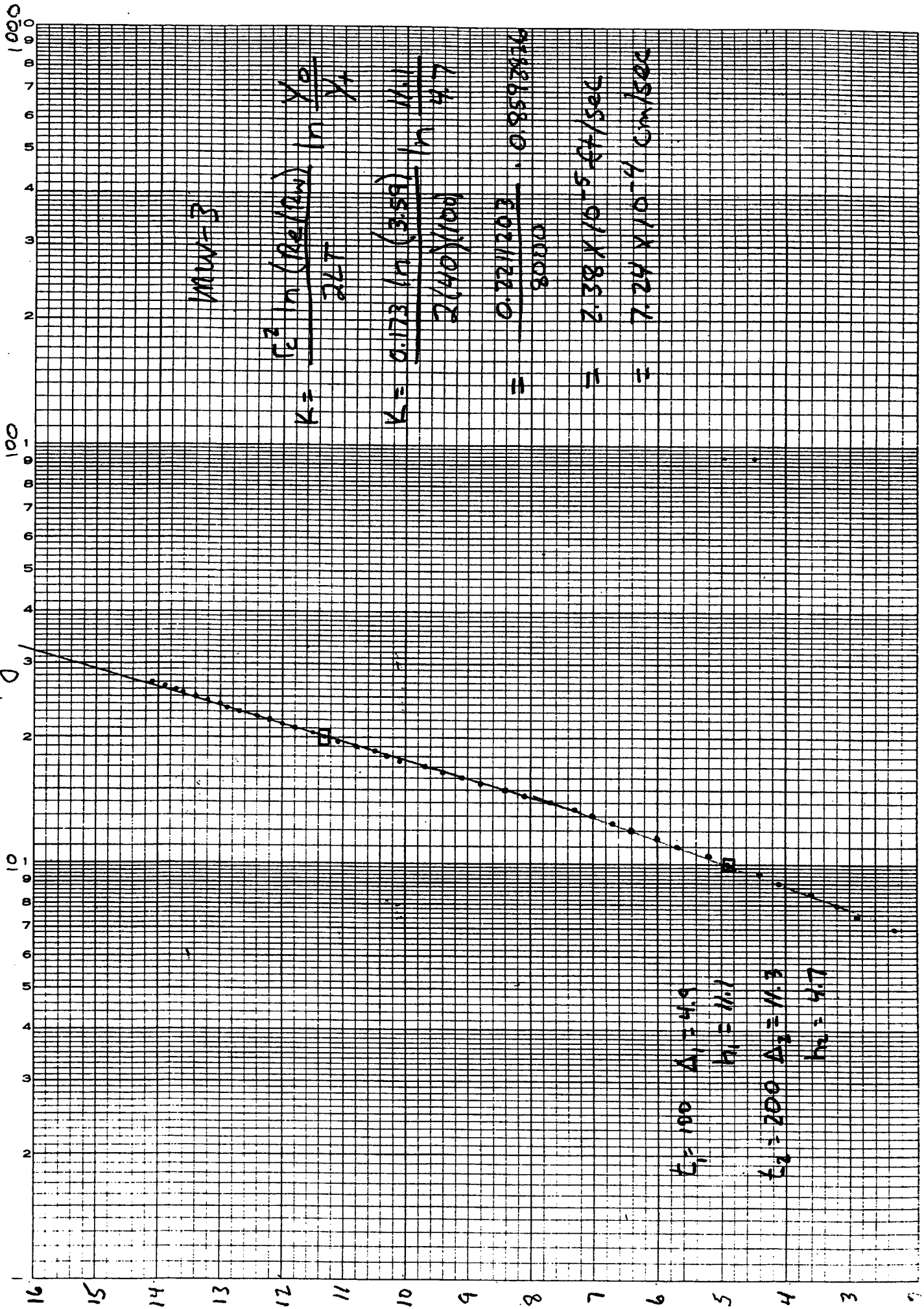
$$\ln R_e/r_w = \left[\frac{1.1}{\ln(H/r_w)} + \frac{C}{L/r_w} \right]^{-1}$$

$$\frac{1.1}{\ln(43.35/0.417)} + \frac{3.9}{40/0.417}^{-1}$$

$$= 0.237 + 0.041^{-1}$$

$$= 3.59$$

log time sec



CITY OF AMARILLO
MUNICIPAL SOLID WASTE LANDFILL
PERMIT NO. 73

SLUG TEST
RECOVERY

WELL NO.	STATIC WATER ELEV.,FT	TIME SEC	WATER LEVEL, FT	H/Ho	WATER ELEV.,FT	TIME SEC	WATER LEVEL,FT	H/Ho	WATER ELEV.,FT
MW-3	3589.16	0				245	212.1	13.20	3580.71
		5	225.3		3567.51	250	211.9	13.40	3580.91
		10	224.8	0.50	3568.01	255	211.7	13.60	3581.11
		15	224.8	0.50	3568.01	260	211.6	13.70	3581.21
		20	226.4	-1.10	3566.41	265	211.4	13.90	3581.41
		25	226.4	-1.10	3566.41	270	211.2	14.10	3581.61
		30	226.0	-0.70	3566.81	275	211.1	14.20	3581.71
		35	225.6	-0.30	3567.21	280	210.8	14.50	3582.01
		40	225.2	0.10	3567.61	285	210.7	14.60	3582.11
		45	225.0	0.30	3567.81	290	210.6	14.70	3582.21
		55	224.5	0.80	3568.31	300	210.4	14.90	3582.41
		60	224.1	1.20	3568.71	310	210.1	15.20	3582.71
		65	223.5	1.80	3569.31	320	209.9	15.40	3582.91
		70	223.0	2.30	3569.81	330	209.7	15.60	3583.11
		75	222.4	2.90	3570.41	340	209.4	15.90	3583.41
		80	222.1	3.20	3570.71	350	209.2	16.10	3583.61
		85	221.7	3.60	3571.11	360	208.9	16.40	3583.91
		90	221.2	4.10	3571.61	370	208.8	16.50	3584.01
		95	220.9	4.40	3571.91	380	208.5	16.80	3584.31
		100	220.4	4.90	3572.41	390	208.4	16.90	3584.41
		105	220.1	5.20	3572.71	400	208.1	17.20	3584.71
		110	219.6	5.70	3573.21	410	207.9	17.40	3584.91
		115	219.3	6.00	3573.51	420	207.8	17.50	3585.01
		120	218.9	6.40	3573.91	430	207.4	17.90	3585.41
		125	218.6	6.70	3574.21	440	207.3	18.00	3585.51
		130	218.3	7.00	3574.51	450	207.2	18.10	3585.61
		135	218.0	7.30	3574.81	460	207.0	18.30	3585.81
		140	217.6	7.70	3575.21	470	206.8	18.50	3586.01
		145	217.2	8.10	3575.61	480	206.6	18.70	3586.21
		150	216.9	8.40	3575.91	490	206.5	18.80	3586.31
		155	216.5	8.80	3576.31	500	206.3	19.00	3586.51
		160	216.2	9.10	3576.61	510	206.2	19.10	3586.61
		165	215.9	9.40	3576.91	520	206.1	19.20	3586.71
		170	215.6	9.70	3577.21	530	205.9	19.40	3586.91
		175	215.2	10.10	3577.61	540	205.8	19.50	3587.01
		180	215.0	10.30	3577.81	550	205.7	19.60	3587.11
		185	214.8	10.50	3578.01	560	205.6	19.70	3587.21
		190	214.5	10.80	3578.31	570	205.5	19.80	3587.31
		195	214.2	11.10	3578.61	580	205.4	19.90	3587.41
		200	214.0	11.30	3578.81	590	205.3	20.00	3587.51
		205	213.8	11.50	3579.01	600	205.2	20.10	3587.61
		210	213.5	11.80	3579.31	610	205.1	20.20	3587.71
		215	213.3	12.00	3579.51	620	205.1	20.20	3587.71
		220	213.1	12.20	3579.71	630	205.0	20.30	3587.81
		225	212.9	12.40	3579.91	640	204.9	20.40	3587.91
		230	212.6	12.70	3580.21	650	204.8	20.50	3588.01
		235	212.4	12.90	3580.41	660	204.8	20.50	3588.01
		240	212.3	13.00	3580.51	670	204.7	20.60	3588.11

HDR Engineering, Inc.

HDR

Project	City of Amarillo MSWLF	Computed	BAM	Date	10/19/94
Subject	In-situ Permeability Calculations	Checked		Date	
Task	Bowser and Rice Method	Sheet	1	Of	3

MW-6

$$K = \frac{r_c^2 \ln(R_e/R_w)}{2LT} \ln \frac{Y_0}{Y_t}$$

$$R_w = 0.417$$

$$r_c = 0.417$$

$$L = 40$$

$$Y_0 = 4.2$$

$$Y_t = 1.5$$

$$t = 60$$

$$\ln R_e/R_w = \left[\frac{1.1}{\ln(27.15/0.417)} + \frac{3.9}{40/0.417} \right]^{-1}$$

$$= 0.263 + 0.041$$

$$= 3.29$$

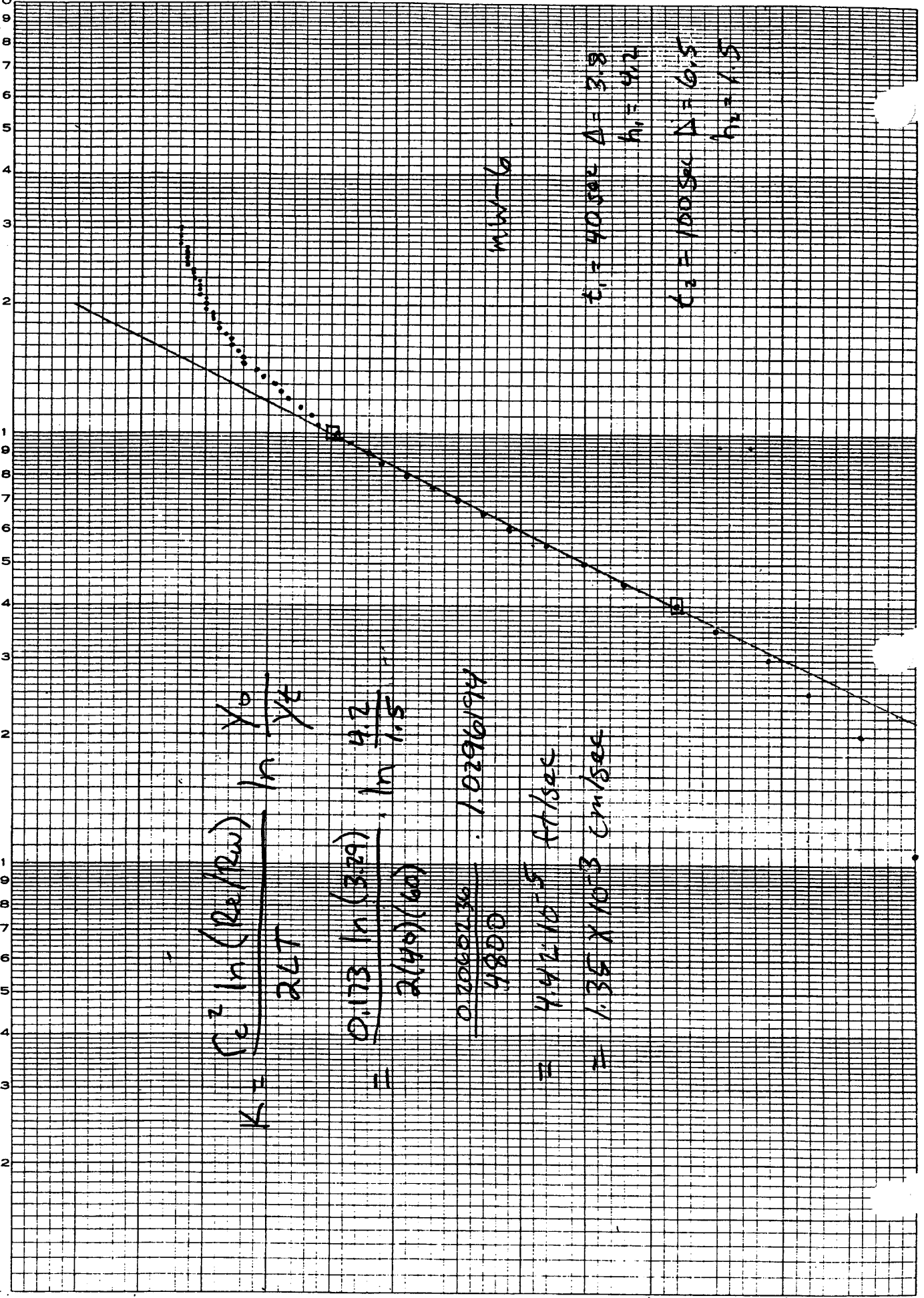
log time sec

1000

100

10

1



$$K = \frac{e^2 \ln(R_2/R_1)}{2LT} \ln \frac{Y_0}{Y_1}$$

$$= \frac{0.173 \ln(379)}{2(40)(60)} \ln \frac{9.2}{1.5}$$

$$= \frac{0.0000136}{4800} \cdot 1.0296194$$

$$= 4.92 \times 10^{-5} \text{ ft/sec}$$

$$= 1.38 \times 10^{-3} \text{ cm/sec}$$

MIN - 6

$$t_1 = 40 \text{ sec } \Delta = 3.8$$

$$h_1 = 402$$

$$t_2 = 100 \text{ sec } \Delta = 6.5$$

$$h_2 = 1.5$$

CITY OF AMARILLO
MUNICIPAL SOLID WASTE LANDFILL
PERMIT NO. 73

SLUG TEST
RECOVERY

WELL NO.	STATIC WATER ELEV.,FT	TIME SEC	WATER LEVEL,FT	H/Ho	WATER ELEV.,FT	TIME SEC	WATER LEVEL,FT	H/Ho	WATER ELEV.,FT
MW-6	3601.52	5	157.00		3593.72	155	149.75	7.25	3600.97
		10	156.90	0.10	3593.82	160	149.70	7.30	3601.02
		15	155.00	2.00	3595.72	165	149.70	7.30	3601.02
		20	154.60	2.40	3596.12	170	149.65	7.35	3601.07
		25	154.20	2.80	3596.52	175	149.60	7.40	3601.12
		30	153.90	3.10	3596.82	180	149.60	7.40	3601.12
		35	153.50	3.50	3597.22	185	149.55	7.45	3601.17
		40	153.20	3.80	3597.52	190	149.55	7.45	3601.17
		45	152.80	4.20	3597.92	195	149.50	7.50	3601.22
		50	152.50	4.50	3598.22	200	149.50	7.50	3601.22
		55	152.20	4.80	3598.52	205	149.50	7.50	3601.22
		60	151.90	5.10	3598.82	210	149.45	7.55	3601.27
		65	151.70	5.30	3599.02	215	149.45	7.55	3601.27
		70	151.50	5.50	3599.22	220	149.45	7.55	3601.27
		75	151.30	5.70	3599.42	225	149.45	7.55	3601.27
		80	151.10	5.90	3599.62	230	149.40	7.60	3601.32
		85	150.90	6.10	3599.82	235	149.40	7.60	3601.32
		90	150.80	6.20	3599.92	240	149.40	7.60	3601.32
		95	150.65	6.35	3600.07	245	149.35	7.65	3601.37
		100	150.55	6.45	3600.17	250	149.35	7.65	3601.37
		105	150.40	6.60	3600.32	255	149.35	7.65	3601.37
		110	150.35	6.65	3600.37	260	149.35	7.65	3601.37
		115	150.25	6.75	3600.47	265	149.35	7.65	3601.37
		120	150.15	6.85	3600.57	270	149.35	7.65	3601.37
		125	150.10	6.90	3600.62	275	149.30	7.70	3601.42
		130	150.05	6.95	3600.67	280	149.30	7.70	3601.42
		135	149.95	7.05	3600.77	285	149.30	7.70	3601.42
		140	149.90	7.10	3600.82	290	149.30	7.70	3601.42
		145	149.80	7.20	3600.92	295	149.30	7.70	3601.42
		150	149.80	7.20	3600.92	300	149.30	7.70	3601.42

Computation

HDR

Project	City of Amarillo MSWLF.	Computed	BAM	Date	
Subject	In-situ Permeability Calculation	Checked		Date	
Task	Bowmer and Rice method	Sheet	1	Of	1

P-1

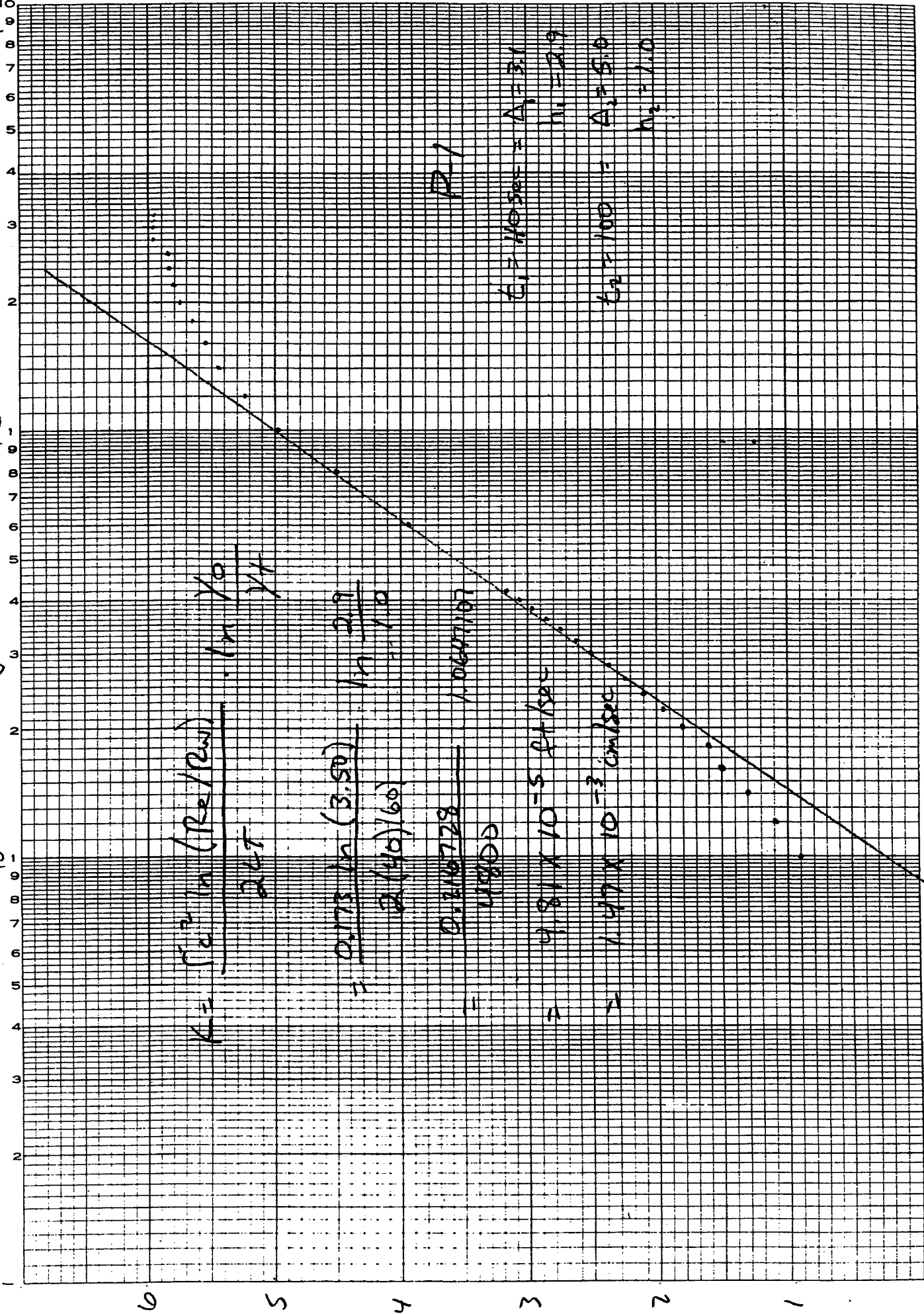
$$K = \frac{r_c^2 \ln(R_e/R_w)}{2LT} \ln \frac{Y_0}{Y_t}$$

$$\begin{aligned} R_w &= 0.417 \text{ ft} \\ r_c &= 0.417 \text{ ft} \\ L &= 40 \text{ ft} \\ Y_0 &= 2.9 \\ Y_t &= 1.0 \end{aligned}$$

$$\begin{aligned} \ln R_e/r_w &= \left[\frac{1.1}{\ln(H/r_w)} + \frac{L}{L/r_w} \right]^{-1} \\ &= \frac{1.1}{\ln(37.23/0.417)} + \frac{3.90}{40/0.417}^{-1} \\ &= 0.2448916 + 0.0406575^{-1} \\ &= 3.50 \end{aligned}$$

time sec

1000
100
10
1



$$K = \frac{(\sigma^2 \ln(R_e/R_w))}{2ct} \cdot \ln \frac{y_0}{y_1}$$

$$= \frac{0.175 \ln(3.50)}{2(40)(60)} \ln \frac{2.9}{1.0}$$

$$= \frac{0.216728}{4800} \cdot 1.0607107$$

$$= 4.81 \times 10^{-5} \text{ ft/sec}$$

$$\approx 1.47 \times 10^{-3} \text{ cm/sec}$$

R-1

$$t_1 = 16.5 \text{ sec} = A_1 = 3.1$$

$$n_1 = 2.9$$

$$t_2 = 100 = A_2 = 5.0$$

$$n_2 = 1.0$$

100
10

SE2000
 Environmental Logger
 10/07 10:11

Unit# 9600 Test 4

Setups: INPUT 1

 Type Level (F)
 Mode TOC
 I.D. P1

Static W.L. = 997.240

Reference 1000.00 2,000
 SG 1.000
 Linearity 0.011
 Scale factor 10.095
 Offset 0.030
 Delay mSEC 50.000

Step 0 09/21 18:02:37

Elapsed Time	INPUT	1

0.0000	1003.16	
0.0333 2	1003.17	
0.0666 4	1002.90	
0.1000 6	1002.66	
0.1333 8	1002.45	
0.1666 10	1002.26	
0.2000 12	1002.05	
0.2333 14	1001.86	
0.2666 16	1001.68	
0.3000 18	1001.52	
0.3333 20	1001.36	
0.3666 22	1001.21	
0.4000 24	1001.06	
0.4333 26	1000.92	
0.4666 28	1000.79	
0.5000 30	1000.66	
0.5333 32	1000.54	
0.5666 34	1000.41	
0.6000 36	1000.30	
0.6333 38	1000.19	
0.6666 40	1000.08	

W.L.	H/H ₀

996.84	
996.83	0.01
997.10	0.26
997.34	0.50
997.55	0.71
997.74	0.90
997.95	1.11
998.14	1.30
998.32	1.48
998.42	1.58
998.64	1.80
998.79	1.95
998.94	2.10
999.08	2.24
999.21	2.37
999.34	2.50
999.46	2.62
999.59	2.75
999.70	2.86
999.81	2.97
999.92	3.08

0.7000	42	999.980	1000.02	3.18
0.7333	44	999.875		
0.7666	46	999.783		
0.8000	48	999.691		
0.8333	50	999.605		
0.8666	52	999.516		
0.9000	54	999.443		
0.9333	56	999.373		
0.9666	58	999.296		
1.0000	60	999.226	1000.774	3.934
1.0333	62	999.153		
1.0666	64	999.089		
1.1000	66	999.038		
1.1333	68	998.972		
1.1666	70	998.911		
1.2000	72	998.854		
1.2333	74	998.797		
1.2666	76	998.749		
1.3000	78	998.692		
1.3333	80	998.644	1001.356	4.516
1.3666	82	998.596		
1.4000	84	998.552		
1.4333	86	998.507		
1.4666	88	998.469		
1.5000	90	998.421		
1.5333	92	998.386		
1.5666	94	998.341		
1.6000	96	998.306		
1.6333	98	998.271		
1.6666	100	998.233	1001.767	4.927
1.7000	102	998.198		
1.7333	104	998.166		
1.7666	106	998.135		
1.8000	108	998.106		
1.8333	110	998.074		
1.8666	112	998.046		
1.9000	114	998.020		
1.9333	116	997.995		
1.9666	118	997.966		
2.0000	120	997.940	1002.06	5.22
2.0333	122	997.921		
2.0666	124	997.899		
2.1000	126	997.877		
2.1333	128	997.848		
2.1666	130	997.820		

2.2000	132	997.797		
2.2333	134	997.781		
2.2666	136	997.759		
2.3000	138	997.743		
2.3333	140	997.718	1002.282	5.472
2.3666	142	997.708		
2.4000	144	997.692		
2.4333	146	997.673		
2.4666	148	997.657		
2.5000	150	997.644		
2.5333	152	997.629		
2.5666	154	997.616		
2.6000	156	997.603		
2.6333	158	997.594		
2.6666	160	997.574	1002.426	5.586
2.7000	162	997.562		
2.7333	164	997.552		
2.7666	166	997.543		
2.8000	168	997.530		
2.8333	170	997.520		
2.8666	172	997.508		
2.9000	174	997.498		
2.9333	176	997.489		
2.9666	178	997.482		
3.0000	180	997.473	1002.527	5.687
3.0333	182	997.463		
3.0666	184	997.457		
3.1000	186	997.447		
3.1333	188	997.441		
3.1666	190	997.434		
3.2000	192	997.425		
3.2333	194	997.415		
3.2666	196	997.412		
3.3000	198	997.406		
3.3333	200	997.399	1002.601	5.761
3.3666	202	997.393		
3.4000	204	997.390		
3.4333	206	997.380		
3.4666	208	997.374		
3.5000	210	997.371		
3.5333	212	997.364		
3.5666	214	997.358		
3.6000	216	997.355		
3.6333	218	997.352		
3.6666	220	997.342	1002.658	5.819

3.7000	222	997.336		
3.7333	224	997.336		
3.7666	226	997.329		
3.8000	228	997.326		
3.8333	230	997.323		
3.8666	232	997.320		
3.9000	234	997.313		
3.9333	236	997.310		
3.9666	238	997.307		
4.0000	240	997.304	1002.696	5.856
4.0333	242	997.301		
4.0666	244	997.298		
4.1000	246	997.294		
4.1333	248	997.291		
4.1666	250	997.288		
4.2000	252	997.285		
4.2333	254	997.282		
4.2666	256	997.282		
4.3000	258	997.275		
4.3333	260	997.275	1002.725	5.885
4.3666	262	997.272		
4.4000	264	997.269		
4.4333	266	997.266		
4.4666	268	997.266		
4.5000	270	997.263		
4.5333	272	997.263		
4.5666	274	997.256		
4.6000	276	997.259		
4.6333	278	997.256		
4.6666	280	997.253	1002.747	5.907
4.7000	282	997.253		
4.7333	284	997.250		
4.7666	286	997.247		
4.8000	288	997.247		
4.8333	290	997.247		
4.8666	292	997.247		
4.9000	294	997.243		
4.9333	296	997.243		
4.9666	298	997.240		
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5.0666		997.237		
5.1000		997.237		
5.1333		997.234		
5.1666		997.234		

5.2000		997.234		
5.2333		997.231		
5.2666		997.231		
5.3000		997.231		
5.3333	320	997.228-	1002.772	5.932
5.3666		997.228		
5.4000		997.224		
5.4333		997.224		
5.4666		997.224		
5.5000		997.221		
5.5333		997.221		
5.5666		997.224		
5.6000		997.221		
5.6333		997.221		
5.6666	340	997.221	1002.779	5.939
5.7000		997.221		
5.7333		997.218		
5.7666		997.218		
5.8000		997.218		
5.8333		997.215		
5.8666		997.215		
5.9000		997.215		
5.9333		997.215		
5.9666		997.215		
6.0000	360	997.212	1002.788	5.948
6.0333		997.208		
6.0666		997.212		
6.1000		997.212		
6.1333		997.212		
6.1666		997.212		
6.2000		997.208		
6.2333		997.208		
6.2666		997.205		
6.3000		997.205		
6.3333	380	997.205	1002.795	5.955
6.3666		997.208		
6.4000		997.205		
6.4333		997.205		
6.4666		997.205		
6.5000		997.205		
6.5333		997.205		
6.5666		997.202		
6.6000		997.205		
6.6333		997.199		
6.6666	400	997.202	1002.798	5.958

6.7000	997.205			
6.7333	997.202			
6.7666	997.199			
6.8000	997.202			
6.8333	997.199			
6.8666	997.199			
6.9000	997.199			
6.9333	997.196			
6.9666	997.193			
7.0000	997.193	470	1982.807	5.967
7.0333	997.202			
7.0666	997.196			
7.1000	997.199			
7.1333	997.196			
7.1666	997.196			
7.2000	997.196			
7.2333	997.196			
7.2666	997.196			
7.3000	997.193			
7.3333	997.196			
7.3666	997.196			
7.4000	997.196			
7.4333	997.193			
7.4666	997.193			
7.5000	997.193			
7.5333	997.193			
7.5666	997.196			
7.6000	997.196			
7.6333	997.193			
7.6666	997.193			
7.7000	997.196			
7.7333	997.196			
7.7666	997.196			
7.8000	997.193			
7.8333	997.193			
7.8666	997.193			
7.9000	997.193			
7.9333	997.189			
7.9666	997.193			
8.0000	997.193			
8.0333	997.193			
8.0666	997.196			
8.1000	997.193			
8.1333	997.193			
8.1666	997.193			

8.2000	997.193
8.2333	997.193
8.2666	997.193
8.3000	997.193
8.3333	997.193
8.3666	997.193
8.4000	997.189
8.4333	997.193
8.4666	997.196
8.5000	997.193
8.5333	997.193
8.5666	997.189
8.6000	997.183
8.6333	997.193
8.6666	997.193
8.7000	997.193
8.7333	997.189
8.7666	997.193
8.8000	997.193
8.8333	997.193
8.8666	997.193
8.9000	997.193
8.9333	997.193
8.9666	997.193
9.0000	997.193
9.0333	997.193
9.0666	997.193
9.1000	997.193
9.1333	997.193
9.1666	997.193
9.2000	997.193
9.2333	997.193
9.2666	997.193
9.3000	997.193
9.3333	997.193
9.3666	997.189
9.4000	997.193
9.4333	997.193
9.4666	997.193
9.5000	997.193
9.5333	997.196
9.5666	997.193
9.6000	997.193
9.6333	997.193
9.6666	997.193

9.7000	997.193
9.7333	997.193
9.7666	997.193
9.8000	997.193
9.8333	997.193
9.8666	997.193
9.9000	997.193
9.9333	997.193
9.9666	997.193
10.0000	997.193
10.0333	997.193

HDR Engineering, Inc.



Project	City of Amarillo MSWLF	Computed	BPM	Date	10/19/
Subject	In-situ Permeability Calculations	Checked		Date	
Task	Boyer and Rice method	Sheet	1	Of	3

P-2

$$K = \frac{r_c^2 \ln(R_e/R_w)}{2LT} \cdot \ln \frac{y_0}{y_t}$$

- RW = 0.417
- r_c = 0.417
- L = 40'
- y₀ = 1.95
- y_t = 0.75
- t = 60

$$\begin{aligned} \ln R_e/R_w &= \left[\frac{1.1}{\ln(22.15/0.417)} + \frac{3.9}{40/0.417} \right]^{-1} \\ &= 0.263 + 0.041 \\ &= 3.28 \end{aligned}$$

log time sec

10 9 8 7 6 5 4 3 2 1 0

100 90 80 70 60 50 40 30 20 10 0

$$k = \frac{C_0^2 \ln(R_2/R_1)}{2.3T} \ln \frac{Y_0}{Y_4}$$

$$= \frac{0.178 \ln(3.28)}{2(40)(60)} \ln \frac{1.95}{0.75}$$

$$= \frac{0.2054969}{4800} = 0.9885 \times 10^{-5}$$

$$= 4.09 \times 10^{-5} \text{ ft/sec}$$

$$= 1.25 \times 10^{-3} \text{ cm/sec}$$

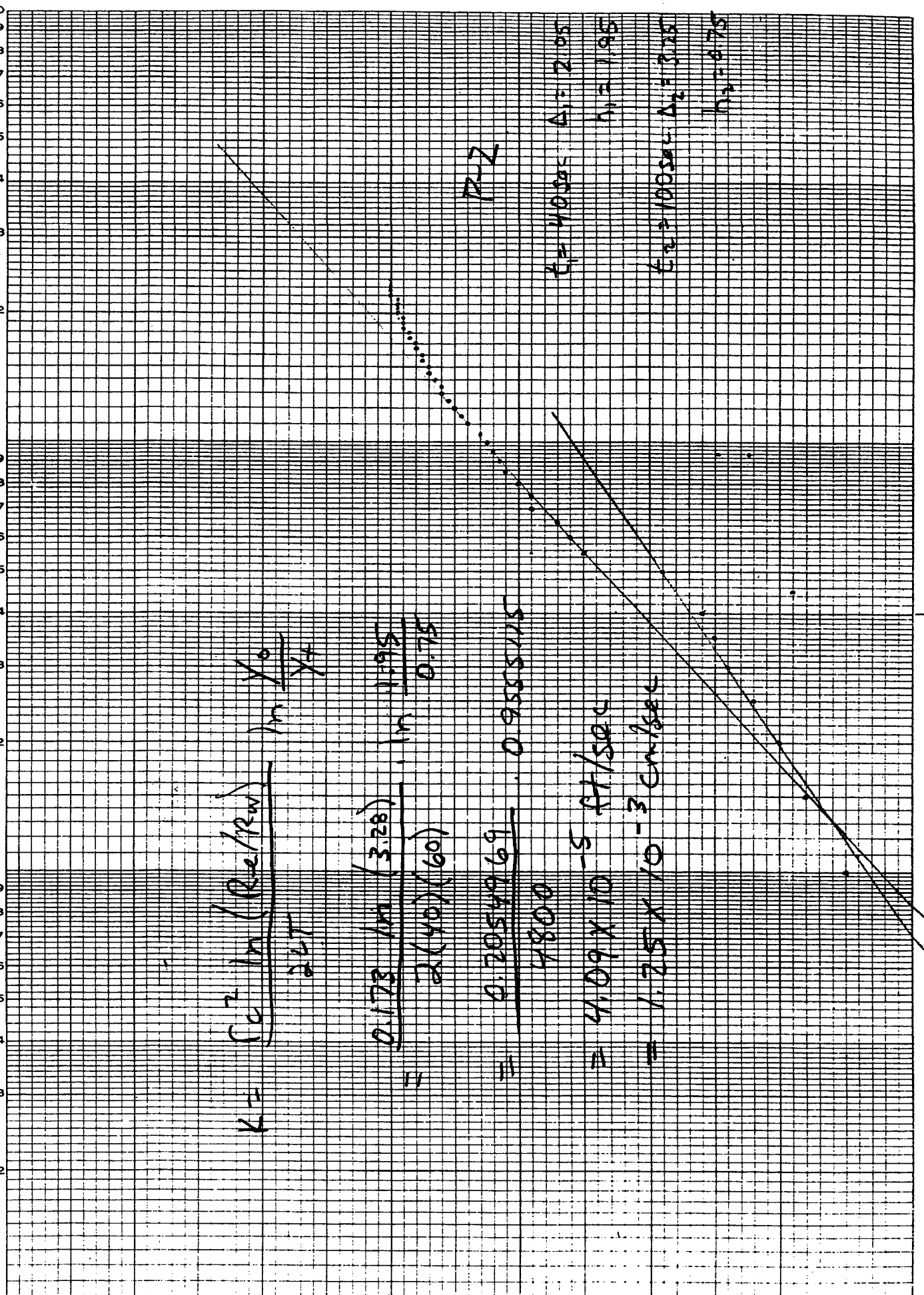
P-2

$t_1 = 40 \text{ sec}$ $\Delta_1 = 2.05$

$t_2 = 195$

$t_2 = 100 \text{ sec}$ $\Delta_2 = 3.28$

$t_3 = 675$



CITY OF AMARILLO
MUNICIPAL SOLID WASTE LANDFILL
PERMIT NO. 73

SLUG TEST
RECOVERY

STATIC WATER					SLUG TEST RECOVERY				
WELL NO.	ELEV.,FT	TIME SEC	WATER LEVEL,FT	H/Ho	WATER ELEV.,FT	TIME SEC	WATER LEVEL,FT	H/Ho	WATER ELEV.,FT
P-2	3595.17	0							
		5	207.40		3590.87	125	203.85	3.55	3594.42
		10	206.90	0.50	3591.37	130	203.80	3.60	3594.47
		15	206.60	0.80	3591.67	135	203.80	3.60	3594.47
		20	206.40	1.00	3591.87	140	203.75	3.65	3594.52
		25	206.20	1.20	3592.07	145	203.70	3.70	3594.57
		30	206.00	1.40	3592.27	150	203.70	3.70	3594.57
		35	205.90	1.50	3592.37	155	203.65	3.75	3594.62
		40	205.80	1.60	3592.47	160	203.65	3.75	3594.62
		45	206.50	0.90	3591.77	165	203.60	3.80	3594.67
		50	205.50	1.90	3592.77	170	203.60	3.80	3594.67
		55	204.90	2.50	3593.37	175	203.55	3.85	3594.72
		60	204.80	2.60	3593.47	180	203.55	3.85	3594.72
		65	204.70	2.70	3593.57	185	203.50	3.90	3594.77
		70	204.50	2.90	3593.77	190	203.50	3.90	3594.77
		75	204.50	2.90	3593.77	195	203.50	3.90	3594.77
		80	204.40	3.00	3593.87	200	203.45	3.95	3594.82
		85	204.30	3.10	3593.97	205	203.45	3.95	3594.82
		90	204.25	3.15	3594.02	210	203.45	3.95	3594.82
		95	204.20	3.20	3594.07	215	203.45	3.95	3594.82
		100	204.15	3.25	3594.12	220	203.40	4.00	3594.87
		105	204.10	3.30	3594.17	225	203.40	4.00	3594.87
		110	204.00	3.40	3594.27	230	203.40	4.00	3594.87
		115	203.95	3.45	3594.32	235	203.40	4.00	3594.87
		120	203.90	3.50	3594.37	240	203.40	4.00	3594.87

HDR Engineering, Inc.

HDR

Project	City of Amarillo MSWLF	Computed	BAM	Date	10/19/94
Subject	In-situ Permeability Calculations	Checked		Date	
Task	Bower and Rye Method	Sheet	1	Of	3

P-3

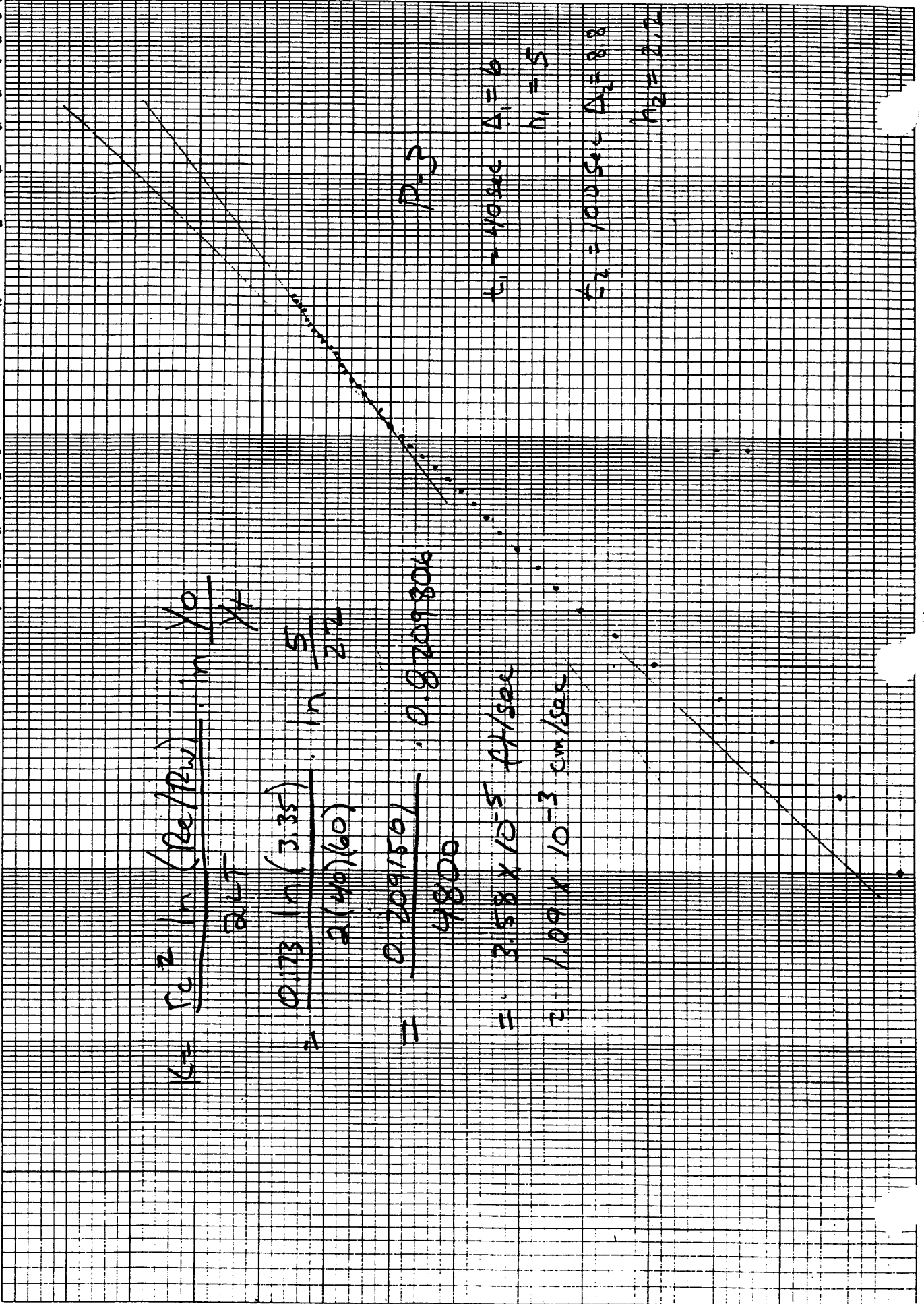
$$\begin{aligned}
 R_w &= 0.417 \\
 r_c &= 0.417 \\
 L &= 40 \text{ ft} \\
 Y_0 &= 5 \text{ ft} \\
 Y_t &= 2.2 \text{ ft} \\
 t &= 60 \text{ Sec}
 \end{aligned}$$

$$K = \frac{r_c^2 \ln(R_e/R_w) \cdot \ln \frac{Y_0}{Y_t}}{2LT}$$

$$\begin{aligned}
 \ln R_e/R_w & \left[\frac{1.1}{\ln(29.90/0.417)} + \frac{3.9}{40/0.417} \right]^{-1} \\
 &= 0.257 + 0.041 \\
 &= 3.35
 \end{aligned}$$

log time sec

1000
100
10
1



$$k = \frac{r_0^2 \ln(R_0/R_w)}{2.3T} \cdot \ln \frac{y_0}{y}$$

$$= \frac{0.173 \ln(3.35)}{2(40)(60)} \cdot \ln \frac{5}{2.0}$$

$$= \frac{0.2091507}{4800} \cdot 0.8209806$$

$$= 3.58 \times 10^{-5} \text{ ft/sec}$$

$$= 1.09 \times 10^{-3} \text{ cm/sec}$$

P=3

t₁ = 10 sec

n = 6

t₂ = 100 sec

n = 8

CITY OF AMARILLO
MUNICIPAL SOLID WASTE LANDFILL
PERMIT NO. 73

SLUG TEST
RECOVERY

WELL NO.	STATIC WATER ELEV.,FT	TIME SEC	WATER LEVEL,FT	H/Ho	WATER ELEV.,FT	TIME SEC	WATER LEVEL,FT	H/Ho	WATER ELEV.,FT
P-3	3599.61	0							
		5	158.10		3588.56	215	147.60	10.50	3599.06
		✓10	156.90	1.20	3589.76	220	147.55	10.55	3599.11
		✓15	156.00	2.10	3590.66	225	147.50	10.60	3599.16
		20	155.00	3.10	3591.66	230	147.50	10.60	3599.16
		25	154.20	3.90	3592.46	235	147.50	10.60	3599.16
		30	153.20	4.90	3593.46	240	147.45	10.65	3599.21
		35	152.60	5.50	3594.06	245	147.40	10.70	3599.26
		40	152.10	6.00	3594.56	250	147.40	10.70	3599.26
		45	151.70	6.40	3594.96	255	147.40	10.70	3599.26
		50	151.40	6.70	3595.26	260	147.40	10.70	3599.26
		55	151.10	7.00	3595.56	265	147.40	10.70	3599.26
		60	150.80	7.30	3595.86	270	147.35	10.75	3599.31
		65	150.60	7.50	3596.06	275	147.35	10.75	3599.31
		70	150.40	7.70	3596.26	280	147.35	10.75	3599.31
		75	150.20	7.90	3596.46	285	147.30	10.80	3599.36
		80	150.00	8.10	3596.66	290	147.30	10.80	3599.36
		85	149.80	8.30	3596.86	295	147.30	10.80	3599.36
		90	149.60	8.50	3597.06	300	147.25	10.85	3599.41
		95	149.40	8.70	3597.26	305	147.25	10.85	3599.41
		100	149.30	8.80	3597.36	310	147.25	10.85	3599.41
		105	149.10	9.00	3597.56	315	147.25	10.85	3599.41
		110	149.00	9.10	3597.66	320	147.25	10.85	3599.41
		115	148.95	9.15	3597.71	325	147.25	10.85	3599.41
		120	148.80	9.30	3597.86	330	147.20	10.90	3599.46
		125	148.70	9.40	3597.96	335	147.20	10.90	3599.46
		130	148.60	9.50	3598.06	340	147.20	10.90	3599.46
		135	148.50	9.60	3598.16	345	147.20	10.90	3599.46
		140	148.40	9.70	3598.26	350	147.20	10.90	3599.46
		145	148.35	9.75	3598.31	355	147.20	10.90	3599.46
		150	148.30	9.80	3598.36	360	147.20	10.90	3599.46
		155	148.25	9.85	3598.41	365	147.20	10.90	3599.46
		160	148.15	9.95	3598.51	370	147.20	10.90	3599.46
		165	148.05	10.05	3598.61	375	147.20	10.90	3599.46
		170	148.00	10.10	3598.66	380	147.15	10.95	3599.51
		175	147.90	10.20	3598.76	385	147.15	10.95	3599.51
		180	147.85	10.25	3598.81	390	147.15	10.95	3599.51
		185	147.80	10.30	3598.86	395	147.15	10.95	3599.51
		190	147.75	10.35	3598.91	400	147.15	10.95	3599.51
		195	147.75	10.35	3598.91	405	147.15	10.95	3599.51
		200	147.70	10.40	3598.96	410	147.15	10.95	3599.51
		205	147.65	10.45	3599.01	415	147.15	10.95	3599.51
		210	147.60	10.50	3599.06	420	147.15	10.95	3599.51

HDR Engineering, Inc.

HDR

Project	City of Amarillo MSWLF	Computed	BAM	Date	10/18/14
Subject	In-situ Field Permeability Calculations	Checked		Date	
Task	Hvorslev Method G	Sheet	1	Of	3

$$K_h = \frac{d^2 \cdot \ln\left(\frac{2mL}{D}\right)}{8 \cdot L \cdot T} \cdot \ln \frac{H_1}{H_2}$$

K_h = horizontal Hydraulic Conductivity, cm/sec
 d = diameter of standpipe, cm
 m = Transformation Ratio
 L = Length of intake area, cm
 D = Diameter of intake area, cm
 T = Time Lag, sec

MW-2

Screen (BGS) 205-245 4" 40'
 Filter Pack (BGS) 200-245
 Static Water Level 219.00 (9/20/94)

Parameters

$m = 3$
 $d = 10.16$ cm
 $D = 10.16$ cm
 $L = 1219.20$ cm
 $H_1 = \text{Drawdown } t_1$
 $H_2 = \text{Drawdown } t_2$

$$K_h = \frac{(10.16)^2 \cdot \ln\left(\frac{2(3)(1219.2)}{10.16}\right)}{8(1219.2)(10)} \cdot \ln \frac{9}{6.8}$$

$$\begin{aligned}
 t_1 &= 228.0 \\
 t_2 &= 225.80 \\
 &= \frac{103.23(6.58)}{97536} \cdot 0.280 \\
 &= 1.95 \times 10^{-3} \text{ cm/sec}
 \end{aligned}$$

$$\begin{aligned}
 t_1 &= 228.0 \\
 t_2 &= 224.60 \\
 K_h &= \frac{679.2534}{8(1219.2)(30)} \cdot \ln \frac{9}{5.6} \\
 &= \frac{679.2534}{292608} \cdot 0.474458 \\
 &= 1.10 \times 10^{-3} \text{ cm/sec}
 \end{aligned}$$

HDR Engineering, Inc.

HDR

Project	City of Amarillo MSWLF	Computed	BAM	Date	10/18/94
Subject	In-situ Field Permeability Calculations	Checked		Date	
Task	Hvorslev Method G	Sheet	2	Of	3

MW-2 Cont

$$t_1 = 228. \quad K_h = \frac{679.2534}{9753.6(60)} \cdot \ln \frac{9}{4.1}$$

$$t_2 = 223.10$$

$$= 0.0011607 \cdot 0.7862376$$

$$= 9.13 \times 10^{-4}$$

$$\text{Ave } K_h = 1.32 \times 10^{-3} \text{ cm/sec}$$

MW-3

Screen 207-247' (BGS) 4" 40'
 Filter Pack 200-247' (BGS)
 Static Water Level 203.65' BGS

Parameters

$m = 3$
 $d = 10.16 \text{ cm}$
 $D = 10.16 \text{ cm}$
 $L = 1291.20$
 $H_1 = \text{drawdown } t_1$
 $H_2 = \text{drawdown } t_2$

$$t_1 = 226.4$$

$$t_2 = 224.5$$

$$K_h = \frac{103.23(6.58)}{(9753.6)(240)} \cdot \ln \frac{22.75}{20.85}$$

$$= 0.0002902 \cdot 0.0872112$$

$$= 2.53 \times 10^{-5} \text{ cm/sec}$$

$$t_1 = 224.5$$

$$t_2 = 221.7$$

$$K_h = \frac{103.23(6.58)}{(9753.6)(160)} \cdot \ln \frac{20.85}{18.05}$$

$$= 0.0004353 \cdot 0.1442683$$

$$= 6.28 \times 10^{-5} \text{ cm/sec}$$

HDR Engineering, Inc.

HDR

Project	City of Amarillo MSWLF	Computed	BAM	Date	10/18/11
Subject	In-situ Field Permeability Calculations	Checked		Date	
Task		Sheet	3	Of	3

MW-3 Cont.

$$t_1 = 220.4$$

$$t_2 = 214.0$$

$$K_h = \frac{103.23(6.58)}{9753.6(100)} \cdot \ln \frac{16.75}{10.35}$$

$$= 0.0006964 \cdot 0.4814117$$

$$= 3.35 \times 10^{-4} \text{ cm/sec}$$

$$t_1 = 214$$

$$t_2 = 210.4$$

$$K_h = \frac{103.23(6.58)}{9753.6(100)} \cdot \ln \frac{10.35}{6.75}$$

$$= 0.0006964 \cdot 0.427444$$

$$= 2.97 \times 10^{-4} \text{ cm/sec}$$

$$\text{Average } K_h = 1.80 \times 10^{-4} \text{ cm/sec}$$

CITY OF AMARILLO
MUNICIPAL SOLID WASTE LANDFILL
PERMIT NO. 73

SLUG TEST
RECOVERY

WELL NO.	STATIC WATER ELEV.,FT	TIME SEC	WATER LEVEL, FT	H/Ho	WATER ELEV.,FT	TIME SEC	WATER LEVEL, FT	H/Ho	WATER ELEV.,FT
MW-2	3590.64	0	228.00		3581.89	215	220.20	7.80	3589.69
		5	226.20	1.80	3583.69	220	220.15	7.85	3589.74
		10	225.80	2.20	3584.09	225	220.15	7.85	3589.74
		15	225.55	2.45	3584.34	230	220.10	7.90	3589.79
		20	225.25	2.75	3584.64	235	220.05	7.95	3589.84
		25	224.90	3.10	3584.99	240	220.00	8.00	3589.89
		30	224.60	3.40	3585.29	245	220.00	8.00	3589.89
		35	224.40	3.60	3585.49	250	219.95	8.05	3589.94
		40	224.10	3.90	3585.79	255	219.95	8.05	3589.94
		45	223.55	4.45	3586.34	260	219.90	8.10	3589.99
		55	223.30	4.70	3586.59	265	219.90	8.10	3589.99
		60	223.10	4.90	3586.79	270	219.85	8.15	3590.04
		65	223.00	5.00	3586.89	275	219.80	8.20	3590.09
		70	222.80	5.20	3587.09	280	219.80	8.20	3590.09
		75	222.60	5.40	3587.29	285	219.80	8.20	3590.09
		80	222.50	5.50	3587.39	290	219.80	8.20	3590.09
		85	222.35	5.65	3587.54	295	219.80	8.20	3590.09
		90	222.20	5.80	3587.69	300	219.75	8.25	3590.14
		95	222.05	5.95	3587.84	305	219.75	8.25	3590.14
		100	221.90	6.10	3587.99	310	219.70	8.30	3590.19
		105	221.80	6.20	3588.09	315	219.70	8.30	3590.19
		110	221.75	6.25	3588.14	320	219.70	8.30	3590.19
		115	221.65	6.35	3588.24	325	219.70	8.30	3590.19
		120	221.55	6.45	3588.34	330	219.65	8.35	3590.24
		125	221.45	6.55	3588.44	335	219.65	8.35	3590.24
		130	221.35	6.65	3588.54	340	219.65	8.35	3590.24
		135	221.25	6.75	3588.64	345	219.65	8.35	3590.24
		140	221.20	6.80	3588.69	350	219.60	8.40	3590.29
		145	221.05	6.95	3588.84	355	219.60	8.40	3590.29
		150	221.00	7.00	3588.89	360	219.60	8.40	3590.29
		155	220.19	7.81	3589.7	365	219.60	8.40	3590.29
		160	220.80	7.20	3589.09	370	219.60	8.40	3590.29
		165	220.75	7.25	3589.14	375	219.55	8.45	3590.34
		170	220.65	7.35	3589.24	380	219.55	8.45	3590.34
		175	220.65	7.35	3589.24	385	219.55	8.45	3590.34
		180	220.55	7.45	3589.34	390	219.55	8.45	3590.34
		185	220.45	7.55	3589.44	395	219.55	8.45	3590.34
		190	220.40	7.60	3589.49	400	219.55	8.45	3590.34
		195	220.35	7.65	3589.54	405	219.55	8.45	3590.34
		200	220.30	7.70	3589.59	410	219.55	8.45	3590.34
		205	220.30	7.70	3589.59	415	219.55	8.45	3590.34
		210	220.20	7.80	3589.69	420	219.55	8.45	3590.34

CITY OF AMARILLO
MUNICIPAL SOLID WASTE LANDFILL
PERMIT NO. 73

SLUG TEST
RECOVERY

WELL NO.	STATIC WATER ELEV.,FT	TIME SEC	WATER LEVEL, FT	H/Ho	WATER ELEV.,FT	TIME SEC	WATER LEVEL,FT	H/Ho	WATER ELEV.,FT
MW-3	3589.16	0				245	212.1	13.20	3580.71
		5	225.3		3567.51	250	211.9	13.40	3580.91
		10	224.8	0.50	3568.01	255	211.7	13.60	3581.11
		15	224.8	0.50	3568.01	260	211.6	13.70	3581.21
		20	226.4	-1.10	3566.41	265	211.4	13.90	3581.41
		25	226.4	-1.10	3566.41	270	211.2	14.10	3581.61
		30	226.0	-0.70	3566.81	275	211.1	14.20	3581.71
		35	225.6	-0.30	3567.21	280	210.8	14.50	3582.01
		40	225.2	0.10	3567.61	285	210.7	14.60	3582.11
		45	225.0	0.30	3567.81	290	210.6	14.70	3582.21
		55	224.5	0.80	3568.31	300	210.4	14.90	3582.41
		60	224.1	1.20	3568.71	310	210.1	15.20	3582.71
		65	223.5	1.80	3569.31	320	209.9	15.40	3582.91
		70	223.0	2.30	3569.81	330	209.7	15.60	3583.11
		75	222.4	2.90	3570.41	340	209.4	15.90	3583.41
		80	222.1	3.20	3570.71	350	209.2	16.10	3583.61
		85	221.7	3.60	3571.11	360	208.9	16.40	3583.91
		90	221.2	4.10	3571.61	370	208.8	16.50	3584.01
		95	220.9	4.40	3571.91	380	208.5	16.80	3584.31
		100	220.4	4.90	3572.41	390	208.4	16.90	3584.41
		105	220.1	5.20	3572.71	400	208.1	17.20	3584.71
		110	219.6	5.70	3573.21	410	207.9	17.40	3584.91
		115	219.3	6.00	3573.51	420	207.8	17.50	3585.01
		120	218.9	6.40	3573.91	430	207.4	17.90	3585.41
		125	218.6	6.70	3574.21	440	207.3	18.00	3585.51
		130	218.3	7.00	3574.51	450	207.2	18.10	3585.61
		135	218.0	7.30	3574.81	460	207.0	18.30	3585.81
		140	217.6	7.70	3575.21	470	206.8	18.50	3586.01
		145	217.2	8.10	3575.61	480	206.6	18.70	3586.21
		150	216.9	8.40	3575.91	490	206.5	18.80	3586.31
		155	216.5	8.80	3576.31	500	206.3	19.00	3586.51
		160	216.2	9.10	3576.61	510	206.2	19.10	3586.61
		165	215.9	9.40	3576.91	520	206.1	19.20	3586.71
		170	215.6	9.70	3577.21	530	205.9	19.40	3586.91
		175	215.2	10.10	3577.61	540	205.8	19.50	3587.01
		180	215.0	10.30	3577.81	550	205.7	19.60	3587.11
		185	214.8	10.50	3578.01	560	205.6	19.70	3587.21
		190	214.5	10.80	3578.31	570	205.5	19.80	3587.31
		195	214.2	11.10	3578.61	580	205.4	19.90	3587.41
		200	214.0	11.30	3578.81	590	205.3	20.00	3587.51
		205	213.8	11.50	3579.01	600	205.2	20.10	3587.61
		210	213.5	11.80	3579.31	610	205.1	20.20	3587.71
		215	213.3	12.00	3579.51	620	205.1	20.20	3587.71
		220	213.1	12.20	3579.71	630	205.0	20.30	3587.81
		225	212.9	12.40	3579.91	640	204.9	20.40	3587.91
		230	212.6	12.70	3580.21	650	204.8	20.50	3588.01
		235	212.4	12.90	3580.41	660	204.8	20.50	3588.01
		240	212.3	13.00	3580.51	670	204.7	20.60	3588.11

HDR Engineering, Inc.

HDR

Project	City of Amarillo MSWLF	Computed	BAM	Date	10/19/94
Subject	In-situ Permeability Calculations	Checked		Date	
Task	Hvorslev Method G	Sheet	1	Of	1

Static W.L. = 149.20

MW-6

$$157.00 = H_1$$

$$152.20 = H_2$$

$$K_h = \frac{d^2 \cdot \ln\left(\frac{2ML}{D}\right) \cdot \ln\left(\frac{H_1}{H_2}\right)}{8 \cdot L \cdot T}$$

$$= \frac{(10.16)^2 \cdot \ln\left(\frac{2(3)(1219.20)}{10.16}\right) \cdot \ln\left(\frac{7.8}{3.0}\right)}{8(1219.20)(50)}$$

$$= \frac{103.23 \cdot 6.58}{487680} = 0.841$$

$$= 0.0013928 \cdot 0.9555115$$

$$K_h = 1.33 \times 10^{-3} \text{ cm/sec}$$

CITY OF AMARILLO
MUNICIPAL SOLID WASTE LANDFILL
PERMIT NO. 73

SLUG TEST
RECOVERY

WELL NO.	STATIC WATER ELEV.,FT	TIME SEC	WATER LEVEL,FT	H/Ho	WATER ELEV.,FT	TIME SEC	WATER LEVEL,FT	H/Ho	WATER ELEV.,FT
MW-6	3601.52	5	157.00		3593.72	155	149.75	7.25	3600.97
		10	156.90	0.10	3593.82	160	149.70	7.30	3601.02
		15	155.00	2.00	3595.72	165	149.70	7.30	3601.02
		20	154.60	2.40	3596.12	170	149.65	7.35	3601.07
		25	154.20	2.80	3596.52	175	149.60	7.40	3601.12
		30	153.90	3.10	3596.82	180	149.60	7.40	3601.12
		35	153.50	3.50	3597.22	185	149.55	7.45	3601.17
		40	153.20	3.80	3597.52	190	149.55	7.45	3601.17
		45	152.80	4.20	3597.92	195	149.50	7.50	3601.22
		50	152.50	4.50	3598.22	200	149.50	7.50	3601.22
		55	152.20	4.80	3598.52	205	149.50	7.50	3601.22
		60	151.90	5.10	3598.82	210	149.45	7.55	3601.27
		65	151.70	5.30	3599.02	215	149.45	7.55	3601.27
		70	151.50	5.50	3599.22	220	149.45	7.55	3601.27
		75	151.30	5.70	3599.42	225	149.45	7.55	3601.27
		80	151.10	5.90	3599.62	230	149.40	7.60	3601.32
		85	150.90	6.10	3599.82	235	149.40	7.60	3601.32
		90	150.80	6.20	3599.92	240	149.40	7.60	3601.32
		95	150.65	6.35	3600.07	245	149.35	7.65	3601.37
		100	150.55	6.45	3600.17	250	149.35	7.65	3601.37
		105	150.40	6.60	3600.32	255	149.35	7.65	3601.37
		110	150.35	6.65	3600.37	260	149.35	7.65	3601.37
		115	150.25	6.75	3600.47	265	149.35	7.65	3601.37
		120	150.15	6.85	3600.57	270	149.35	7.65	3601.37
		125	150.10	6.90	3600.62	275	149.30	7.70	3601.42
		130	150.05	6.95	3600.67	280	149.30	7.70	3601.42
		135	149.95	7.05	3600.77	285	149.30	7.70	3601.42
		140	149.90	7.10	3600.82	290	149.30	7.70	3601.42
		145	149.80	7.20	3600.92	295	149.30	7.70	3601.42
		150	149.80	7.20	3600.92	300	149.30	7.70	3601.42

Computation



Project	City of Amarillo MSWLF	Computed	BAM	Date
Subject	In-situ Permeability Calculations	Checked		Date
Task	Hvorslev Method G	Sheet	1	Of 1

P-1

$$\begin{aligned}
 K_h &= \frac{d^2 \cdot \ln\left(\frac{2ML}{D}\right) \cdot \ln\frac{H_1}{H_2}}{8 \cdot L \cdot T} \\
 &= \frac{(10.16)^2 \cdot \ln\left(\frac{(2)(3)(1219.2)}{10.16}\right) \cdot \ln\frac{2.9}{1.0}}{8(40)(60)} \\
 &= \frac{679.14715}{19200} \cdot 1.0647107 \\
 &= 3.77 \times 10^{-2} \text{ cm/sec}
 \end{aligned}$$

HDR Engineering, Inc.

HDR

Project	City of Amarillo MSWLF	Computed	BRM	Date	10/1/17
Subject	In-situ Permeability Calculations	Checked		Date	
Task	Horstev Method G	Sheet	1	Of	1

Static W.L. = 203.1

P-2

$$K_h = \frac{d^2 \cdot \ln\left(\frac{2ML}{D}\right)}{8 \cdot L \cdot T} \cdot \ln \frac{H_1}{H_2}$$

$$H_1 = 207.40$$

$$H_2 = 203.90$$

$$= \frac{(10.16)^2 \cdot \ln\left(\frac{2(3)(1219.20)}{10.16}\right)}{8(1219.2)(120)} \cdot \ln \frac{4.3}{0.8}$$

$$= \frac{1679.1761}{1170432} \cdot 1.6817586$$

$$= 9.76 \times 10^{-4} \text{ cm/sec}$$

$$H_1 = 207.40$$

$$H_2 = 204.80$$

$$K_h = \frac{679.1761}{8(1219.2)(60)} \cdot \ln \frac{4.3}{1.7}$$

$$= 0.0011606 \cdot 0.9279868$$

$$= 1.08 \times 10^{-3} \text{ cm/sec}$$

$$\text{Average} = 1.03 \times 10^{-3} \text{ cm/sec}$$

CITY OF AMARILLO
MUNICIPAL SOLID WASTE LANDFILL
PERMIT NO. 73

SLUG TEST
RECOVERY

STATIC WATER		TIME SEC	WATER LEVEL, FT	H/Ho	WATER ELEV., FT	TIME SEC	WATER LEVEL, FT	H/Ho	WATER ELEV., FT
WELL NO.	ELEV., FT								
P-2	3595.17	0							
		5	207.40		3590.87	125	203.85	3.55	3594.42
		10	206.90	0.50	3591.37	130	203.80	3.60	3594.47
		15	206.60	0.80	3591.67	135	203.80	3.60	3594.47
		20	206.40	1.00	3591.87	140	203.75	3.65	3594.52
		25	206.20	1.20	3592.07	145	203.70	3.70	3594.57
		30	206.00	1.40	3592.27	150	203.70	3.70	3594.57
		35	205.90	1.50	3592.37	155	203.65	3.75	3594.62
		40	205.80	1.60	3592.47	160	203.65	3.75	3594.62
		45	206.50	0.90	3591.77	165	203.60	3.80	3594.67
		50	205.50	1.90	3592.77	170	203.60	3.80	3594.67
		55	204.90	2.50	3593.37	175	203.55	3.85	3594.72
		60	204.80	2.60	3593.47	180	203.55	3.85	3594.72
		65	204.70	2.70	3593.57	185	203.50	3.90	3594.77
		70	204.50	2.90	3593.77	190	203.50	3.90	3594.77
		75	204.50	2.90	3593.77	195	203.50	3.90	3594.77
		80	204.40	3.00	3593.87	200	203.45	3.95	3594.82
		85	204.30	3.10	3593.97	205	203.45	3.95	3594.82
		90	204.25	3.15	3594.02	210	203.45	3.95	3594.82
		95	204.20	3.20	3594.07	215	203.45	3.95	3594.82
		100	204.15	3.25	3594.12	220	203.40	4.00	3594.87
		105	204.10	3.30	3594.17	225	203.40	4.00	3594.87
		110	204.00	3.40	3594.27	230	203.40	4.00	3594.87
		115	203.95	3.45	3594.32	235	203.40	4.00	3594.87
		120	203.90	3.50	3594.37	240	203.40	4.00	3594.87

HDR Engineering, Inc.

HDR

Project	City of Amarillo MSWLF	Computed	BAM	Date	10/19/11
Subject	In-situ Permeability Calculations	Checked		Date	
Task	Hvorslev Method G	Sheet	1	Of	1

Static W.L. = 147.0

P-3

$$K_h = \frac{d^2 \cdot \ln\left(\frac{2ML}{D}\right)}{8 \cdot L \cdot T} \cdot \ln \frac{H_1}{H_2}$$

$$H_1 = 158.10$$

$$H_2 = 148.80$$

$$= \frac{679.1761}{2(292)(120)} \cdot \ln \frac{11.05}{1.75}$$

$$= 0.0023211 \cdot 1.8428146$$

$$= 4.28 \times 10^{-3} \text{ cm/sec}$$

CITY OF AMARILLO
MUNICIPAL SOLID WASTE LANDFILL
PERMIT NO. 73

SLUG TEST
RECOVERY

WELL NO.	STATIC WATER ELEV.,FT	TIME SEC	WATER LEVEL,FT	H/Ho	WATER ELEV.,FT	TIME SEC	WATER LEVEL,FT	H/Ho	WATER ELEV.,FT
P-3	3599.61	0							
		5	158.10		3588.56	215	147.60	10.50	3599.06
		10	156.90	1.20	3589.76	220	147.55	10.55	3599.11
		15	156.00	2.10	3590.66	225	147.50	10.60	3599.16
		20	155.00	3.10	3591.66	230	147.50	10.60	3599.16
		25	154.20	3.90	3592.46	235	147.50	10.60	3599.16
		30	153.20	4.90	3593.46	240	147.45	10.65	3599.21
		35	152.60	5.50	3594.06	245	147.40	10.70	3599.26
		40	152.10	6.00	3594.56	250	147.40	10.70	3599.26
		45	151.70	6.40	3594.96	255	147.40	10.70	3599.26
		50	151.40	6.70	3595.26	260	147.40	10.70	3599.26
		55	151.10	7.00	3595.56	265	147.40	10.70	3599.26
		60	150.80	7.30	3595.86	270	147.35	10.75	3599.31
		65	150.60	7.50	3596.06	275	147.35	10.75	3599.31
		70	150.40	7.70	3596.26	280	147.35	10.75	3599.31
		75	150.20	7.90	3596.46	285	147.30	10.80	3599.36
		80	150.00	8.10	3596.66	290	147.30	10.80	3599.36
		85	149.80	8.30	3596.86	295	147.30	10.80	3599.36
		90	149.60	8.50	3597.06	300	147.25	10.85	3599.41
		95	149.40	8.70	3597.26	305	147.25	10.85	3599.41
		100	149.30	8.80	3597.36	310	147.25	10.85	3599.41
		105	149.10	9.00	3597.56	315	147.25	10.85	3599.41
		110	149.00	9.10	3597.66	320	147.25	10.85	3599.41
		115	148.95	9.15	3597.71	325	147.25	10.85	3599.41
		120	148.80	9.30	3597.86	330	147.20	10.90	3599.46
		125	148.70	9.40	3597.96	335	147.20	10.90	3599.46
		130	148.60	9.50	3598.06	340	147.20	10.90	3599.46
		135	148.50	9.60	3598.16	345	147.20	10.90	3599.46
		140	148.40	9.70	3598.26	350	147.20	10.90	3599.46
		145	148.35	9.75	3598.31	355	147.20	10.90	3599.46
		150	148.30	9.80	3598.36	360	147.20	10.90	3599.46
		155	148.25	9.85	3598.41	365	147.20	10.90	3599.46
		160	148.15	9.95	3598.51	370	147.20	10.90	3599.46
		165	148.05	10.05	3598.61	375	147.20	10.90	3599.46
		170	148.00	10.10	3598.66	380	147.15	10.95	3599.51
		175	147.90	10.20	3598.76	385	147.15	10.95	3599.51
		180	147.85	10.25	3598.81	390	147.15	10.95	3599.51
		185	147.80	10.30	3598.86	395	147.15	10.95	3599.51
		190	147.75	10.35	3598.91	400	147.15	10.95	3599.51
		195	147.75	10.35	3598.91	405	147.15	10.95	3599.51
		200	147.70	10.40	3598.96	410	147.15	10.95	3599.51
		205	147.65	10.45	3599.01	415	147.15	10.95	3599.51
		210	147.60	10.50	3599.06	420	147.15	10.95	3599.51

HDR Engineering, Inc.



Project	City of Amarillo MSWLF	Computed	BAM	Date	10/25/17
Subject	Equilibrium Well Equation	Checked		Date	
Task	Estimate Hydraulic Conductivity	Sheet	1	Of	3

$$Q = \frac{K(H^2 - h^2)}{1,055 \log R/r}$$

Driscoll, p. 213

- Q = pumping rate, gpm
- K = hydraulic conductivity of formation, gpd/ft²
- H = static head measured from bottom of aquifer, ft
- h = depth of water in well while pumping, ft
- R = radius of the cone of depression, ft
- r = radius of the well, ft

MW-2

$$\begin{aligned}
 K &= \frac{Q}{1,055 \log R/r} \frac{H^2 - h^2}{H^2 - h^2} \\
 &= \frac{10 (1,055 \log 10/0.167)}{25.75^2 - 18.8^2} \\
 &= \frac{18750.34}{663.06 - 353.44} \\
 &= \frac{18750.34}{309.62} \\
 &= 60.56 \text{ gpd/ft}^2 \\
 &= 2.86 \times 10^{-3} \text{ cm/sec}
 \end{aligned}$$

- Q = 10 gpm
- H = 25.75
- h = 18.8
- R = 10' (assumed)
- r = 0.167

HDR Engineering, Inc.

HDR

Project	City of Amarillo MSWLF	Computed	BRM	Date	10/25/97
Subject	Equilibrium Well Equation	Checked		Date	
Task	Estimate Hydraulic Conductivity	Sheet	2	Of	3

MW-2 Cont.

$$\begin{aligned}
 R &= 20' & K &= \frac{10(1,055) \log 20/.167}{25.75^2 - 18.8^2} \\
 & & &= \frac{21926.21}{663.06 - 353.44} \\
 & & &= 70.82 \text{ gpd/ft}^2 \\
 & & &= 3.34 \times 10^{-3} \text{ cm/sec}
 \end{aligned}$$

MW-3

$$\begin{aligned}
 K &= \frac{6(1,055) \log 20/.167}{43.35^2 - 21.70^2} \\
 &= \frac{13155.73}{1879.22 - 470.89} \\
 &= 9.34 \text{ gpd/ft}^2 \\
 &= 4.4 \times 10^{-4} \text{ cm/sec}
 \end{aligned}$$

$$\begin{aligned}
 Q &= 6 \text{ gpm} \\
 H &= 43.35 \\
 h &= 21.70 \\
 R &= 20 \\
 r &= 0.167
 \end{aligned}$$

HDR Engineering, Inc.

HDR

Project	City of Amarillo MSWLF	Computed	DAM	Date	10/2/11
Subject	Equilibrium Well Equation	Checked		Date	
Task	Estimate Hydraulic Conductivity	Sheet	3	Of	3

MW-6

$$\begin{aligned}
 K &= \frac{12(1,055) \log 20/0.167}{27.15^2 - 19^2} \\
 &= \frac{26311.45}{737.12 - 361} \\
 &= 69.95 \text{ gpd/ft}^2 \\
 &= 3.3 \times 10^{-3} \text{ cm/sec}
 \end{aligned}$$

$$\begin{aligned}
 Q &= 12 \text{ gpm} \\
 H &= 27.15 \\
 h &= 19 \\
 R &= 20' \\
 r &= 0.167
 \end{aligned}$$

P-3

$$\begin{aligned}
 K &= \frac{10(1,055) \log 20/0.167}{17.95^2 - 6.9^2} \\
 &= \frac{4926.21}{322.20 - 47.61} \\
 &= 79 \text{ gpd/ft}^2 \\
 &= 3.77 \times 10^{-3} \text{ cm/sec}
 \end{aligned}$$

$$\begin{aligned}
 Q &= 10 \\
 H &= 17.95 \\
 h &= 6.9 \\
 R &= 20 \\
 r &= 0.167
 \end{aligned}$$

HDR Engineering, Inc.



Project	City of Amarillo MSWLF	Computed	BAM	Date	10/26/9
Subject	Estimate Radius of Influence	Checked		Date	
Task		Sheet	1	Of	1

$$r_0^2 = \frac{0.3Tt}{S}$$

S = Coefficient of Storage
 T = Transmissivity, gal/ft
 t = time since pumping started, days
 r_0 = intercept of extended straight line at zero drawdown, ft

$$\begin{aligned}
 r_0^2 &= \frac{0.3(6600)(0.042)}{0.2} \\
 &= \sqrt{415.8} \\
 &= 20.39
 \end{aligned}$$

Using average of Transmissivities computed for wells in Randal County, TWDB Report 98, Compilation of Results of Aquifer Tests in Texas

APPENDIX C
HELP MODEL RUNS

Amarillo - Year One - GCL/FML (LF=0.01) - 10-2 SAND DRAIN, 2%, 840' -o
One lift of waste with daily cover (SC) - LAI=0.0 - RO=0.0
NOVEMBER 29, 1994

LAYER 1

VERTICAL PERCOLATION LAYER

THICKNESS	=	6.00 INCHES
POROSITY	=	0.3980 VOL/VOL
FIELD CAPACITY	=	0.2443 VOL/VOL
WILTING POINT	=	0.1361 VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.2443 VOL/VOL
SATURATED HYDRAULIC CONDUCTIVITY	=	0.000119999997 CM/SEC

LAYER 2

VERTICAL PERCOLATION LAYER

THICKNESS	=	120.00 INCHES
POROSITY	=	0.5200 VOL/VOL
FIELD CAPACITY	=	0.2942 VOL/VOL
WILTING POINT	=	0.1400 VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.2000 VOL/VOL
SATURATED HYDRAULIC CONDUCTIVITY	=	0.000099999997 CM/SEC

LAYER 3

VERTICAL PERCOLATION LAYER

THICKNESS	=	12.00 INCHES
POROSITY	=	0.3980 VOL/VOL
FIELD CAPACITY	=	0.2443 VOL/VOL
WILTING POINT	=	0.1361 VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.2443 VOL/VOL
SATURATED HYDRAULIC CONDUCTIVITY	=	0.000099999997 CM/SEC

LAYER 4

LATERAL DRAINAGE LAYER

THICKNESS = 12.00 INCHES
 POROSITY = 0.4170 VOL/VOL
 FIELD CAPACITY = 0.0454 VOL/VOL
 WILTING POINT = 0.0200 VOL/VOL
 INITIAL SOIL WATER CONTENT = 0.0454 VOL/VOL
 SATURATED HYDRAULIC CONDUCTIVITY = 0.009999999776 CM/SEC
 SLOPE = 2.00 PERCENT
 DRAINAGE LENGTH = 840.0 FEET

LAYER 5

BARRIER SOIL LINER WITH FLEXIBLE MEMBRANE LINER

THICKNESS = 0.30 INCHES
 POROSITY = 0.4000 VOL/VOL
 FIELD CAPACITY = 0.3560 VOL/VOL
 WILTING POINT = 0.2899 VOL/VOL
 INITIAL SOIL WATER CONTENT = 0.4000 VOL/VOL
 SATURATED HYDRAULIC CONDUCTIVITY = 0.000000005000 CM/SEC
 LINER LEAKAGE FRACTION = 0.01000000

GENERAL SIMULATION DATA

SCS RUNOFF CURVE NUMBER = 70.00
 TOTAL AREA OF COVER = 1. SQ FT
 EVAPORATIVE ZONE DEPTH = 10.00 INCHES
 POTENTIAL RUNOFF FRACTION = 0.000000
 UPPER LIMIT VEG. STORAGE = 4.4680 INCHES
 INITIAL VEG. STORAGE = 2.2658 INCHES
 INITIAL SNOW WATER CONTENT = 0.0000 INCHES
 INITIAL TOTAL WATER STORAGE IN
 SOIL AND WASTE LAYERS = 29.0622 INCHES

SOIL WATER CONTENT INITIALIZED BY USER.

CLIMATOLOGICAL DATA

SYNTHETIC RAINFALL WITH SYNTHETIC DAILY TEMPERATURES AND
 SOLAR RADIATION FOR AMARILLO TEXAS

MAXIMUM LEAF AREA INDEX = 0.00
 START OF GROWING SEASON (JULIAN DATE) = 104
 END OF GROWING SEASON (JULIAN DATE) = 302

NORMAL MEAN MONTHLY TEMPERATURES, DEGREES FAHRENHEIT

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
-----	-----	-----	-----	-----	-----
35.10	39.20	47.10	56.80	65.40	74.10
78.60	76.50	69.10	58.50	46.00	36.90

 MONTHLY TOTALS FOR YEAR 10

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
PRECIPITATION (INCHES)	0.82 3.10	1.75 3.14	0.32 1.25	1.43 2.55	0.88 1.01	2.98 0.54
RUNOFF (INCHES)	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000
EVAPOTRANSPIRATION (INCHES)	1.617 1.108	0.904 4.106	1.257 0.759	0.736 2.797	1.538 1.078	2.762 0.416
LATERAL DRAINAGE FROM LAYER 4 (INCHES)	0.0036 0.0177	0.0081 0.0179	0.0124 0.0173	0.0142 0.0177	0.0163 0.0168	0.0166 0.0170
PERCOLATION FROM LAYER 5 (INCHES)	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001

 MONTHLY SUMMARIES FOR DAILY HEADS

DAILY HEAD ON LAYER 5 (INCHES)	0.09 0.42	0.21 0.43	0.30 0.43	0.35 0.42	0.39 0.41	0.41 0.41
STD. DEV. OF DAILY HEAD ON LAYER 5 (INCHES)	0.05 0.00	0.03 0.00	0.02 0.00	0.01 0.00	0.01 0.00	0.00 0.00

 ANNUAL TOTALS FOR YEAR 10

	(INCHES)	(CU. FT.)	PERCENT
PRECIPITATION	19.77	2.	100.00
RUNOFF	0.000	0.	0.00
EVAPOTRANSPIRATION	19.078	2.	96.50
LATERAL DRAINAGE FROM LAYER 4	0.1755	0.	0.89
PERCOLATION FROM LAYER 5	0.0014	0.	0.01
CHANGE IN WATER STORAGE	0.515	0.	2.61
JUL WATER AT START OF YEAR	29.06	2.	
SOIL WATER AT END OF YEAR	29.58	2.	
SNOW WATER AT START OF YEAR	0.00	0.	

SNOW WATER AT END OF YEAR	0.00	0.	
ANNUAL WATER BUDGET BALANCE	0.00	0.	0.00

AVERAGE MONTHLY VALUES IN INCHES FOR YEARS 10 THROUGH 10

JAN/JUL FEB/AUG MAR/SEP APR/OCT MAY/NOV JUN/DEC

PRECIPITATION

TOTALS	0.82	1.75	0.32	1.43	0.88	2.98
	3.10	3.14	1.25	2.55	1.01	0.54
STD. DEVIATIONS	0.00	0.00	0.00	0.00	0.00	0.00
	0.00	0.00	0.00	0.00	0.00	0.00

RUNOFF

TOTALS	0.000	0.000	0.000	0.000	0.000	0.000
	0.000	0.000	0.000	0.000	0.000	0.000
STD. DEVIATIONS	0.000	0.000	0.000	0.000	0.000	0.000
	0.000	0.000	0.000	0.000	0.000	0.000

EVAPOTRANSPIRATION

TOTALS	1.617	0.904	1.257	0.736	1.538	2.762
	1.108	4.106	0.759	2.797	1.078	0.416
STD. DEVIATIONS	0.000	0.000	0.000	0.000	0.000	0.000
	0.000	0.000	0.000	0.000	0.000	0.000

LATERAL DRAINAGE FROM LAYER 4

TOTALS	0.0036	0.0081	0.0124	0.0142	0.0163	0.0166
	0.0177	0.0179	0.0173	0.0177	0.0168	0.0170
STD. DEVIATIONS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

PERCOLATION FROM LAYER 5

TOTALS	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001
	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001
STD. DEVIATIONS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 10 THROUGH 10

	(INCHES)	(CU. FT.)	PERCENT
PRECIPITATION	19.77 (0.000)	2.	100.00
RUNOFF	0.000 (0.000)	0.	0.00
EVAPOTRANSPIRATION	19.078 (0.000)	2.	96.50
LATERAL DRAINAGE FROM LAYER 4	0.1755 (0.0000)	0.	0.89
PERCOLATION FROM LAYER 5	0.0014 (0.0000)	0.	0.01
CHANGE IN WATER STORAGE	0.515 (0.000)	0.	2.61

PEAK DAILY VALUES FOR YEARS 10 THROUGH 10

	(INCHES)	(CU. FT.)
PRECIPITATION	1.05	0.1
RUNOFF	0.000	0.0
LATERAL DRAINAGE FROM LAYER 4	0.0006	0.0
PERCOLATION FROM LAYER 5	0.0000	0.0
HEAD ON LAYER 5	0.4	
SNOW WATER	0.06	0.0
MAXIMUM VEG. SOIL WATER (VOL/VOL)	0.3792	
MINIMUM VEG. SOIL WATER (VOL/VOL)	0.1355	

FINAL WATER STORAGE AT END OF YEAR 10

LAYER	(INCHES)	(VOL/VOL)
1	0.92	0.1535
2	25.23	0.2102
3	2.62	0.2180
4	0.69	0.0578
5	0.12	0.4000
SNOW WATER	0.00	

Amarillo - Year two - only one year
two lifts of waste with daily cover
NOVEMBER 29, 1994

LAYER 1

VERTICAL PERCOLATION LAYER

THICKNESS	=	6.00 INCHES
POROSITY	=	0.3980 VOL/VOL
FIELD CAPACITY	=	0.2443 VOL/VOL
WILTING POINT	=	0.1361 VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.2443 VOL/VOL
SATURATED HYDRAULIC CONDUCTIVITY	=	0.000119999997 CM/SEC

LAYER 2

VERTICAL PERCOLATION LAYER

THICKNESS	=	120.00 INCHES
POROSITY	=	0.5200 VOL/VOL
FIELD CAPACITY	=	0.2942 VOL/VOL
WILTING POINT	=	0.1400 VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.2000 VOL/VOL
SATURATED HYDRAULIC CONDUCTIVITY	=	0.000099999997 CM/SEC

LAYER 3

VERTICAL PERCOLATION LAYER

THICKNESS	=	120.00 INCHES
POROSITY	=	0.5200 VOL/VOL
FIELD CAPACITY	=	0.2942 VOL/VOL
WILTING POINT	=	0.1400 VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.2102 VOL/VOL
SATURATED HYDRAULIC CONDUCTIVITY	=	0.000099999997 CM/SEC

LAYER 4

VERTICAL PERCOLATION LAYER

THICKNESS = 12.00 INCHES
 POROSITY = 0.3980 VOL/VOL
 FIELD CAPACITY = 0.2443 VOL/VOL
 WILTING POINT = 0.1361 VOL/VOL
 INITIAL SOIL WATER CONTENT = 0.2108 VOL/VOL
 SATURATED HYDRAULIC CONDUCTIVITY = 0.000119999997 CM/SEC

LAYER 5

LATERAL DRAINAGE LAYER

THICKNESS = 12.00 INCHES
 POROSITY = 0.4170 VOL/VOL
 FIELD CAPACITY = 0.0454 VOL/VOL
 WILTING POINT = 0.0200 VOL/VOL
 INITIAL SOIL WATER CONTENT = 0.0578 VOL/VOL
 SATURATED HYDRAULIC CONDUCTIVITY = 0.009999999776 CM/SEC
 SLOPE = 2.00 PERCENT
 DRAINAGE LENGTH = 840.0 FEET

LAYER 6

BARRIER SOIL LINER WITH FLEXIBLE MEMBRANE LINER

THICKNESS = 0.30 INCHES
 POROSITY = 0.4000 VOL/VOL
 FIELD CAPACITY = 0.3560 VOL/VOL
 WILTING POINT = 0.2899 VOL/VOL
 INITIAL SOIL WATER CONTENT = 0.4000 VOL/VOL
 SATURATED HYDRAULIC CONDUCTIVITY = 0.000000005000 CM/SEC
 LINER LEAKAGE FRACTION = 0.01000000

GENERAL SIMULATION DATA

SCS RUNOFF CURVE NUMBER = 70.00
 TOTAL AREA OF COVER = 1. SQ FT
 EVAPORATIVE ZONE DEPTH = 10.00 INCHES
 POTENTIAL RUNOFF FRACTION = 0.000000
 UPPER LIMIT VEG. STORAGE = 4.4680 INCHES
 INITIAL VEG. STORAGE = 2.2658 INCHES
 INITIAL SNOW WATER CONTENT = 0.0000 INCHES
 INITIAL TOTAL WATER STORAGE IN
 SOIL AND WASTE LAYERS = 54.0330 INCHES

SOIL WATER CONTENT INITIALIZED BY USER.

CLIMATOLOGICAL DATA

SYNTHETIC RAINFALL WITH SYNTHETIC DAILY TEMPERATURES AND
 SOLAR RADIATION FOR AMARILLO TEXAS

MAXIMUM LEAF AREA INDEX = 0.00
 START OF GROWING SEASON (JULIAN DATE) = 104
 END OF GROWING SEASON (JULIAN DATE) = 302

NORMAL MEAN MONTHLY TEMPERATURES, DEGREES FAHRENHEIT

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
35.10	39.20	47.10	56.80	65.40	74.10
78.60	76.50	69.10	58.50	46.00	36.90

MONTHLY TOTALS FOR YEAR 10

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
PRECIPITATION (INCHES)	0.82 3.10	1.75 3.14	0.32 1.25	1.43 2.55	0.88 1.01	2.98 0.54
RUNOFF (INCHES)	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000
EVAPOTRANSPIRATION (INCHES)	1.617 1.108	0.904 4.106	1.257 0.759	0.736 2.797	1.538 1.078	2.762 0.416
LATERAL DRAINAGE FROM LAYER 5 (INCHES)	0.0162 0.0121	0.0140 0.0115	0.0148 0.0106	0.0136 0.0104	0.0133 0.0096	0.0123 0.0095
PERCOLATION FROM LAYER 6 (INCHES)	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001

MONTHLY SUMMARIES FOR DAILY HEADS

AVG. DAILY HEAD ON LAYER 6 (INCHES)	0.39 0.29	0.37 0.27	0.35 0.26	0.33 0.25	0.32 0.24	0.30 0.23
STD. DEV. OF DAILY HEAD ON LAYER 6 (INCHES)	0.01 0.00	0.01 0.00	0.01 0.00	0.00 0.00	0.00 0.00	0.00 0.00

ANNUAL TOTALS FOR YEAR 10

	(INCHES)	(CU. FT.)	PERCENT
PRECIPITATION	19.77	2.	100.00
RUNOFF	0.000	0.	0.00

EVAPOTRANSPIRATION	19.078	2.	96.50
LATERAL DRAINAGE FROM LAYER 5	0.1478	0.	0.75
PERCOLATION FROM LAYER 6	0.0012	0.	0.01
CHANGE IN WATER STORAGE	0.543	0.	2.75
SOIL WATER AT START OF YEAR	54.03	5.	
SOIL WATER AT END OF YEAR	54.58	5.	
SNOW WATER AT START OF YEAR	0.00	0.	
SNOW WATER AT END OF YEAR	0.00	0.	
ANNUAL WATER BUDGET BALANCE	0.00	0.	0.00

AVERAGE MONTHLY VALUES IN INCHES FOR YEARS 10 THROUGH 10

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
	-----	-----	-----	-----	-----	-----
PRECIPITATION						
TOTALS	0.82 3.10	1.75 3.14	0.32 1.25	1.43 2.55	0.88 1.01	2.98 0.54
STD. DEVIATIONS	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00
RUNOFF						
TOTALS	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000
STD. DEVIATIONS	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000
EVAPOTRANSPIRATION						
TOTALS	1.617 1.108	0.904 4.106	1.257 0.759	0.736 2.797	1.538 1.078	2.762 0.416
STD. DEVIATIONS	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000
LATERAL DRAINAGE FROM LAYER 5						
TOTALS	0.0162 0.0121	0.0140 0.0115	0.0148 0.0106	0.0136 0.0104	0.0133 0.0096	0.0123 0.0095
STD. DEVIATIONS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
PERCOLATION FROM LAYER 6						

TOTALS	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001
	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001
STD. DEVIATIONS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 10 THROUGH 10

	(INCHES)	(CU. FT.)	PERCENT
	-----	-----	-----
PRECIPITATION	19.77 (0.000)	2.	100.00
RUNOFF	0.000 (0.000)	0.	0.00
EVAPOTRANSPIRATION	19.078 (0.000)	2.	96.50
LATERAL DRAINAGE FROM LAYER 5	0.1478 (0.0000)	0.	0.75
PERCOLATION FROM LAYER 6	0.0012 (0.0000)	0.	0.01
CHANGE IN WATER STORAGE	0.543 (0.000)	0.	2.75

PEAK DAILY VALUES FOR YEARS 10 THROUGH 10

	(INCHES)	(CU. FT.)
	-----	-----
PRECIPITATION	1.05	0.1
RUNOFF	0.000	0.0
LATERAL DRAINAGE FROM LAYER 5	0.0005	0.0
PERCOLATION FROM LAYER 6	0.0000	0.0
HEAD ON LAYER 6	0.4	
SNOW WATER	0.06	0.0
MAXIMUM VEG. SOIL WATER (VOL/VOL)	0.3792	
MINIMUM VEG. SOIL WATER (VOL/VOL)	0.1355	

LAYER	(INCHES)	(VOL / VOL)
1	0.92	0.1535
2	25.23	0.2102
3	25.22	0.2102
4	2.46	0.2050
5	0.63	0.0523
6	0.12	0.4000
SNOW WATER	0.00	

Amarillo - Year three - only one year
three lifts of waste with daily cover
NOVEMBER 29, 1994

LAYER 1

VERTICAL PERCOLATION LAYER

THICKNESS	=	6.00 INCHES
POROSITY	=	0.3980 VOL/VOL
FIELD CAPACITY	=	0.2443 VOL/VOL
WILTING POINT	=	0.1361 VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.2443 VOL/VOL
SATURATED HYDRAULIC CONDUCTIVITY	=	0.000119999997 CM/SEC

LAYER 2

VERTICAL PERCOLATION LAYER

THICKNESS	=	120.00 INCHES
POROSITY	=	0.5200 VOL/VOL
FIELD CAPACITY	=	0.2942 VOL/VOL
WILTING POINT	=	0.1400 VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.2000 VOL/VOL
SATURATED HYDRAULIC CONDUCTIVITY	=	0.000099999997 CM/SEC

LAYER 3

VERTICAL PERCOLATION LAYER

THICKNESS	=	120.00 INCHES
POROSITY	=	0.5200 VOL/VOL
FIELD CAPACITY	=	0.2942 VOL/VOL
WILTING POINT	=	0.1400 VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.2102 VOL/VOL
SATURATED HYDRAULIC CONDUCTIVITY	=	0.000099999997 CM/SEC

LAYER 4

VERTICAL PERCOLATION LAYER

THICKNESS = 120.00 INCHES
POROSITY = 0.5200 VOL/VOL
FIELD CAPACITY = 0.2942 VOL/VOL
WILTING POINT = 0.1400 VOL/VOL
INITIAL SOIL WATER CONTENT = 0.2102 VOL/VOL
SATURATED HYDRAULIC CONDUCTIVITY = 0.00009999997 CM/SEC

LAYER 5

VERTICAL PERCOLATION LAYER

THICKNESS = 12.00 INCHES
POROSITY = 0.3980 VOL/VOL
FIELD CAPACITY = 0.2443 VOL/VOL
WILTING POINT = 0.1361 VOL/VOL
INITIAL SOIL WATER CONTENT = 0.2050 VOL/VOL
SATURATED HYDRAULIC CONDUCTIVITY = 0.000119999997 CM/SEC

LAYER 6

LATERAL DRAINAGE LAYER

THICKNESS = 12.00 INCHES
POROSITY = 0.4170 VOL/VOL
FIELD CAPACITY = 0.0454 VOL/VOL
WILTING POINT = 0.0200 VOL/VOL
INITIAL SOIL WATER CONTENT = 0.0523 VOL/VOL
SATURATED HYDRAULIC CONDUCTIVITY = 0.00999999776 CM/SEC
SLOPE = 2.00 PERCENT
DRAINAGE LENGTH = 840.0 FEET

LAYER 7

BARRIER SOIL LINER WITH FLEXIBLE MEMBRANE LINER

THICKNESS = 0.30 INCHES
POROSITY = 0.4000 VOL/VOL
FIELD CAPACITY = 0.3560 VOL/VOL
WILTING POINT = 0.2899 VOL/VOL
INITIAL SOIL WATER CONTENT = 0.4000 VOL/VOL
SATURATED HYDRAULIC CONDUCTIVITY = 0.000000005000 CM/SEC
LINER LEAKAGE FRACTION = 0.01000000

GENERAL SIMULATION DATA

SCS RUNOFF CURVE NUMBER = 70.00
TOTAL AREA OF COVER = 1.50 FT
EVAPORATIVE ZONE DEPTH = 10.00 INCHES
POTENTIAL RUNOFF FRACTION = 0.000000
UPPER LIMIT VEG. STORAGE = 4.4680 INCHES

ANNUAL TOTALS FOR YEAR 10

	(INCHES)	(CU. FT.)	PERCENT
PRECIPITATION	19.77	2.	100.00
RUNOFF	0.000	0.	0.00
EVAPOTRANSPIRATION	19.078	2.	96.50
LATERAL DRAINAGE FROM LAYER 6	0.0868	0.	0.44
PERCOLATION FROM LAYER 7	0.0010	0.	0.00
CHANGE IN WATER STORAGE	0.604	0.	3.06
SOIL WATER AT START OF YEAR	79.12	7.	
SOIL WATER AT END OF YEAR	79.73	7.	
SNOW WATER AT START OF YEAR	0.00	0.	
SNOW WATER AT END OF YEAR	0.00	0.	
ANNUAL WATER BUDGET BALANCE	0.00	0.	0.00

AVERAGE MONTHLY VALUES IN INCHES FOR YEARS 10 THROUGH 10

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
PRECIPITATION						
TOTALS	0.82 3.10	1.75 3.14	0.32 1.25	1.43 2.55	0.88 1.01	2.98 0.54
STD. DEVIATIONS	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00
RUNOFF						
TOTALS	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000
STD. DEVIATIONS	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000
EVAPOTRANSPIRATION						
TOTALS	1.617 1.108	0.904 4.106	1.257 0.759	0.736 2.797	1.538 1.078	2.762 0.416

STD. DEVIATIONS	0.000	0.000	0.000	0.000	0.000	0.000
	0.000	0.000	0.000	0.000	0.000	0.000

LATERAL DRAINAGE FROM LAYER 6

TOTALS	0.0090	0.0079	0.0084	0.0078	0.0077	0.0072
	0.0071	0.0069	0.0064	0.0064	0.0060	0.0060
STD. DEVIATIONS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

PERCOLATION FROM LAYER 7

TOTALS	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001
	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001
STD. DEVIATIONS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 10 THROUGH 10

	(INCHES)	(CU. FT.)	PERCENT
PRECIPITATION	19.77 (0.000)	2.	100.00
RUNOFF	0.000 (0.000)	0.	0.00
EVAPOTRANSPIRATION	19.078 (0.000)	2.	96.50
LATERAL DRAINAGE FROM LAYER 6	0.0868 (0.0000)	0.	0.44
PERCOLATION FROM LAYER 7	0.0010 (0.0000)	0.	0.00
CHANGE IN WATER STORAGE	0.604 (0.000)	0.	3.06

PEAK DAILY VALUES FOR YEARS 10 THROUGH 10

	(INCHES)	(CU. FT.)
PRECIPITATION	1.05	0.1
RUNOFF	0.000	0.0
LATERAL DRAINAGE FROM LAYER 6	0.0003	0.0
PERCOLATION FROM LAYER 7	0.0000	0.0
HEAD ON LAYER 7	0.2	
SNOW WATER	0.06	0.0

MAXIMUM VEG. SOIL WATER (VOL/VOL) 0.3792

MINIMUM VEG. SOIL WATER (VOL/VOL) 0.1355

FINAL WATER STORAGE AT END OF YEAR 10

LAYER	(INCHES)	(VOL/VOL)
1	0.92	0.1535
2	25.23	0.2102
3	25.22	0.2102
4	25.22	0.2102
5	2.42	0.2013
6	0.60	0.0497
7	0.12	0.4000
SNOW WATER	0.00	

Amarillo - Year FIVE - FIVE years EVAP DEPTH=18" LAI=2.0
 five lifts of waste with INTERMEDIATE cover RO=1.0
 November 29, 1994

LAYER 1

VERTICAL PERCOLATION LAYER

THICKNESS	=	12.00 INCHES
POROSITY	=	0.3980 VOL/VOL
FIELD CAPACITY	=	0.2443 VOL/VOL
WILTING POINT	=	0.1361 VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.2443 VOL/VOL
SATURATED HYDRAULIC CONDUCTIVITY	=	0.000119999997 CM/SEC

LAYER 2

VERTICAL PERCOLATION LAYER

THICKNESS	=	240.00 INCHES
POROSITY	=	0.5200 VOL/VOL
FIELD CAPACITY	=	0.2942 VOL/VOL
WILTING POINT	=	0.1400 VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.2000 VOL/VOL
SATURATED HYDRAULIC CONDUCTIVITY	=	0.000099999997 CM/SEC

LAYER 3

VERTICAL PERCOLATION LAYER

THICKNESS	=	120.00 INCHES
POROSITY	=	0.5200 VOL/VOL
FIELD CAPACITY	=	0.2942 VOL/VOL
WILTING POINT	=	0.1400 VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.2102 VOL/VOL
SATURATED HYDRAULIC CONDUCTIVITY	=	0.000099999997 CM/SEC

LAYER 4

VERTICAL PERCOLATION LAYER

THICKNESS = 120.00 INCHES
POROSITY = 0.5200 VOL/VOL
FIELD CAPACITY = 0.2942 VOL/VOL
WILTING POINT = 0.1400 VOL/VOL
INITIAL SOIL WATER CONTENT = 0.2102 VOL/VOL
SATURATED HYDRAULIC CONDUCTIVITY = 0.000099999997 CM/SEC

LAYER 5

VERTICAL PERCOLATION LAYER

THICKNESS = 120.00 INCHES
POROSITY = 0.5200 VOL/VOL
FIELD CAPACITY = 0.2942 VOL/VOL
WILTING POINT = 0.1400 VOL/VOL
INITIAL SOIL WATER CONTENT = 0.2102 VOL/VOL
SATURATED HYDRAULIC CONDUCTIVITY = 0.000099999997 CM/SEC

LAYER 6

VERTICAL PERCOLATION LAYER

THICKNESS = 12.00 INCHES
POROSITY = 0.3980 VOL/VOL
FIELD CAPACITY = 0.2443 VOL/VOL
WILTING POINT = 0.1361 VOL/VOL
INITIAL SOIL WATER CONTENT = 0.2013 VOL/VOL
SATURATED HYDRAULIC CONDUCTIVITY = 0.0001199999997 CM/SEC

LAYER 7

LATERAL DRAINAGE LAYER

THICKNESS = 12.00 INCHES
POROSITY = 0.4170 VOL/VOL
FIELD CAPACITY = 0.0454 VOL/VOL
WILTING POINT = 0.0200 VOL/VOL
INITIAL SOIL WATER CONTENT = 0.0497 VOL/VOL
SATURATED HYDRAULIC CONDUCTIVITY = 0.009999999776 CM/SEC
SLOPE = 2.00 PERCENT
DRAINAGE LENGTH = 840.0 FEET

LAYER 8

BARRIER SOIL LINER WITH FLEXIBLE MEMBRANE LINER

THICKNESS = 0.30 INCHES
POROSITY = 0.4000 VOL/VOL
FIELD CAPACITY = 0.3560 VOL/VOL
WILTING POINT = 0.2899 VOL/VOL
INITIAL SOIL WATER CONTENT = 0.4000 VOL/VOL
SATURATED HYDRAULIC CONDUCTIVITY = 0.000000005000 CM/SEC

LAYER 8 (INCHES) 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001

 MONTHLY SUMMARIES FOR DAILY HEADS

AVG. DAILY HEAD ON	0.14	0.13	0.13	0.13	0.12	0.12
LAYER 8 (INCHES)	0.11	0.11	0.11	0.11	0.10	0.10
STD. DEV. OF DAILY HEAD	0.00	0.00	0.00	0.00	0.00	0.00
ON LAYER 8 (INCHES)	0.00	0.00	0.00	0.00	0.00	0.00

 ANNUAL TOTALS FOR YEAR 1

	(INCHES)	(CU. FT.)	PERCENT
	-----	-----	-----
PRECIPITATION	15.41	1.	100.00
RUNOFF	0.025	0.	0.16
EVAPOTRANSPIRATION	16.617	1.	107.84
LATERAL DRAINAGE FROM LAYER 7	0.0578	0.	0.38
PERCOLATION FROM LAYER 8	0.0009	0.	0.01
CHANGE IN WATER STORAGE	-1.291	0.	-8.38
SOIL WATER AT START OF YEAR	129.74	11.	
SOIL WATER AT END OF YEAR	128.44	11.	
SNOW WATER AT START OF YEAR	0.00	0.	
SNOW WATER AT END OF YEAR	0.00	0.	
ANNUAL WATER BUDGET BALANCE	0.00	0.	0.00

 MONTHLY TOTALS FOR YEAR 2

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
	-----	-----	-----	-----	-----	-----
PRECIPITATION (INCHES)	0.14	1.00	0.46	1.33	0.41	1.07
	1.38	6.03	3.63	0.68	0.05	0.44
RUNOFF (INCHES)	0.000	0.000	0.000	0.000	0.000	0.000
	0.000	0.000	0.410	0.000	0.000	0.000

EVAPOTRANSPIRATION	0.382	0.394	0.375	1.355	1.258	1.024
(INCHES)	1.409	6.047	3.080	0.645	0.225	0.085
LATERAL DRAINAGE FROM	0.0041	0.0037	0.0040	0.0038	0.0038	0.0036
LAYER 7 (INCHES)	0.0037	0.0036	0.0034	0.0035	0.0033	0.0033
PERCOLATION FROM	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001
LAYER 8 (INCHES)	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001

MONTHLY SUMMARIES FOR DAILY HEADS

AVG. DAILY HEAD ON	0.10	0.10	0.09	0.09	0.09	0.09
LAYER 8 (INCHES)	0.09	0.09	0.08	0.08	0.08	0.08
STD. DEV. OF DAILY HEAD	0.00	0.00	0.00	0.00	0.00	0.00
ON LAYER 8 (INCHES)	0.00	0.00	0.00	0.00	0.00	0.00

ANNUAL TOTALS FOR YEAR 2

	(INCHES)	(CU. FT.)	PERCENT
PRECIPITATION	16.62	1.	100.00
RUNOFF	0.410	0.	2.47
EVAPOTRANSPIRATION	16.280	1.	97.95
LATERAL DRAINAGE FROM LAYER 7	0.0437	0.	0.26
PERCOLATION FROM LAYER 8	0.0008	0.	0.00
CHANGE IN WATER STORAGE	-0.114	0.	-0.69
SOIL WATER AT START OF YEAR	128.44	11.	
SOIL WATER AT END OF YEAR	128.33	11.	
SNOW WATER AT START OF YEAR	0.00	0.	
SNOW WATER AT END OF YEAR	0.00	0.	
ANNUAL WATER BUDGET BALANCE	0.00	0.	0.00

MONTHLY TOTALS FOR YEAR 3

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
PRECIPITATION (INCHES)	0.33 1.71	0.17 2.54	0.92 4.79	1.20 2.21	0.21 1.00	6.80 0.86
RUNOFF (INCHES)	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.864 0.000
EVAPOTRANSPIRATION (INCHES)	0.308 1.794	0.267 2.535	0.448 3.120	1.811 2.549	0.314 1.043	5.351 1.186
LATERAL DRAINAGE FROM LAYER 7 (INCHES)	0.0033 0.0030	0.0029 0.0030	0.0032 0.0028	0.0030 0.0029	0.0031 0.0027	0.0029 0.0028
PERCOLATION FROM LAYER 8 (INCHES)	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001

MONTHLY SUMMARIES FOR DAILY HEADS

AVG. DAILY HEAD ON LAYER 8 (INCHES)	0.08 0.07	0.08 0.07	0.08 0.07	0.07 0.07	0.07 0.07	0.07 0.07
STD. DEV. OF DAILY HEAD ON LAYER 8 (INCHES)	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00

ANNUAL TOTALS FOR YEAR 3

	(INCHES)	(CU. FT.)	PERCENT
PRECIPITATION	22.74	2.	100.00
RUNOFF	0.864	0.	3.80
EVAPOTRANSPIRATION	20.727	2.	91.15
LATERAL DRAINAGE FROM LAYER 7	0.0357	0.	0.16
PERCOLATION FROM LAYER 8	0.0008	0.	0.00
CHANGE IN WATER STORAGE	1.113	0.	4.89
SOIL WATER AT START OF YEAR	128.33	11.	
SOIL WATER AT END OF YEAR	129.44	11.	
SNOW WATER AT START OF YEAR	0.00	0.	
SNOW WATER AT END OF YEAR	0.00	0.	
ANNUAL WATER BUDGET BALANCE	0.00	0.	0.00

 MONTHLY TOTALS FOR YEAR 4

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
PRECIPITATION (INCHES)	0.04 0.77	0.26 2.00	0.82 3.69	0.03 0.00	1.27 0.26	2.57 0.00
RUNOFF (INCHES)	0.000 0.000	0.000 0.027	0.000 0.358	0.000 0.000	0.000 0.000	0.023 0.000
EVAPOTRANSPIRATION (INCHES)	0.747 0.864	0.288 1.108	0.372 2.518	0.344 1.710	1.381 0.225	2.522 0.000
LATERAL DRAINAGE FROM LAYER 7 (INCHES)	0.0028 0.0026	0.0026 0.0025	0.0027 0.0024	0.0026 0.0025	0.0026 0.0024	0.0025 0.0024
PERCOLATION FROM LAYER 8 (INCHES)	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001

 MONTHLY SUMMARIES FOR DAILY HEADS

AVG. DAILY HEAD ON LAYER 8 (INCHES)	0.07 0.06	0.07 0.06	0.06 0.06	0.06 0.06	0.06 0.06	0.06 0.06
STD. DEV. OF DAILY HEAD ON LAYER 8 (INCHES)	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00

 ANNUAL TOTALS FOR YEAR 4

	(INCHES)	(CU. FT.)	PERCENT
PRECIPITATION	11.71	1.	100.00
RUNOFF	0.409	0.	3.49
EVAPOTRANSPIRATION	12.081	1.	103.16
LATERAL DRAINAGE FROM LAYER 7	0.0307	0.	0.26
PERCOLATION FROM LAYER 8	0.0008	0.	0.01
CHANGE IN WATER STORAGE	-0.811	0.	-6.93
SOIL WATER AT START OF YEAR	129.44	11.	
SOIL WATER AT END OF YEAR	128.63	11.	
SNOW WATER AT START OF YEAR	0.00	0.	

SNOW WATER AT END OF YEAR	0.00	0.	
ANNUAL WATER BUDGET BALANCE	0.00	0.	0.00

MONTHLY TOTALS FOR YEAR 5

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
PRECIPITATION (INCHES)	0.45 2.81	0.87 2.34	0.67 1.26	0.21 0.59	1.08 0.83	4.53 0.75
RUNOFF (INCHES)	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.106 0.000
EVAPOTRANSPIRATION (INCHES)	0.168 2.810	0.367 2.300	0.310 1.304	0.300 0.586	1.434 0.423	5.127 0.519
LATERAL DRAINAGE FROM LAYER 7 (INCHES)	0.0024 0.0023	0.0022 0.0023	0.0024 0.0022	0.0023 0.0022	0.0023 0.0021	0.0022 0.0022
PERCOLATION FROM LAYER 8 (INCHES)	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001

MONTHLY SUMMARIES FOR DAILY HEADS

AVG. DAILY HEAD ON LAYER 8 (INCHES)	0.06 0.05	0.06 0.05	0.06 0.05	0.06 0.05	0.06 0.05	0.06 0.05
STD. DEV. OF DAILY HEAD ON LAYER 8 (INCHES)	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00

ANNUAL TOTALS FOR YEAR 5

	(INCHES)	(CU. FT.)	PERCENT
PRECIPITATION	16.39	1.	100.00
RUNOFF	0.106	0.	0.64
EVAPOTRANSPIRATION	15.647	1.	95.47
LATERAL DRAINAGE FROM LAYER 7	0.0271	0.	0.17
PERCOLATION FROM LAYER 8	0.0007	0.	0.00

AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1 THROUGH 5

	(INCHES)	(CU. FT.)	PERCENT
PRECIPITATION	16.57 (3.971)	1.	100.00
RUNOFF	0.363 (0.330)	0.	2.19
EVAPOTRANSPIRATION	16.270 (3.079)	1.	98.17
LATERAL DRAINAGE FROM LAYER 7	0.0390 (0.0122)	0.	0.24
PERCOLATION FROM LAYER 8	0.0008 (0.0001)	0.	0.00
CHANGE IN WATER STORAGE	-0.099 (0.987)	0.	-0.60

PEAK DAILY VALUES FOR YEARS 1 THROUGH 5

	(INCHES)	(CU. FT.)
PRECIPITATION	2.82	0.2
RUNOFF	0.544	0.0
LATERAL DRAINAGE FROM LAYER 7	0.0002	0.0
PERCOLATION FROM LAYER 8	0.0000	0.0
HEAD ON LAYER 8	0.1	
SNOW WATER	0.03	0.0
MAXIMUM VEG. SOIL WATER (VOL/VOL)	0.3201	
MINIMUM VEG. SOIL WATER (VOL/VOL)	0.1355	

FINAL WATER STORAGE AT END OF YEAR 5

LAYER	(INCHES)	(VOL/VOL)
1	2.27	0.1892
2	48.33	0.2014

3	25.19	0.2100
4	25.22	0.2102
5	25.22	0.2102
6	2.32	0.1930
7	0.56	0.0470
8	0.12	0.4000

SNOW WATER 0.00

Amarillo - 20 years, CN=90, RoC=1.0
seven lifts of waste with final cover (24" SC & 12 " CCL)
NOVEMBER 29, 1994

LAYER 1

VERTICAL PERCOLATION LAYER

THICKNESS	=	24.00 INCHES
POROSITY	=	0.4640 VOL/VOL
FIELD CAPACITY	=	0.3104 VOL/VOL
WILTING POINT	=	0.1875 VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.1892 VOL/VOL
SATURATED HYDRAULIC CONDUCTIVITY	=	0.000010000000 CM/SEC

LAYER 2

BARRIER SOIL LINER

THICKNESS	=	12.00 INCHES
POROSITY	=	0.4224 VOL/VOL
FIELD CAPACITY	=	0.3495 VOL/VOL
WILTING POINT	=	0.2648 VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.2648 VOL/VOL
SATURATED HYDRAULIC CONDUCTIVITY	=	0.000010000000 CM/SEC

LAYER 3

VERTICAL PERCOLATION LAYER

THICKNESS	=	240.00 INCHES
POROSITY	=	0.5200 VOL/VOL
FIELD CAPACITY	=	0.2942 VOL/VOL
WILTING POINT	=	0.1400 VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.2000 VOL/VOL
SATURATED HYDRAULIC CONDUCTIVITY	=	0.000099999997 CM/SEC

LAYER 4

VERTICAL PERCOLATION LAYER

THICKNESS = 240.00 INCHES
 POROSITY = 0.5200 VOL/VOL
 FIELD CAPACITY = 0.2942 VOL/VOL
 WILTING POINT = 0.1400 VOL/VOL
 INITIAL SOIL WATER CONTENT = 0.2014 VOL/VOL
 SATURATED HYDRAULIC CONDUCTIVITY = 0.000099999997 CM/SEC

LAYER 5

VERTICAL PERCOLATION LAYER

THICKNESS = 120.00 INCHES
 POROSITY = 0.5200 VOL/VOL
 FIELD CAPACITY = 0.2942 VOL/VOL
 WILTING POINT = 0.1400 VOL/VOL
 INITIAL SOIL WATER CONTENT = 0.2100 VOL/VOL
 SATURATED HYDRAULIC CONDUCTIVITY = 0.000099999997 CM/SEC

LAYER 6

VERTICAL PERCOLATION LAYER

THICKNESS = 120.00 INCHES
 POROSITY = 0.5200 VOL/VOL
 FIELD CAPACITY = 0.2942 VOL/VOL
 WILTING POINT = 0.1400 VOL/VOL
 INITIAL SOIL WATER CONTENT = 0.2102 VOL/VOL
 SATURATED HYDRAULIC CONDUCTIVITY = 0.000099999997 CM/SEC

LAYER 7

VERTICAL PERCOLATION LAYER

THICKNESS = 120.00 INCHES
 POROSITY = 0.5200 VOL/VOL
 FIELD CAPACITY = 0.2942 VOL/VOL
 WILTING POINT = 0.1400 VOL/VOL
 INITIAL SOIL WATER CONTENT = 0.2102 VOL/VOL
 SATURATED HYDRAULIC CONDUCTIVITY = 0.000099999997 CM/SEC

LAYER 8

VERTICAL PERCOLATION LAYER

THICKNESS = 12.00 INCHES
 POROSITY = 0.3980 VOL/VOL
 FIELD CAPACITY = 0.2443 VOL/VOL
 WILTING POINT = 0.1361 VOL/VOL
 INITIAL SOIL WATER CONTENT = 0.1930 VOL/VOL
 SATURATED HYDRAULIC CONDUCTIVITY = 0.000119999997 CM/SEC

LAYER 9

LATERAL DRAINAGE LAYER

THICKNESS = 12.00 INCHES
POROSITY = 0.4170 VOL/VOL
FIELD CAPACITY = 0.0454 VOL/VOL
WILTING POINT = 0.0200 VOL/VOL
INITIAL SOIL WATER CONTENT = 0.0470 VOL/VOL
SATURATED HYDRAULIC CONDUCTIVITY = 0.009999999776 CM/SEC
SLOPE = 2.00 PERCENT
DRAINAGE LENGTH = 840.0 FEET

LAYER 10

BARRIER SOIL LINER WITH FLEXIBLE MEMBRANE LINER

THICKNESS = 0.30 INCHES
POROSITY = 0.4000 VOL/VOL
FIELD CAPACITY = 0.3560 VOL/VOL
WILTING POINT = 0.2899 VOL/VOL
INITIAL SOIL WATER CONTENT = 0.4000 VOL/VOL
SATURATED HYDRAULIC CONDUCTIVITY = 0.000000005000 CM/SEC
LINER LEAKAGE FRACTION = 0.01000000

GENERAL SIMULATION DATA

SCS RUNOFF CURVE NUMBER = 90.00
TOTAL AREA OF COVER = 1. SQ FT
EVAPORATIVE ZONE DEPTH = 22.00 INCHES
POTENTIAL RUNOFF FRACTION = 1.000000
UPPER LIMIT VEG. STORAGE = 10.2080 INCHES
INITIAL VEG. STORAGE = 4.1624 INCHES
INITIAL SNOW WATER CONTENT = 0.0000 INCHES
INITIAL TOTAL WATER STORAGE IN
SOIL AND WASTE LAYERS = 182.7024 INCHES

SOIL WATER CONTENT INITIALIZED BY USER.

CLIMATOLOGICAL DATA

SYNTHETIC RAINFALL WITH SYNTHETIC DAILY TEMPERATURES AND
SOLAR RADIATION FOR AMARILLO TEXAS

MAXIMUM LEAF AREA INDEX = 3.30
START OF GROWING SEASON (JULIAN DATE) = 104
END OF GROWING SEASON (JULIAN DATE) = 302

NORMAL MEAN MONTHLY TEMPERATURES, DEGREES FAHRENHEIT

JAN/JUL FEB/AUG MAR/SEP APR/OCT MAY/NOV JUN/DEC

35.10	39.20	47.10	56.80	65.40	74.10
78.60	76.50	69.10	58.50	46.00	36.90

MONTHLY TOTALS FOR YEAR 1

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
PRECIPITATION (INCHES)	0.40 3.01	0.35 3.57	1.70 0.80	0.04 1.86	0.15 1.14	1.54 0.85
RUNOFF (INCHES)	0.000 0.706	0.011 0.695	0.281 0.013	0.000 0.440	0.000 0.592	0.109 0.000
EVAPOTRANSPIRATION (INCHES)	0.149 2.495	0.487 3.036	1.475 0.702	0.120 1.505	0.100 0.548	1.133 0.398
PERCOLATION FROM LAYER 2 (INCHES)	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
LATERAL DRAINAGE FROM LAYER 9 (INCHES)	0.0021 0.0021	0.0019 0.0021	0.0021 0.0020	0.0020 0.0020	0.0021 0.0020	0.0020 0.0020
PERCOLATION FROM LAYER 10 (INCHES)	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001

MONTHLY SUMMARIES FOR DAILY HEADS

AVG. DAILY HEAD ON LAYER 2 (INCHES)	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00
STD. DEV. OF DAILY HEAD ON LAYER 2 (INCHES)	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00
AVG. DAILY HEAD ON LAYER 10 (INCHES)	0.05 0.05	0.05 0.05	0.05 0.05	0.05 0.05	0.05 0.05	0.05 0.05
STD. DEV. OF DAILY HEAD ON LAYER 10 (INCHES)	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00

ANNUAL TOTALS FOR YEAR 1

	(INCHES)	(CU. FT.)	PERCENT
PRECIPITATION	15.41	1.	100.00
RUNOFF	2.847	0.	18.47
EVAPOTRANSPIRATION	12.149	1.	78.84

PERCOLATION FROM LAYER 2	0.0000	0.	0.00
LATERAL DRAINAGE FROM LAYER 9	0.0244	0.	0.16
PERCOLATION FROM LAYER 10	0.0007	0.	0.00
CHANGE IN WATER STORAGE	0.389	0.	2.52
SOIL WATER AT START OF YEAR	182.70	15.	
SOIL WATER AT END OF YEAR	183.09	15.	
SNOW WATER AT START OF YEAR	0.00	0.	
SNOW WATER AT END OF YEAR	0.00	0.	
ANNUAL WATER BUDGET BALANCE	0.00	0.	0.00

MONTHLY TOTALS FOR YEAR 2

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
PRECIPITATION (INCHES)	0.14 1.38	1.00 6.03	0.46 3.63	1.33 0.68	0.41 0.05	1.07 0.44
RUNOFF (INCHES)	0.000 0.000	0.068 2.513	0.000 1.890	0.007 0.053	0.000 0.000	0.054 0.016
EVAPOTRANSPIRATION (INCHES)	0.330 1.417	0.372 3.521	0.565 1.579	1.582 0.601	0.840 0.237	1.001 0.084
PERCOLATION FROM LAYER 2 (INCHES)	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
LATERAL DRAINAGE FROM LAYER 9 (INCHES)	0.0020 0.0019	0.0018 0.0019	0.0020 0.0018	0.0019 0.0019	0.0019 0.0018	0.0019 0.0019
PERCOLATION FROM LAYER 10 (INCHES)	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001

MONTHLY SUMMARIES FOR DAILY HEADS

AVG. DAILY HEAD ON LAYER 2 (INCHES)	0.00	0.00	0.00	0.00	0.00	0.00
STD. DEV. OF DAILY HEAD ON LAYER 2 (INCHES)	0.00	0.00	0.00	0.00	0.00	0.00
AVG. DAILY HEAD ON LAYER 10 (INCHES)	0.05	0.05	0.05	0.05	0.05	0.05

STD. DEV. OF DAILY HEAD	0.00	0.00	0.00	0.00	0.00	0.00
ON LAYER 10 (INCHES)	0.00	0.00	0.00	0.00	0.00	0.00

ANNUAL TOTALS FOR YEAR 2

	(INCHES)	(CU. FT.)	PERCENT
PRECIPITATION	16.62	1.	100.00
RUNOFF	4.602	0.	27.69
EVAPOTRANSPIRATION	12.130	1.	72.99
PERCOLATION FROM LAYER 2	0.0000	0.	0.00
LATERAL DRAINAGE FROM LAYER 9	0.0226	0.	0.14
PERCOLATION FROM LAYER 10	0.0007	0.	0.00
CHANGE IN WATER STORAGE	-0.135	0.	-0.81
SOIL WATER AT START OF YEAR	183.09	15.	
SOIL WATER AT END OF YEAR	182.96	15.	
SNOW WATER AT START OF YEAR	0.00	0.	
SNOW WATER AT END OF YEAR	0.00	0.	
ANNUAL WATER BUDGET BALANCE	0.00	0.	0.00

MONTHLY TOTALS FOR YEAR 3

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
PRECIPITATION (INCHES)	0.33 1.71	0.17 2.54	0.92 4.79	1.20 2.21	0.21 1.00	6.80 0.86
RUNOFF (INCHES)	0.000 0.166	0.000 0.772	0.058 1.463	0.288 0.228	0.000 0.264	4.576 0.004
EVAPOTRANSPIRATION (INCHES)	0.259 1.539	0.232 1.765	1.142 2.674	0.989 2.479	0.162 0.406	2.271 1.225
PERCOLATION FROM LAYER 2 (INCHES)	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
LATERAL DRAINAGE FROM	0.0018	0.0017	0.0018	0.0018	0.0018	0.0017

LAYER 9 (INCHES)	0.0018	0.0018	0.0017	0.0018	0.0017	0.0017
PERCOLATION FROM	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001
LAYER 10 (INCHES)	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001

MONTHLY SUMMARIES FOR DAILY HEADS

AVG. DAILY HEAD ON	0.00	0.00	0.00	0.00	0.00	0.00
LAYER 2 (INCHES)	0.00	0.00	0.00	0.00	0.00	0.00
STD. DEV. OF DAILY HEAD	0.00	0.00	0.00	0.00	0.00	0.00
ON LAYER 2 (INCHES)	0.00	0.00	0.00	0.00	0.00	0.00
AVG. DAILY HEAD ON	0.04	0.04	0.04	0.04	0.04	0.04
LAYER 10 (INCHES)	0.04	0.04	0.04	0.04	0.04	0.04
STD. DEV. OF DAILY HEAD	0.00	0.00	0.00	0.00	0.00	0.00
ON LAYER 10 (INCHES)	0.00	0.00	0.00	0.00	0.00	0.00

ANNUAL TOTALS FOR YEAR 3

	(INCHES)	(CU. FT.)	PERCENT
	-----	-----	-----
PRECIPITATION	22.74	2.	100.00
RUNOFF	7.819	1.	34.38
EVAPOTRANSPIRATION	15.144	1.	66.60
PERCOLATION FROM LAYER 2	0.0000	0.	0.00
LATERAL DRAINAGE FROM LAYER 9	0.0211	0.	0.09
PERCOLATION FROM LAYER 10	0.0007	0.	0.00
CHANGE IN WATER STORAGE	-0.244	0.	-1.07
SOIL WATER AT START OF YEAR	182.96	15.	
SOIL WATER AT END OF YEAR	182.71	15.	
SNOW WATER AT START OF YEAR	0.00	0.	
SNOW WATER AT END OF YEAR	0.00	0.	
ANNUAL WATER BUDGET BALANCE	0.00	0.	0.00

MONTHLY TOTALS FOR YEAR 4

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
PRECIPITATION (INCHES)	0.04 0.77	0.26 2.00	0.82 3.69	0.03 0.00	1.27 0.26	2.57 0.00
RUNOFF (INCHES)	0.000 0.019	0.000 0.621	0.006 2.107	0.000 0.000	0.413 0.000	0.715 0.000
EVAPOTRANSPIRATION (INCHES)	0.157 0.844	0.214 1.037	0.451 1.531	0.307 0.393	0.988 0.260	1.763 0.000
PERCOLATION FROM LAYER 2 (INCHES)	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
LATERAL DRAINAGE FROM LAYER 9 (INCHES)	0.0017 0.0017	0.0016 0.0017	0.0017 0.0016	0.0017 0.0017	0.0017 0.0016	0.0016 0.0016
PERCOLATION FROM LAYER 10 (INCHES)	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001

MONTHLY SUMMARIES FOR DAILY HEADS

AVG. DAILY HEAD ON LAYER 2 (INCHES)	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00
STD. DEV. OF DAILY HEAD ON LAYER 2 (INCHES)	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00
AVG. DAILY HEAD ON LAYER 10 (INCHES)	0.04 0.04	0.04 0.04	0.04 0.04	0.04 0.04	0.04 0.04	0.04 0.04
STD. DEV. OF DAILY HEAD ON LAYER 10 (INCHES)	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00

ANNUAL TOTALS FOR YEAR 4

	(INCHES)	(CU. FT.)	PERCENT
PRECIPITATION	11.71	1.	100.00
RUNOFF	3.880	0.	33.14
EVAPOTRANSPIRATION	7.947	1.	67.86
PERCOLATION FROM LAYER 2	0.0000	0.	0.00
LATERAL DRAINAGE FROM LAYER 9	0.0200	0.	0.17
PERCOLATION FROM LAYER 10	0.0007	0.	0.01
CHANGE IN WATER STORAGE	-0.138	0.	-1.18

SOIL WATER AT START OF YEAR	182.71	15.	
SOIL WATER AT END OF YEAR	182.57	15.	
SNOW WATER AT START OF YEAR	0.00	0.	
SNOW WATER AT END OF YEAR	0.00	0.	
ANNUAL WATER BUDGET BALANCE	0.00	0.	0.00

MONTHLY TOTALS FOR YEAR 5

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
PRECIPITATION (INCHES)	0.45 2.81	0.87 2.34	0.67 1.26	0.21 0.59	1.08 0.83	4.53 0.75
RUNOFF (INCHES)	0.076 0.772	0.262 0.572	0.011 0.158	0.000 0.172	0.207 0.114	1.643 0.000
EVAPOTRANSPIRATION (INCHES)	0.146 2.038	0.384 1.656	0.316 1.215	0.296 0.418	1.580 0.420	2.887 0.498
PERCOLATION FROM LAYER 2 (INCHES)	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
LATERAL DRAINAGE FROM LAYER 9 (INCHES)	0.0016 0.0016	0.0015 0.0016	0.0016 0.0015	0.0016 0.0016	0.0016 0.0015	0.0016 0.0016
PERCOLATION FROM LAYER 10 (INCHES)	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001

MONTHLY SUMMARIES FOR DAILY HEADS

AVG. DAILY HEAD ON LAYER 2 (INCHES)	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00
STD. DEV. OF DAILY HEAD ON LAYER 2 (INCHES)	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00
AVG. DAILY HEAD ON LAYER 10 (INCHES)	0.04 0.04	0.04 0.04	0.04 0.04	0.04 0.04	0.04 0.04	0.04 0.04
STD. DEV. OF DAILY HEAD ON LAYER 10 (INCHES)	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00

ANNUAL TOTALS FOR YEAR 5

	(INCHES)	(CU. FT.)	PERCENT
PRECIPITATION	16.39	1.	100.00
RUNOFF	3.987	0.	24.33
EVAPOTRANSPIRATION	11.855	1.	72.33
PERCOLATION FROM LAYER 2	0.0000	0.	0.00
LATERAL DRAINAGE FROM LAYER 9	0.0189	0.	0.12
PERCOLATION FROM LAYER 10	0.0007	0.	0.00
CHANGE IN WATER STORAGE	0.528	0.	3.22
SOIL WATER AT START OF YEAR	182.57	15.	
SOIL WATER AT END OF YEAR	183.10	15.	
SNOW WATER AT START OF YEAR	0.00	0.	
SNOW WATER AT END OF YEAR	0.00	0.	
ANNUAL WATER BUDGET BALANCE	0.00	0.	0.00

MONTHLY TOTALS FOR YEAR 6

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
PRECIPITATION (INCHES)	0.59 2.28	1.56 1.59	2.31 2.13	0.22 2.39	2.72 0.04	6.74 1.40
RUNOFF (INCHES)	0.012 0.330	0.000 0.291	0.159 0.451	0.000 0.617	0.359 0.000	3.026 0.118
EVAPOTRANSPIRATION (INCHES)	0.375 2.441	0.996 1.809	2.167 1.202	1.519 1.665	2.362 0.625	2.712 0.744
PERCOLATION FROM LAYER 2 (INCHES)	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
LATERAL DRAINAGE FROM LAYER 9 (INCHES)	0.0016 0.0015	0.0014 0.0015	0.0016 0.0015	0.0015 0.0015	0.0015 0.0015	0.0015 0.0015
PERCOLATION FROM LAYER 10 (INCHES)	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001

MONTHLY SUMMARIES FOR DAILY HEADS

AVG. DAILY HEAD ON LAYER 2 (INCHES)	0.00	0.00	0.00	0.00	0.00	0.00
STD. DEV. OF DAILY HEAD ON LAYER 2 (INCHES)	0.00	0.00	0.00	0.00	0.00	0.00
AVG. DAILY HEAD ON LAYER 10 (INCHES)	0.04	0.04	0.04	0.04	0.04	0.04
STD. DEV. OF DAILY HEAD ON LAYER 10 (INCHES)	0.00	0.00	0.00	0.00	0.00	0.00

ANNUAL TOTALS FOR YEAR 6

	(INCHES)	(CU. FT.)	PERCENT
PRECIPITATION	23.97	2.	100.00
RUNOFF	5.364	0.	22.38
EVAPOTRANSPIRATION	18.616	2.	77.66
PERCOLATION FROM LAYER 2	0.0000	0.	0.00
LATERAL DRAINAGE FROM LAYER 9	0.0181	0.	0.08
PERCOLATION FROM LAYER 10	0.0007	0.	0.00
CHANGE IN WATER STORAGE	-0.029	0.	-0.12
SOIL WATER AT START OF YEAR	183.10	15.	
SOIL WATER AT END OF YEAR	183.07	15.	
SNOW WATER AT START OF YEAR	0.00	0.	
SNOW WATER AT END OF YEAR	0.00	0.	
ANNUAL WATER BUDGET BALANCE	0.00	0.	0.00

MONTHLY TOTALS FOR YEAR 7

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
PRECIPITATION (INCHES)	0.29	0.04	0.35	2.49	2.82	2.65
	1.37	2.08	0.08	2.19	1.96	0.51

RUNOFF (INCHES)	0.000	0.000	0.000	0.555	0.730	0.814
	0.217	0.413	0.000	0.883	0.200	0.001
EVAPOTRANSPIRATION (INCHES)	0.828	0.040	0.290	1.967	2.120	1.709
	1.072	1.874	0.080	0.968	1.586	0.925
PERCOLATION FROM LAYER 2 (INCHES)	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
LATERAL DRAINAGE FROM LAYER 9 (INCHES)	0.0015	0.0014	0.0015	0.0014	0.0015	0.0014
	0.0015	0.0015	0.0014	0.0015	0.0014	0.0015
PERCOLATION FROM LAYER 10 (INCHES)	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001
	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001

 MONTHLY SUMMARIES FOR DAILY HEADS

AVG. DAILY HEAD ON LAYER 2 (INCHES)	0.00	0.00	0.00	0.00	0.00	0.00
	0.00	0.00	0.00	0.00	0.00	0.00
STD. DEV. OF DAILY HEAD ON LAYER 2 (INCHES)	0.00	0.00	0.00	0.00	0.00	0.00
	0.00	0.00	0.00	0.00	0.00	0.00
AVG. DAILY HEAD ON LAYER 10 (INCHES)	0.04	0.04	0.04	0.04	0.04	0.04
	0.04	0.04	0.04	0.03	0.03	0.03
STD. DEV. OF DAILY HEAD ON LAYER 10 (INCHES)	0.00	0.00	0.00	0.00	0.00	0.00
	0.00	0.00	0.00	0.00	0.00	0.00

 ANNUAL TOTALS FOR YEAR 7

	(INCHES)	(CU. FT.)	PERCENT
	-----	-----	-----
PRECIPITATION	16.83	1.	100.00
RUNOFF	3.814	0.	22.66
EVAPOTRANSPIRATION	13.457	1.	79.96
PERCOLATION FROM LAYER 2	0.0000	0.	0.00
LATERAL DRAINAGE FROM LAYER 9	0.0174	0.	0.10
PERCOLATION FROM LAYER 10	0.0007	0.	0.00
CHANGE IN WATER STORAGE	-0.459	0.	-2.73
SOIL WATER AT START OF YEAR	183.07	15.	
SOIL WATER AT END OF YEAR	182.61	15.	
SNOW WATER AT START OF YEAR	0.00	0.	
SNOW WATER AT END OF YEAR	0.00	0.	
ANNUAL WATER BUDGET BALANCE	0.00	0.	0.00

 MONTHLY TOTALS FOR YEAR 8

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
PRECIPITATION (INCHES)	0.59 0.37	0.54 3.58	1.32 3.05	2.18 2.41	5.74 0.00	7.26 0.95
RUNOFF (INCHES)	0.001 0.000	0.000 2.158	0.289 0.668	0.794 0.342	2.192 0.000	3.822 0.326
EVAPOTRANSPIRATION (INCHES)	0.685 0.775	0.470 1.422	0.857 2.137	1.630 1.474	3.089 0.840	3.492 0.624
PERCOLATION FROM LAYER 2 (INCHES)	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
LATERAL DRAINAGE FROM LAYER 9 (INCHES)	0.0014 0.0014	0.0014 0.0014	0.0014 0.0014	0.0014 0.0014	0.0014 0.0014	0.0014 0.0014
PERCOLATION FROM LAYER 10 (INCHES)	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001

 MONTHLY SUMMARIES FOR DAILY HEADS

AVG. DAILY HEAD ON LAYER 2 (INCHES)	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00
STD. DEV. OF DAILY HEAD ON LAYER 2 (INCHES)	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00
AVG. DAILY HEAD ON LAYER 10 (INCHES)	0.03 0.03	0.03 0.03	0.03 0.03	0.03 0.03	0.03 0.03	0.03 0.03
STD. DEV. OF DAILY HEAD ON LAYER 10 (INCHES)	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00

 ANNUAL TOTALS FOR YEAR 8

	(INCHES)	(CU. FT.)	PERCENT
PRECIPITATION	27.99	2.	100.00
RUNOFF	10.592	1.	37.84

LATERAL DRAINAGE FROM	0.0014	0.0012	0.0014	0.0013	0.0014	0.0013
LAYER 9 (INCHES)	0.0013	0.0013	0.0013	0.0013	0.0013	0.0013
PERCOLATION FROM	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001
LAYER 10 (INCHES)	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001

MONTHLY SUMMARIES FOR DAILY HEADS

AVG. DAILY HEAD ON	0.00	0.00	0.00	0.00	0.00	0.00
LAYER 2 (INCHES)	0.00	0.00	0.00	0.00	0.00	0.00
STD. DEV. OF DAILY HEAD	0.00	0.00	0.00	0.00	0.00	0.00
ON LAYER 2 (INCHES)	0.00	0.00	0.00	0.00	0.00	0.00
AVG. DAILY HEAD ON	0.03	0.03	0.03	0.03	0.03	0.03
LAYER 10 (INCHES)	0.03	0.03	0.03	0.03	0.03	0.03
STD. DEV. OF DAILY HEAD	0.00	0.00	0.00	0.00	0.00	0.00
ON LAYER 10 (INCHES)	0.00	0.00	0.00	0.00	0.00	0.00

ANNUAL TOTALS FOR YEAR 10

	(INCHES)	(CU. FT.)	PERCENT
	-----	-----	-----
PRECIPITATION	19.77	2.	100.00
RUNOFF	4.495	0.	22.73
EVAPOTRANSPIRATION	15.285	1.	77.31
PERCOLATION FROM LAYER 2	0.0000	0.	0.00
LATERAL DRAINAGE FROM LAYER 9	0.0159	0.	0.08
PERCOLATION FROM LAYER 10	0.0007	0.	0.00
CHANGE IN WATER STORAGE	-0.026	0.	-0.13
SOIL WATER AT START OF YEAR	182.49	15.	
SOIL WATER AT END OF YEAR	182.47	15.	
SNOW WATER AT START OF YEAR	0.00	0.	
SNOW WATER AT END OF YEAR	0.00	0.	
ANNUAL WATER BUDGET BALANCE	0.00	0.	0.00

MONTHLY TOTALS FOR YEAR 11

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
PRECIPITATION (INCHES)	0.61 2.81	0.53 2.03	1.23 2.67	0.30 0.00	2.15 0.49	4.71 0.41
RUNOFF (INCHES)	0.002 0.756	0.006 0.402	0.178 1.367	0.012 0.000	0.456 0.011	1.544 0.000
EVAPOTRANSPIRATION (INCHES)	0.608 2.257	0.401 1.650	0.691 1.303	0.773 0.000	1.681 0.069	2.954 0.378
PERCOLATION FROM LAYER 2 (INCHES)	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
LATERAL DRAINAGE FROM LAYER 9 (INCHES)	0.0013 0.0013	0.0012 0.0013	0.0013 0.0013	0.0013 0.0013	0.0013 0.0013	0.0013 0.0013
PERCOLATION FROM LAYER 10 (INCHES)	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001

MONTHLY SUMMARIES FOR DAILY HEADS

AVG. DAILY HEAD ON LAYER 2 (INCHES)	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00
STD. DEV. OF DAILY HEAD ON LAYER 2 (INCHES)	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00
AVG. DAILY HEAD ON LAYER 10 (INCHES)	0.03 0.03	0.03 0.03	0.03 0.03	0.03 0.03	0.03 0.03	0.03 0.03
STD. DEV. OF DAILY HEAD ON LAYER 10 (INCHES)	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00

ANNUAL TOTALS FOR YEAR 11

	(INCHES)	(CU. FT.)	PERCENT
PRECIPITATION	17.94	1.	100.00
RUNOFF	4.733	0.	26.38
EVAPOTRANSPIRATION	12.766	1.	71.16
PERCOLATION FROM LAYER 2	0.0000	0.	0.00
LATERAL DRAINAGE FROM LAYER 9	0.0155	0.	0.09
PERCOLATION FROM LAYER 10	0.0007	0.	0.00
CHANGE IN WATER STORAGE	0.425	0.	2.37

SOIL WATER AT START OF YEAR	182.47	15.	
SOIL WATER AT END OF YEAR	182.89	15.	
SNOW WATER AT START OF YEAR	0.00	0.	
SNOW WATER AT END OF YEAR	0.00	0.	
ANNUAL WATER BUDGET BALANCE	0.00	0.	0.00

MONTHLY TOTALS FOR YEAR 12

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
PRECIPITATION (INCHES)	0.59 2.22	0.61 6.97	0.00 1.39	0.00 0.17	3.81 0.25	6.37 0.20
RUNOFF (INCHES)	0.012 0.309	0.089 4.781	0.000 0.267	0.000 0.000	2.057 0.000	3.486 0.000
VAPOTRANSPIRATION (INCHES)	0.370 1.969	0.319 1.826	0.210 1.238	0.260 0.493	1.960 0.250	2.926 0.089
PERCOLATION FROM LAYER 2 (INCHES)	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
LATERAL DRAINAGE FROM LAYER 9 (INCHES)	0.0013 0.0013	0.0012 0.0013	0.0013 0.0012	0.0013 0.0013	0.0013 0.0012	0.0012 0.0013
PERCOLATION FROM LAYER 10 (INCHES)	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001

MONTHLY SUMMARIES FOR DAILY HEADS

AVG. DAILY HEAD ON LAYER 2 (INCHES)	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00
STD. DEV. OF DAILY HEAD ON LAYER 2 (INCHES)	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00
AVG. DAILY HEAD ON LAYER 10 (INCHES)	0.03 0.03	0.03 0.03	0.03 0.03	0.03 0.03	0.03 0.03	0.03 0.03
STD. DEV. OF DAILY HEAD ON LAYER 10 (INCHES)	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00

 ANNUAL TOTALS FOR YEAR 12

	(INCHES)	(CU. FT.)	PERCENT
PRECIPITATION	22.58	2.	100.00
RUNOFF	11.001	1.	48.72
EVAPOTRANSPIRATION	11.910	1.	52.75
PERCOLATION FROM LAYER 2	0.0000	0.	0.00
LATERAL DRAINAGE FROM LAYER 9	0.0152	0.	0.07
PERCOLATION FROM LAYER 10	0.0007	0.	0.00
CHANGE IN WATER STORAGE	-0.347	0.	-1.53
SOIL WATER AT START OF YEAR	182.89	15.	
SOIL WATER AT END OF YEAR	182.54	15.	
SNOW WATER AT START OF YEAR	0.00	0.	
SNOW WATER AT END OF YEAR	0.00	0.	
ANNUAL WATER BUDGET BALANCE	0.00	0.	0.00

 MONTHLY TOTALS FOR YEAR 13

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
PRECIPITATION (INCHES)	0.26 1.08	0.15 4.26	0.32 0.64	2.47 0.21	2.39 0.00	2.69 0.48
RUNOFF (INCHES)	0.000 0.012	0.000 1.363	0.013 0.051	1.482 0.000	0.844 0.000	1.124 0.007
EVAPOTRANSPIRATION (INCHES)	0.310 1.038	0.180 2.927	0.120 0.589	0.610 0.136	2.056 0.074	1.652 0.210
PERCOLATION FROM LAYER 2 (INCHES)	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
LATERAL DRAINAGE FROM LAYER 9 (INCHES)	0.0013 0.0013	0.0011 0.0013	0.0013 0.0012	0.0012 0.0013	0.0013 0.0012	0.0012 0.0013
PERCOLATION FROM LAYER 10 (INCHES)	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001

 MONTHLY SUMMARIES FOR DAILY HEADS

AVG. DAILY HEAD ON LAYER 2 (INCHES)	0.00	0.00	0.00	0.00	0.00	0.00
STD. DEV. OF DAILY HEAD ON LAYER 2 (INCHES)	0.00	0.00	0.00	0.00	0.00	0.00
AVG. DAILY HEAD ON LAYER 10 (INCHES)	0.03	0.03	0.03	0.03	0.03	0.03
STD. DEV. OF DAILY HEAD ON LAYER 10 (INCHES)	0.00	0.00	0.00	0.00	0.00	0.00

ANNUAL TOTALS FOR YEAR 13

	(INCHES)	(CU. FT.)	PERCENT
PRECIPITATION	14.95	1.	100.00
RUNOFF	4.896	0.	32.75
EVAPOTRANSPIRATION	9.902	1.	66.23
PERCOLATION FROM LAYER 2	0.0000	0.	0.00
LATERAL DRAINAGE FROM LAYER 9	0.0149	0.	0.10
PERCOLATION FROM LAYER 10	0.0007	0.	0.00
CHANGE IN WATER STORAGE	0.137	0.	0.91
SOIL WATER AT START OF YEAR	182.54	15.	
SOIL WATER AT END OF YEAR	182.68	15.	
SNOW WATER AT START OF YEAR	0.00	0.	
SNOW WATER AT END OF YEAR	0.00	0.	
ANNUAL WATER BUDGET BALANCE	0.00	0.	0.00

MONTHLY TOTALS FOR YEAR 14

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
PRECIPITATION (INCHES)	0.46	0.18	0.89	0.70	1.70	3.63
	1.83	1.83	1.14	2.81	0.79	0.61

RUNOFF (INCHES)	0.013	0.000	0.000	0.014	0.168	2.150
	0.159	0.266	0.412	1.645	0.240	0.000
EVAPOTRANSPIRATION (INCHES)	0.289	0.365	0.478	0.312	2.516	1.231
	1.745	1.777	0.728	0.895	0.701	0.565
PERCOLATION FROM LAYER 2 (INCHES)	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
LATERAL DRAINAGE FROM LAYER 9 (INCHES)	0.0013	0.0011	0.0012	0.0012	0.0012	0.0012
	0.0012	0.0012	0.0012	0.0012	0.0012	0.0012
PERCOLATION FROM LAYER 10 (INCHES)	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001
	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001

MONTHLY SUMMARIES FOR DAILY HEADS

AVG. DAILY HEAD ON LAYER 2 (INCHES)	0.00	0.00	0.00	0.00	0.00	0.00
	0.00	0.00	0.00	0.00	0.00	0.00
STD. DEV. OF DAILY HEAD ON LAYER 2 (INCHES)	0.00	0.00	0.00	0.00	0.00	0.00
	0.00	0.00	0.00	0.00	0.00	0.00
AVG. DAILY HEAD ON LAYER 10 (INCHES)	0.03	0.03	0.03	0.03	0.03	0.03
	0.03	0.03	0.03	0.03	0.03	0.03
STD. DEV. OF DAILY HEAD ON LAYER 10 (INCHES)	0.00	0.00	0.00	0.00	0.00	0.00
	0.00	0.00	0.00	0.00	0.00	0.00

ANNUAL TOTALS FOR YEAR 14

	(INCHES)	(CU. FT.)	PERCENT
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PRECIPITATION	16.57	1.	100.00
RUNOFF	5.068	0.	30.58
EVAPOTRANSPIRATION	11.601	1.	70.01
PERCOLATION FROM LAYER 2	0.0000	0.	0.00
LATERAL DRAINAGE FROM LAYER 9	0.0146	0.	0.09
PERCOLATION FROM LAYER 10	0.0007	0.	0.00
CHANGE IN WATER STORAGE	-0.115	0.	-0.69
SOIL WATER AT START OF YEAR	182.68	15.	
SOIL WATER AT END OF YEAR	182.57	15.	
SNOW WATER AT START OF YEAR	0.00	0.	
SNOW WATER AT END OF YEAR	0.00	0.	

ANNUAL WATER BUDGET BALANCE 0.00 0. 0.00

MONTHLY TOTALS FOR YEAR 15

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
PRECIPITATION (INCHES)	0.65 1.30	0.08 4.08	1.91 0.39	0.52 1.22	0.68 0.99	1.85 0.79
RUNOFF (INCHES)	0.111 0.000	0.000 1.264	0.580 0.000	0.000 0.200	0.113 0.310	0.676 0.104
EVAPOTRANSPIRATION (INCHES)	0.359 1.455	0.424 2.696	1.044 0.491	0.772 0.760	0.324 0.425	1.295 0.492
PERCOLATION FROM LAYER 2 (INCHES)	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
LATERAL DRAINAGE FROM LAYER 9 (INCHES)	0.0012 0.0012	0.0011 0.0012	0.0012 0.0012	0.0012 0.0012	0.0012 0.0012	0.0012 0.0012
PERCOLATION FROM LAYER 10 (INCHES)	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001

MONTHLY SUMMARIES FOR DAILY HEADS

AVG. DAILY HEAD ON LAYER 2 (INCHES)	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00
STD. DEV. OF DAILY HEAD ON LAYER 2 (INCHES)	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00
AVG. DAILY HEAD ON LAYER 10 (INCHES)	0.03 0.03	0.03 0.03	0.03 0.03	0.03 0.03	0.03 0.03	0.03 0.03
STD. DEV. OF DAILY HEAD ON LAYER 10 (INCHES)	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00

ANNUAL TOTALS FOR YEAR 15

	(INCHES)	(CU. FT.)	PERCENT
PRECIPITATION	14.46	1.	100.00
RUNOFF	3.359	0.	23.23

LATERAL DRAINAGE FROM LAYER 9 (INCHES)	0.0012	0.0011	0.0012	0.0012	0.0012	0.0012
PERCOLATION FROM LAYER 10 (INCHES)	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001

MONTHLY SUMMARIES FOR DAILY HEADS

AVG. DAILY HEAD ON LAYER 2 (INCHES)	0.00	0.00	0.00	0.00	0.00	0.00
STD. DEV. OF DAILY HEAD ON LAYER 2 (INCHES)	0.00	0.00	0.00	0.00	0.00	0.00
AVG. DAILY HEAD ON LAYER 10 (INCHES)	0.03	0.03	0.03	0.03	0.03	0.03
STD. DEV. OF DAILY HEAD ON LAYER 10 (INCHES)	0.00	0.00	0.00	0.00	0.00	0.00

ANNUAL TOTALS FOR YEAR 17

	(INCHES)	(CU. FT.)	PERCENT
PRECIPITATION	11.05	1.	100.00
RUNOFF	2.335	0.	21.13
EVAPOTRANSPIRATION	8.750	1.	79.19
PERCOLATION FROM LAYER 2	0.0000	0.	0.00
LATERAL DRAINAGE FROM LAYER 9	0.0140	0.	0.13
PERCOLATION FROM LAYER 10	0.0007	0.	0.01
CHANGE IN WATER STORAGE	-0.050	0.	-0.45
SOIL WATER AT START OF YEAR	182.41	15.	
SOIL WATER AT END OF YEAR	182.36	15.	
SNOW WATER AT START OF YEAR	0.00	0.	
SNOW WATER AT END OF YEAR	0.00	0.	
ANNUAL WATER BUDGET BALANCE	0.00	0.	0.00

 MONTHLY TOTALS FOR YEAR 18

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
PRECIPITATION (INCHES)	0.00 2.00	0.43 2.76	1.28 4.61	0.33 0.60	1.51 0.00	1.17 0.11
RUNOFF (INCHES)	0.000 0.486	0.000 0.848	0.194 1.465	0.000 0.155	0.234 0.000	0.096 0.000
EVAPOTRANSPIRATION (INCHES)	0.000 1.514	0.248 1.796	0.388 2.683	0.370 0.686	2.076 0.338	1.114 0.110
PERCOLATION FROM LAYER 2 (INCHES)	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
LATERAL DRAINAGE FROM LAYER 9 (INCHES)	0.0012 0.0012	0.0011 0.0012	0.0012 0.0011	0.0011 0.0012	0.0012 0.0011	0.0011 0.0012
PERCOLATION FROM LAYER 10 (INCHES)	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001

 MONTHLY SUMMARIES FOR DAILY HEADS

G. DAILY HEAD ON LAYER 2 (INCHES)	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00
STD. DEV. OF DAILY HEAD ON LAYER 2 (INCHES)	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00
AVG. DAILY HEAD ON LAYER 10 (INCHES)	0.03 0.03	0.03 0.03	0.03 0.03	0.03 0.03	0.03 0.03	0.03 0.03
STD. DEV. OF DAILY HEAD ON LAYER 10 (INCHES)	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00

 ANNUAL TOTALS FOR YEAR 18

	(INCHES)	(CU. FT.)	PERCENT
PRECIPITATION	14.80	1.	100.00
RUNOFF	3.478	0.	23.50
EVAPOTRANSPIRATION	11.322	1.	76.50
PERCOLATION FROM LAYER 2	0.0000	0.	0.00
LATERAL DRAINAGE FROM LAYER 9	0.0139	0.	0.09
PERCOLATION FROM LAYER 10	0.0007	0.	0.00

CHANGE IN WATER STORAGE	-0.015	0.	-0.10
SOIL WATER AT START OF YEAR	182.36	15.	
SOIL WATER AT END OF YEAR	182.34	15.	
SNOW WATER AT START OF YEAR	0.00	0.	
SNOW WATER AT END OF YEAR	0.00	0.	
ANNUAL WATER BUDGET BALANCE	0.00	0.	0.00

MONTHLY TOTALS FOR YEAR 19

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
PRECIPITATION (INCHES)	0.08 0.23	0.72 0.28	1.00 2.41	0.54 0.89	4.04 0.00	2.16 0.49
RUNOFF (INCHES)	0.000 0.000	0.019 0.003	0.005 0.619	0.010 0.275	1.837 0.000	0.218 0.003
EVAPOTRANSPIRATION (INCHES)	0.038 0.434	0.533 0.277	0.880 1.129	0.855 0.724	1.459 0.439	2.481 0.258
PERCOLATION FROM LAYER 2 (INCHES)	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
LATERAL DRAINAGE FROM LAYER 9 (INCHES)	0.0012 0.0012	0.0011 0.0012	0.0012 0.0011	0.0011 0.0012	0.0012 0.0011	0.0011 0.0012
PERCOLATION FROM LAYER 10 (INCHES)	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001	0.0001 0.0001

MONTHLY SUMMARIES FOR DAILY HEADS

AVG. DAILY HEAD ON LAYER 2 (INCHES)	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00
STD. DEV. OF DAILY HEAD ON LAYER 2 (INCHES)	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00
AVG. DAILY HEAD ON LAYER 10 (INCHES)	0.03 0.03	0.03 0.03	0.03 0.03	0.03 0.03	0.03 0.03	0.03 0.03
STD. DEV. OF DAILY HEAD ON LAYER 10 (INCHES)	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00

MONTHLY SUMMARIES FOR DAILY HEADS

AVG. DAILY HEAD ON LAYER 2 (INCHES)	0.00	0.00	0.00	0.00	0.00	0.00
STD. DEV. OF DAILY HEAD ON LAYER 2 (INCHES)	0.00	0.00	0.00	0.00	0.00	0.00
AVG. DAILY HEAD ON LAYER 10 (INCHES)	0.03	0.03	0.03	0.03	0.03	0.03
STD. DEV. OF DAILY HEAD ON LAYER 10 (INCHES)	0.00	0.00	0.00	0.00	0.00	0.00

ANNUAL TOTALS FOR YEAR 20

	(INCHES)	(CU. FT.)	PERCENT
PRECIPITATION	21.79	2.	100.00
RUNOFF	8.038	1.	36.89
EVAPOTRANSPIRATION	13.629	1.	62.55
PERCOLATION FROM LAYER 2	0.0000	0.	0.00
LATERAL DRAINAGE FROM LAYER 9	0.0137	0.	0.06
PERCOLATION FROM LAYER 10	0.0007	0.	0.00
CHANGE IN WATER STORAGE	0.108	0.	0.50
SOIL WATER AT START OF YEAR	182.67	15.	
SOIL WATER AT END OF YEAR	182.78	15.	
SNOW WATER AT START OF YEAR	0.00	0.	
SNOW WATER AT END OF YEAR	0.00	0.	
ANNUAL WATER BUDGET BALANCE	0.00	0.	0.00

AVERAGE MONTHLY VALUES IN INCHES FOR YEARS 1 THROUGH 20

JAN/JUL FEB/AUG MAR/SEP APR/OCT MAY/NOV JUN/DEC

PRECIPITATION

TOTALS	0.48	0.52	1.01	0.89	2.06	3.32
	1.87	3.31	1.94	1.22	0.47	0.49

STD. DEVIATIONS	0.35	0.47	0.66	0.83	1.43	2.13
	0.88	1.85	1.43	0.99	0.54	0.37

RUNOFF

TOTALS	0.042	0.027	0.115	0.220	0.627	1.335
	0.360	1.311	0.638	0.345	0.109	0.031

STD. DEVIATIONS	0.084	0.062	0.160	0.401	0.676	1.376
	0.369	1.311	0.676	0.418	0.176	0.077

EVAPOTRANSPIRATION

TOTALS	0.336	0.425	0.804	0.842	1.621	1.890
	1.576	2.015	1.197	0.848	0.463	0.390

STD. DEVIATIONS	0.215	0.206	0.528	0.524	0.846	0.876
	0.630	0.803	0.719	0.648	0.344	0.323

PERCOLATION FROM LAYER 2

TOTALS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

STD. DEVIATIONS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

LATERAL DRAINAGE FROM LAYER 9

TOTALS	0.0014	0.0013	0.0014	0.0014	0.0014	0.0014
	0.0014	0.0014	0.0014	0.0014	0.0014	0.0014

STD. DEVIATIONS	0.0003	0.0003	0.0003	0.0003	0.0003	0.0003
	0.0003	0.0003	0.0003	0.0003	0.0002	0.0002

PERCOLATION FROM LAYER 10

TOTALS	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001
	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001

STD. DEVIATIONS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1 THROUGH 20

	(INCHES)	(CU. FT.)	PERCENT
PRECIPITATION	17.59 (4.355)	1.	100.00
RUNOFF	5.162 (2.422)	0.	29.34
EVAPOTRANSPIRATION	12.408 (2.688)	1.	70.54
PERCOLATION FROM LAYER 2	0.0000 (0.0000)	0.	0.00
LATERAL DRAINAGE FROM LAYER 9	0.0168 (0.0032)	0.	0.10

PERCOLATION FROM LAYER 10	0.0007 (0.0000)	0.	0.00
CHANGE IN WATER STORAGE	0.004 (0.325)	0.	0.02

PEAK DAILY VALUES FOR YEARS 1 THROUGH 20

	(INCHES)	(CU. FT.)
PRECIPITATION	3.82	0.3
RUNOFF	3.286	0.3
PERCOLATION FROM LAYER 2	0.0000	0.0
HEAD ON LAYER 2	0.0	
LATERAL DRAINAGE FROM LAYER 9	0.0001	0.0
PERCOLATION FROM LAYER 10	0.0000	0.0
HEAD ON LAYER 10	0.1	
SNOW WATER	0.68	0.1
MAXIMUM VEG. SOIL WATER (VOL/VOL)	0.2643	
MINIMUM VEG. SOIL WATER (VOL/VOL)	0.1871	

FINAL WATER STORAGE AT END OF YEAR 20

LAYER	(INCHES)	(VOL/VOL)
1	4.97	0.2071
2	3.18	0.2648
3	47.87	0.1995
4	48.32	0.2013
5	25.09	0.2091
6	25.21	0.2101
7	25.22	0.2102
8	2.24	0.1867
9	0.56	0.0463

10

0.12

0.4000

SNOW WATER

0.00

**APPENDIX D
MULTIMED MODEL RUNS**

OPTIONS CHOSEN

 Van Genuchten functional coefficients
 User defined coordinate system

1

Layer information

LAYER NO.	LAYER THICKNESS	MATERIAL PROPERTY
1	31.80	1

DATA FOR MATERIAL 1

 VADOSE ZONE MATERIAL VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Saturated hydraulic conductivity	cm/hr	CONSTANT	0.360	-999.	0.100E-10	0.100E+05
Unsaturated zone porosity	--	CONSTANT	0.430	-999.	0.100E-08	0.990
Air entry pressure head	m	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Depth of the unsaturated zone	m	CONSTANT	31.8	-999.	0.100E-08	-999.

DATA FOR MATERIAL 1

 VADOSE ZONE FUNCTION VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Residual water content	--	CONSTANT	0.700E-01	-999.	0.100E-08	1.00
Brook and Corey exponent, EN	--	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
ALFA coefficient	1/cm	CONSTANT	0.500E-02	-999.	0.000E+00	1.00
Van Genuchten exponent, ENN	--	CONSTANT	1.09	-999.	1.00	5.00

1

UNSATURATED ZONE TRANSPORT MODEL PARAMETERS

NLAY	- Number of different layers used	1
NTSTPS	- Number of time values concentration calc	40
DUMMY	- Not presently used	1
ISOL	- Type of scheme used in unsaturated zone	1
N	- Stehfest terms or number of increments	18
NTEL	- Points in Lagrangian interpolation	3
NGPTS	- Number of Gauss points	104
NIT	- Convolution integral segments	2
IBOUND	- Type of boundary condition	2
ITSGEN	- Time values generated or input	1
TMAX	- Max simulation time	-- 0.0
WTFUN	- Weighting factor	-- 1.2

OPTIONS CHOSEN

 Stehfest numerical inversion algorithm
 Nondecaying pulse source
 Computer generated times for computing concentrations

DATA FOR LAYER 1

VADOSE TRANSPORT VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Thickness of layer	m	CONSTANT	31.8	-999.	0.100E-08	-999.
Longitudinal dispersivity of layer	m	DERIVED	-999.	-999.	0.100E-02	0.100E+05
Percent organic matter	--	CONSTANT	1.00	-999.	0.000E+00	100.
Bulk density of soil for layer	g/cc	CONSTANT	1.60	-999.	0.100E-01	5.00
Biological decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.

CHEMICAL SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Solid phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Dissolved phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Overall chemical decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Acid catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Neutral hydrolysis rate constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Base catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Reference temperature	C	CONSTANT	25.0	-999.	0.000E+00	100.
Normalized distribution coefficient	ml/g	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Distribution coefficient	--	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Biodegradation coefficient (sat. zone)	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Air diffusion coefficient	cm ² /s	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
Reference temperature for air diffusion	C	CONSTANT	25.0	-999.	0.000E+00	100.
Molecular weight	g/M	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Mole fraction of solute	--	CONSTANT	0.000E+00	-999.	0.100E-08	1.00
Vapor pressure of solute	mm Hg	CONSTANT	0.000E+00	-999.	0.000E+00	100.
Henry's law constant	atm·m ³ /M	CONSTANT	0.000E+00	-999.	0.100E-09	1.00
Overall 1st order decay sat. zone	1/yr	DERIVED	0.000E+00	0.000E+00	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00

SOURCE SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Infiltration rate	m/yr	CONSTANT	0.273E-04	-999.	0.100E-09	0.100E+11
Area of waste disposal unit	m ²	CONSTANT	0.197E+07	-999.	0.100E-01	-999.
Duration of pulse	yr	CONSTANT	200.	-999.	0.100E-08	-999.
Spread of contaminant source	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Recharge rate	m/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11
Source decay constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Initial concentration at landfill	mg/l	CONSTANT	1.00	-999.	0.000E+00	-999.
Length scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Width scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Near field dilution		DERIVED	1.00	0.000E+00	0.000E+00	1.00

AQUIFER SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Particle diameter	cm	CONSTANT	0.100E-03	-999.	0.100E-08	100.
Aquifer porosity	--	CONSTANT	0.200	-999.	0.100E-08	0.990
Bulk density	g/cc	CONSTANT	1.50	-999.	0.100E-01	5.00
Aquifer thickness	m	CONSTANT	12.2	-999.	0.100E-08	0.100E+06
Source thickness (mixing zone depth)	m	DERIVED	-999.	-999.	0.100E-08	0.100E+06
Conductivity (hydraulic)	m/yr	CONSTANT	100.	-999.	0.100E-06	0.100E+09
Gradient (hydraulic)		CONSTANT	0.500E-02	-999.	0.100E-07	-999.
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Temperature of aquifer	C	CONSTANT	28.0	-999.	0.000E+00	100.
pH	--	CONSTANT	7.50	-999.	0.300	14.0
Organic carbon content (fraction)		CONSTANT	0.100E-02	-999.	0.100E-05	1.00
Well distance from site	m	CONSTANT	15.0	-999.	1.00	-999.
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00

CONCENTRATION AFTER SATURATED ZONE MODEL 0.1052E-04

U. S. ENVIRONMENTAL PROTECTION AGENCY
 EXPOSURE ASSESSMENT
 MULTIMEDIA MODEL
 MULTIMED (Version 1.01, June 1991)

Run options

AMARILLO ALTERNATE LINER DEMONSTRATION - transient leakage

duration sensitivity - WHOLE SITE, AVG LEAKAGE 20-year duration
 Chemical simulated is DEFAULT CHEMICAL

Option Chosen	Saturated and unsaturated zone models
Run was	DETERMIN
Infiltration input by user	
Run was transient	
Reject runs if Y coordinate outside plume	
Do not reject runs if Z coordinate outside plume	
Gaussian source used in saturated zone model	

UNSATURATED ZONE FLOW MODEL PARAMETERS

(input parameter description and value)	
- Total number of nodal points	240
NMAT - Number of different porous materials	1
KPROP - Van Genuchten or Brooks and Corey	1
IMSHGN - Spatial discretization option	1
NVFLAYR - Number of layers in flow model	1

OPTIONS CHOSEN

 Van Genuchten functional coefficients
 User defined coordinate system

1

Layer information

LAYER NO.	LAYER THICKNESS	MATERIAL PROPERTY
1	31.80	1

DATA FOR MATERIAL 1

 VADOSE ZONE MATERIAL VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Saturated hydraulic conductivity	cm/hr	CONSTANT	0.360	-999.	0.100E-10	0.100E+05
Unsaturated zone porosity	--	CONSTANT	0.430	-999.	0.100E-08	0.990
Air entry pressure head	m	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Depth of the unsaturated zone	m	CONSTANT	31.8	-999.	0.100E-08	-999.

DATA FOR MATERIAL 1

 VADOSE ZONE FUNCTION VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Residual water content	--	CONSTANT	0.700E-01	-999.	0.100E-08	1.00
Brook and Corey exponent, EN	--	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
ALFA coefficient	1/cm	CONSTANT	0.500E-02	-999.	0.000E+00	1.00
Van Genuchten exponent, ENN	--	CONSTANT	1.09	-999.	1.00	5.00

1

UNSATURATED ZONE TRANSPORT MODEL PARAMETERS

NLAY	- Number of different layers used	1
NTSTPS	- Number of time values concentration calc	40
DUMMY	- Not presently used	1
ISOL	- Type of scheme used in unsaturated zone	1
N	- Stehfest terms or number of increments	18
NTEL	- Points in Lagrangian interpolation	3
NGPTS	- Number of Gauss points	104
NIT	- Convolution integral segments	2
IBOUND	- Type of boundary condition	2
ITSGEN	- Time values generated or input	1
TMAX	- Max simulation time	-- 0.0
WTFUN	- Weighting factor	-- 1.2

OPTIONS CHOSEN

 Stehfest numerical inversion algorithm
 Nondecaying pulse source
 Computer generated times for computing concentrations

DATA FOR LAYER 1

VADOSE TRANSPORT VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Thickness of layer	m	CONSTANT	31.8	-999.	0.100E-08	-999.
Longitudinal dispersivity of layer	m	DERIVED	-999.	-999.	0.100E-02	0.100E+05
Percent organic matter	--	CONSTANT	1.00	-999.	0.000E+00	100.
Bulk density of soil for layer	g/cc	CONSTANT	1.60	-999.	0.100E-01	5.00
Biological decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.

CHEMICAL SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Solid phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Dissolved phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Overall chemical decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Acid catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Neutral hydrolysis rate constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Base catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Reference temperature	C	CONSTANT	25.0	-999.	0.000E+00	100.
Normalized distribution coefficient	ml/g	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Distribution coefficient	--	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Biodegradation coefficient (sat. zone)	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Air diffusion coefficient	cm ² /s	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
Reference temperature for air diffusion	C	CONSTANT	25.0	-999.	0.000E+00	100.
Molecular weight	g/M	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Mole fraction of solute	--	CONSTANT	0.000E+00	-999.	0.100E-08	1.00
Vapor pressure of solute	mm Hg	CONSTANT	0.000E+00	-999.	0.000E+00	100.
Henry's law constant	atm-m ³ /M	CONSTANT	0.000E+00	-999.	0.100E-09	1.00
Overall 1st order decay sat. zone	1/yr	DERIVED	0.000E+00	0.000E+00	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00

SOURCE SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Infiltration rate	m/yr	CONSTANT	0.273E-04	-999.	0.100E-09	0.100E+11
Area of waste disposal unit	m ²	CONSTANT	0.197E+07	-999.	0.100E-01	-999.
Duration of pulse	yr	CONSTANT	20.0	-999.	0.100E-08	-999.
Spread of contaminant source	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Recharge rate	m/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11
Source decay constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Initial concentration at landfill	mg/l	CONSTANT	1.00	-999.	0.000E+00	-999.
Length scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Width scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Near field dilution		DERIVED	1.00	0.000E+00	0.000E+00	1.00

AQUIFER SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Particle diameter	cm	CONSTANT	0.100E-03	-999.	0.100E-08	100.
Aquifer porosity	--	CONSTANT	0.200	-999.	0.100E-08	0.990
Bulk density	g/cc	CONSTANT	1.50	-999.	0.100E-01	5.00
Aquifer thickness	m	CONSTANT	12.2	-999.	0.100E-08	0.100E+06
Source thickness (mixing zone depth)	m	DERIVED	-999.	-999.	0.100E-08	0.100E+06
Conductivity (hydraulic)	m/yr	CONSTANT	100.	-999.	0.100E-06	0.100E+09
Gradient (hydraulic)		CONSTANT	0.500E-02	-999.	0.100E-07	-999.
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Temperature of aquifer	C	CONSTANT	28.0	-999.	0.000E+00	100.
pH	--	CONSTANT	7.50	-999.	0.300	14.0
Organic carbon content (fraction)		CONSTANT	0.100E-02	-999.	0.100E-05	1.00
Well distance from site	m	CONSTANT	15.0	-999.	1.00	-999.
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00

CONCENTRATION AFTER SATURATED ZONE MODEL 0.1051E-05

U. S. ENVIRONMENTAL PROTECTION AGENCY
 EXPOSURE ASSESSMENT
 MULTIMEDIA MODEL
 MULTIMED (Version 1.01, June 1991)

Run options

AMARILLO ALTERNATE LINER DEMONSTRATION - transient leakage

duration sensitivity - WHOLE SITE, AVG LEAKAGE 2000-year duration
 Chemical simulated is DEFAULT CHEMICAL

Option Chosen	Saturated and unsaturated zone models
Run was	DETERMIN
Infiltration input by user	
Run was transient	
Reject runs if Y coordinate outside plume	
Do not reject runs if Z coordinate outside plume	
Gaussian source used in saturated zone model	

UNSATURATED ZONE FLOW MODEL PARAMETERS

(input parameter description and value)	
- Total number of nodal points	240
NMAT - Number of different porous materials	1
KPROP - Van Genuchten or Brooks and Corey	1
IMSHGN - Spatial discretization option	1
NVFLAYR - Number of layers in flow model	1

OPTIONS CHOSEN

Van Genuchten functional coefficients
 User defined coordinate system

1

Layer information

LAYER NO.	LAYER THICKNESS	MATERIAL PROPERTY
1	31.80	1

DATA FOR MATERIAL 1

VADOSE ZONE MATERIAL VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Saturated hydraulic conductivity	cm/hr	CONSTANT	0.360	-999.	0.100E-10	0.100E+05
Unsaturated zone porosity	--	CONSTANT	0.430	-999.	0.100E-08	0.990
Air entry pressure head	m	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Depth of the unsaturated zone	m	CONSTANT	31.8	-999.	0.100E-08	-999.

DATA FOR MATERIAL 1

VADOSE ZONE FUNCTION VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Residual water content	--	CONSTANT	0.700E-01	-999.	0.100E-08	1.00
Brook and Corey exponent, EN	--	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
ALFA coefficient	1/cm	CONSTANT	0.500E-02	-999.	0.000E+00	1.00
Van Genuchten exponent, ENN	--	CONSTANT	1.09	-999.	1.00	5.00

1

UNSATURATED ZONE TRANSPORT MODEL PARAMETERS

NLAY	- Number of different layers used	1
NTSTPS	- Number of time values concentration calc	40
DUMMY	- Not presently used	1
ISOL	- Type of scheme used in unsaturated zone	1
N	- Stehfest terms or number of increments	18
NTEL	- Points in Lagrangian interpolation	3
NGPTS	- Number of Gauss points	104
NIT	- Convolution integral segments	2
IBOUND	- Type of boundary condition	2
ITSGEN	- Time values generated or input	1
TMAX	- Max simulation time	-- 0.0
WTFUM	- Weighting factor	-- 1.2

OPTIONS CHOSEN

Stehfest numerical inversion algorithm
 Nondecaying pulse source
 Computer generated times for computing concentrations

DATA FOR LAYER 1

VADOSE TRANSPORT VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Thickness of layer	m	CONSTANT	31.8	-999.	0.100E-08	-999.
Longitudinal dispersivity of layer	m	DERIVED	-999.	-999.	0.100E-02	0.100E+05
Percent organic matter	--	CONSTANT	1.00	-999.	0.000E+00	100.
Bulk density of soil for layer	g/cc	CONSTANT	1.60	-999.	0.100E-01	5.00
Biological decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.

CHEMICAL SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Solid phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Dissolved phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Overall chemical decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Acid catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Neutral hydrolysis rate constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Base catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Reference temperature	C	CONSTANT	25.0	-999.	0.000E+00	100.
Normalized distribution coefficient	ml/g	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Distribution coefficient	--	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Biodegradation coefficient (sat. zone)	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Air diffusion coefficient	cm ² /s	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
Reference temperature for air diffusion	C	CONSTANT	25.0	-999.	0.000E+00	100.
Molecular weight	g/M	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Mole fraction of solute	--	CONSTANT	0.000E+00	-999.	0.100E-08	1.00
Vapor pressure of solute	mm Hg	CONSTANT	0.000E+00	-999.	0.000E+00	100.
Henry's law constant	atm-m ³ /M	CONSTANT	0.000E+00	-999.	0.100E-09	1.00
Overall 1st order decay sat. zone	1/yr	DERIVED	0.000E+00	0.000E+00	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00

SOURCE SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Infiltration rate	m/yr	CONSTANT	0.273E-04	-999.	0.100E-09	0.100E+11
Area of waste disposal unit	m ²	CONSTANT	0.197E+07	-999.	0.100E-01	-999.
Duration of pulse	yr	CONSTANT	0.200E+04	-999.	0.100E-08	-999.
Spread of contaminant source	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Recharge rate	m/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11
Source decay constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Initial concentration at landfill	mg/l	CONSTANT	1.00	-999.	0.000E+00	-999.
Length scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Width scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Near field dilution		DERIVED	1.00	0.000E+00	0.000E+00	1.00

AQUIFER SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Particle diameter	cm	CONSTANT	0.100E-03	-999.	0.100E-08	100.
Aquifer porosity	--	CONSTANT	0.200	-999.	0.100E-08	0.990
Bulk density	g/cc	CONSTANT	1.50	-999.	0.100E-01	5.00
Aquifer thickness	m	CONSTANT	12.2	-999.	0.100E-08	0.100E+06
Source thickness (mixing zone depth)	m	DERIVED	-999.	-999.	0.100E-08	0.100E+06
Conductivity (hydraulic)	m/yr	CONSTANT	100.	-999.	0.100E-06	0.100E+09
Gradient (hydraulic)		CONSTANT	0.500E-02	-999.	0.100E-07	-999.
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Temperature of aquifer	C	CONSTANT	28.0	-999.	0.000E+00	100.
pH	--	CONSTANT	7.50	-999.	0.300	14.0
Organic carbon content (fraction)		CONSTANT	0.100E-02	-999.	0.100E-05	1.00
Well distance from site	m	CONSTANT	15.0	-999.	1.00	-999.
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00

CONCENTRATION AFTER SATURATED ZONE MODEL 0.1063E-03

OPTIONS CHOSEN

 Van Genuchten functional coefficients
 User defined coordinate system

1

Layer information

LAYER NO.	LAYER THICKNESS	MATERIAL PROPERTY
1	44.20	1

DATA FOR MATERIAL 1

 VADOSE ZONE MATERIAL VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Saturated hydraulic conductivity	cm/hr	CONSTANT	0.360	-999.	0.100E-10	0.100E+05
Unsaturated zone porosity	--	CONSTANT	0.430	-999.	0.100E-08	0.990
Air entry pressure head	m	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Depth of the unsaturated zone	m	CONSTANT	44.2	-999.	0.100E-08	-999.

DATA FOR MATERIAL 1

 VADOSE ZONE FUNCTION VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Residual water content	--	CONSTANT	0.700E-01	-999.	0.100E-08	1.00
Brook and Corey exponent, EN	--	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
ALFA coefficient	1/cm	CONSTANT	0.500E-02	-999.	0.000E+00	1.00
Van Genuchten exponent, ENN	--	CONSTANT	1.09	-999.	1.00	5.00

1

UNSATURATED ZONE TRANSPORT MODEL PARAMETERS

NLAY	- Number of different layers used	1
NTSTPS	- Number of time values concentration calc	40
DUMMY	- Not presently used	1
ISQL	- Type of scheme used in unsaturated zone	1
N	- Stehfest terms or number of increments	18
NTEL	- Points in Lagrangian interpolation	3
NGPTS	- Number of Gauss points	104
NIT	- Convolution integral segments	2
IBOUND	- Type of boundary condition	2
ITSGEN	- Time values generated or input	1
TMAX	- Max simulation time	-- 0.0
WTFUN	- Weighting factor	-- 1.2

OPTIONS CHOSEN

 Stehfest numerical inversion algorithm
 Nondecaying pulse source
 Computer generated times for computing concentrations

DATA FOR LAYER 1

VADOSE TRANSPORT VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Thickness of layer	m	CONSTANT	44.2	-999.	0.100E-08	-999.
Longitudinal dispersivity of layer	m	DERIVED	-999.	-999.	0.100E-02	0.100E+05
Percent organic matter	--	CONSTANT	1.00	-999.	0.000E+00	100.
Bulk density of soil for layer	g/cc	CONSTANT	1.60	-999.	0.100E-01	5.00
Biological decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.

CHEMICAL SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Solid phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Dissolved phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Overall chemical decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Acid catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Neutral hydrolysis rate constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Base catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Reference temperature	C	CONSTANT	25.0	-999.	0.000E+00	100.
Normalized distribution coefficient	ml/g	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Distribution coefficient	--	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Biodegradation coefficient (sat. zone)	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Air diffusion coefficient	cm ² /s	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
Reference temperature for air diffusion	C	CONSTANT	25.0	-999.	0.000E+00	100.
Molecular weight	g/M	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Mole fraction of solute	--	CONSTANT	0.000E+00	-999.	0.100E-08	1.00
Vapor pressure of solute	mm Hg	CONSTANT	0.000E+00	-999.	0.000E+00	100.
Henry's law constant	atm-m ³ /M	CONSTANT	0.000E+00	-999.	0.100E-09	1.00
Overall 1st order decay sat. zone	1/yr	DERIVED	0.000E+00	0.000E+00	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00

SOURCE SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Infiltration rate	m/yr	CONSTANT	0.273E-04	-999.	0.100E-09	0.100E+11
Area of waste disposal unit	m ²	CONSTANT	0.197E+07	-999.	0.100E-01	-999.
Duration of pulse	yr	CONSTANT	200.	-999.	0.100E-08	-999.
Spread of contaminant source	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Recharge rate	m/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11
Source decay constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Initial concentration at landfill	mg/l	CONSTANT	-1.00	-999.	0.000E+00	-999.
Length scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Width scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Near field dilution		DERIVED	1.00	0.000E+00	0.000E+00	1.00

AQUIFER SPECIFIC VARIABLES

DATA FOR LAYER 1

VADOSE TRANSPORT VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Thickness of layer	m	CONSTANT	31.8	-999.	0.100E-08	-999.
Longitudinal dispersivity of layer	m	DERIVED	-999.	-999.	0.100E-02	0.100E+05
Percent organic matter	--	CONSTANT	1.00	-999.	0.000E+00	100.
Bulk density of soil for layer	g/cc	CONSTANT	1.60	-999.	0.100E-01	5.00
Biological decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.

CHEMICAL SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Solid phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Dissolved phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Overall chemical decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Acid catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Neutral hydrolysis rate constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Base catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Reference temperature	C	CONSTANT	25.0	-999.	0.000E+00	100.
Normalized distribution coefficient	ml/g	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Distribution coefficient	--	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Biodegradation coefficient (sat. zone)	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Air diffusion coefficient	cm ² /s	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
Reference temperature for air diffusion	C	CONSTANT	25.0	-999.	0.000E+00	100.
Molecular weight	g/M	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Mole fraction of solute	--	CONSTANT	0.000E+00	-999.	0.100E-08	1.00
Vapor pressure of solute	mm Hg	CONSTANT	0.000E+00	-999.	0.000E+00	100.
Henry's law constant	atm-m ³ /M	CONSTANT	0.000E+00	-999.	0.100E-09	1.00
Overall 1st order decay sat. zone	1/yr	DERIVED	0.000E+00	0.000E+00	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00

SOURCE SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Infiltration rate	m/yr	CONSTANT	0.273E-04	-999.	0.100E-09	0.100E+11
Area of waste disposal unit	m ²	CONSTANT	0.197E+07	-999.	0.100E-01	-999.
Duration of pulse	yr	CONSTANT	200.	-999.	0.100E-08	-999.
Spread of contaminant source	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Recharge rate	m/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11
Source decay constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Initial concentration at landfill	mg/l	CONSTANT	1.00	-999.	0.000E+00	-999.
Length scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Width scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Near field dilution		DERIVED	1.00	0.000E+00	0.000E+00	1.00

AQUIFER SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Particle diameter	cm	CONSTANT	0.100E-03	-999.	0.100E-08	100.
Aquifer porosity	--	CONSTANT	0.200	-999.	0.100E-08	0.990
Bulk density	g/cc	CONSTANT	1.50	-999.	0.100E-01	5.00
Aquifer thickness	m	CONSTANT	12.2	-999.	0.100E-08	0.100E+06
Source thickness (mixing zone depth)	m	DERIVED	-999.	-999.	0.100E-08	0.100E+06
Conductivity (hydraulic)	m/yr	CONSTANT	100.	-999.	0.100E-06	0.100E+09
Gradient (hydraulic)		CONSTANT	0.500E-02	-999.	0.100E-07	-999.
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Temperature of aquifer	C	CONSTANT	28.0	-999.	0.000E+00	100.
pH	--	CONSTANT	7.50	-999.	0.300	14.0
Organic carbon content (fraction)		CONSTANT	0.100E-02	-999.	0.100E-05	1.00
Well distance from site	m	CONSTANT	15.0	-999.	1.00	-999.
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00

CONCENTRATION AFTER SATURATED ZONE MODEL 0.1158E-04

U. S. ENVIRONMENTAL PROTECTION AGENCY
 EXPOSURE ASSESSMENT
 MULTIMEDIA MODEL
 MULTINED (Version 1.01, June 1991)

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 Run options

AMARILLO ALTERNATE LINER DEMONSTRATION - transient leakage

infiltration sensitivity - WHOLE SITE, AVG LEAKAGE 200-year duration
 Chemical simulated is DEFAULT CHEMICAL

Option Chosen	Saturated and unsaturated zone models
Run was	DETERMIN
Infiltration input by user	
Run was transient	
Reject runs if Y coordinate outside plume	
Do not reject runs if Z coordinate outside plume	
Gaussian source used in saturated zone model	

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UNSATURATED ZONE FLOW MODEL PARAMETERS
 (input parameter description and value)

NP	- Total number of nodal points	240
NMAT	- Number of different porous materials	1
KPROP	- Van Genuchten or Brooks and Corey	1
IMSHGM	- Spatial discretization option	1
NVFLAYR	- Number of layers in flow model	1

OPTIONS CHOSEN

 Van Genuchten functional coefficients
 user defined coordinate system

Layer information

LAYER NO.	LAYER THICKNESS	MATERIAL PROPERTY
1	31.80	1

DATA FOR MATERIAL 1

 VADOSE ZONE MATERIAL VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Saturated hydraulic conductivity	cm/hr	CONSTANT	0.360	-999.	0.100E-10	0.100E+05
Unsaturated zone porosity	--	CONSTANT	0.430	-999.	0.100E-08	0.990
Air entry pressure head	m	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Depth of the unsaturated zone	m	CONSTANT	31.8	-999.	0.100E-08	-999.

DATA FOR MATERIAL 1

 VADOSE ZONE FUNCTION VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Residual water content	--	CONSTANT	0.700E-01	-999.	0.100E-08	1.00
Brook and Corey exponent, EN	--	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
ALFA coefficient	1/cm	CONSTANT	0.270E-01	-999.	0.000E+00	1.00
Van Genuchten exponent, ENN	--	CONSTANT	1.09	-999.	1.00	5.00

UNSATURATED ZONE TRANSPORT MODEL PARAMETERS

NLAY	- Number of different layers used	1
NTSTPS	- Number of time values concentration calc	40
DUMMY	- Not presently used	1
ISOL	- Type of scheme used in unsaturated zone	1
N	- Stehfest terms or number of increments	18
NTEL	- Points in Lagrangian interpolation	3
NGPTS	- Number of Gauss points	104
NIT	- Convolution integral segments	2
IBOUND	- Type of boundary condition	2
ITSGEN	- Time values generated or input	1
TMAX	- Max simulation time	-- 0.0
WTFUN	- Weighting factor	-- 1.2

OPTIONS CHOSEN

 Stehfest numerical inversion algorithm
 Nondecaying pulse source
 Computer generated times for computing concentrations

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Particle diameter	cm	CONSTANT	0.100E-03	-999.	0.100E-08	100.
Aquifer porosity	--	CONSTANT	0.200	-999.	0.100E-08	0.990
Bulk density	g/cc	CONSTANT	1.50	-999.	0.100E-01	5.00
Aquifer thickness	m	CONSTANT	12.2	-999.	0.100E-08	0.100E+06
Source thickness (mixing zone depth)	m	DERIVED	-999.	-999.	0.100E-08	0.100E+06
Conductivity (hydraulic)	m/yr	CONSTANT	100.	-999.	0.100E-06	0.100E+09
Gradient (hydraulic)		CONSTANT	0.500E-02	-999.	0.100E-07	-999.
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Temperature of aquifer	C	CONSTANT	28.0	-999.	0.000E+00	100.
pH	--	CONSTANT	7.50	-999.	0.300	14.0
Organic carbon content (fraction)		CONSTANT	0.100E-02	-999.	0.100E-05	1.00
Well distance from site	m	CONSTANT	15.0	-999.	1.00	-999.
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00

CONCENTRATION AFTER SATURATED ZONE MODEL 0.1052E-06

U. S. ENVIRONMENTAL PROTECTION AGENCY
 EXPOSURE ASSESSMENT
 MULTIMEDIA MODEL
 MULTIMED (Version 1.01, June 1991)

1

Run options

AMARILLO ALTERNATE LINER DEMONSTRATION - transient leakage

vadose depth sensitivity - WHOLE SITE, AVG LEAKAGE 200-year duration
Chemical simulated is DEFAULT CHEMICAL

Option Chosen	Saturated and unsaturated zone models
Run was	DETERMIN
Infiltration input by user	
Run was transient	
Reject runs if Y coordinate outside plume	
Do not reject runs if Z coordinate outside plume	
Gaussian source used in saturated zone model	

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UNSATURATED ZONE FLOW MODEL PARAMETERS		
(input parameter description and value)		
	- Total number of nodal points	240
NMAT	- Number of different porous materials	1
KPROP	- Van Genuchten or Brooks and Corey	1
IMSHGN	- Spatial discretization option	1
NVFLAYR	- Number of layers in flow model	1

OPTIONS CHOSEN

Van Genuchten functional coefficients
 User defined coordinate system

1

Layer information

LAYER NO.	LAYER THICKNESS	MATERIAL PROPERTY
1	21.00	1

DATA FOR MATERIAL 1

VADOSE ZONE MATERIAL VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Saturated hydraulic conductivity	cm/hr	CONSTANT	0.360	-999.	0.100E-10	0.100E+05
Unsaturated zone porosity	--	CONSTANT	0.430	-999.	0.100E-08	0.990
Air entry pressure head	m	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Depth of the unsaturated zone	m	CONSTANT	21.0	-999.	0.100E-08	-999.

DATA FOR MATERIAL 1

VADOSE ZONE FUNCTION VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Residual water content	--	CONSTANT	0.700E-01	-999.	0.100E-08	1.00
Brook and Corey exponent, EN	--	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
ALFA coefficient	1/cm	CONSTANT	0.500E-02	-999.	0.000E+00	1.00
Van Genuchten exponent, ENN	--	CONSTANT	1.09	-999.	1.00	5.00

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UNSATURATED ZONE TRANSPORT MODEL PARAMETERS

NLAY	- Number of different layers used	1
NTSTPS	- Number of time values concentration calc	40
DUMMY	- Not presently used	1
ISOL	- Type of scheme used in unsaturated zone	1
N	- Stehfest terms or number of increments	18
NTEL	- Points in Lagrangian interpolation	3
NGPTS	- Number of Gauss points	104
NIT	- Convolution integral segments	2
IBOUND	- Type of boundary condition	2
ITSGEN	- Time values generated or input	1
TMAX	- Max simulation time	-- 0.0
WTFUN	- Weighting factor	-- 1.2

OPTIONS CHOSEN

Stehfest numerical inversion algorithm
 Nondecaying pulse source
 Computer generated times for computing concentrations

DATA FOR LAYER 1

VADOSE TRANSPORT VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Thickness of layer	m	CONSTANT	21.0	-999.	0.100E-08	-999.
Longitudinal dispersivity of layer	m	DERIVED	-999.	-999.	0.100E-02	0.100E+05
Percent organic matter	--	CONSTANT	1.00	-999.	0.000E+00	100.
Bulk density of soil for layer	g/cc	CONSTANT	1.60	-999.	0.100E-01	5.00
Biological decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.

CHEMICAL SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Solid phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Dissolved phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Overall chemical decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Acid catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Neutral hydrolysis rate constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Base catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Reference temperature	C	CONSTANT	25.0	-999.	0.000E+00	100.
Normalized distribution coefficient	ml/g	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Distribution coefficient	--	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Biodegradation coefficient (sat. zone)	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Air diffusion coefficient	cm ² /s	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
Reference temperature for air diffusion	C	CONSTANT	25.0	-999.	0.000E+00	100.
Molecular weight	g/M	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Mole fraction of solute	--	CONSTANT	0.000E+00	-999.	0.100E-08	1.00
Vapor pressure of solute	mm Hg	CONSTANT	0.000E+00	-999.	0.000E+00	100.
Henry's law constant	atm-m ³ /M	CONSTANT	0.000E+00	-999.	0.100E-09	1.00
Overall 1st order decay sat. zone	1/yr	DERIVED	0.000E+00	0.000E+00	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00

SOURCE SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Infiltration rate	m/yr	CONSTANT	0.273E-04	-999.	0.100E-09	0.100E+11
Area of waste disposal unit	m ²	CONSTANT	0.197E+07	-999.	0.100E-01	-999.
Duration of pulse	yr	CONSTANT	200.	-999.	0.100E-08	-999.
Spread of contaminant source	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Recharge rate	m/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11
Source decay constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Initial concentration at landfill	mg/l	CONSTANT	4.00	-999.	0.000E+00	-999.
Length scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Width scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Near field dilution		DERIVED	1.00	0.000E+00	0.000E+00	1.00

AQUIFER SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Particle diameter	cm	CONSTANT	0.100E-03	-999.	0.100E-08	100.
Aquifer porosity	--	CONSTANT	0.200	-999.	0.100E-08	0.990
Bulk density	g/cc	CONSTANT	1.50	-999.	0.100E-01	5.00
Aquifer thickness	m	CONSTANT	12.2	-999.	0.100E-08	0.100E+06
Source thickness (mixing zone depth)	m	DERIVED	-999.	-999.	0.100E-08	0.100E+06
Conductivity (hydraulic)	m/yr	CONSTANT	100.	-999.	0.100E-06	0.100E+09
Gradient (hydraulic)		CONSTANT	0.500E-02	-999.	0.100E-07	-999.
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Temperature of aquifer	C	CONSTANT	28.0	-999.	0.000E+00	100.
pH	--	CONSTANT	7.50	-999.	0.300	14.0
Organic carbon content (fraction)		CONSTANT	0.100E-02	-999.	0.100E-05	1.00
Well distance from site	m	CONSTANT	15.0	-999.	1.00	-999.
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00

CONCENTRATION AFTER SATURATED ZONE MODEL 0.1555E-04

U. S. ENVIRONMENTAL PROTECTION AGENCY
 EXPOSURE ASSESSMENT
 MULTIMEDIA MODEL
 MULTIMED (Version 1.01, June 1991)

Run options

AMARILLO ALTERNATE LINER DEMONSTRATION - transient leakage

vadose depth sensitivity - WHOLE SITE, AVG LEAKAGE 200-year duration
 Chemical simulated is DEFAULT CHEMICAL

Option Chosen Saturated and unsaturated zone models
 Run was DETERMIN
 Infiltration input by user
 Run was transient
 Reject runs if Y coordinate outside plume
 Do not reject runs if Z coordinate outside plume
 Gaussian source used in saturated zone model

UNSATURATED ZONE FLOW MODEL PARAMETERS
 (input parameter description and value)

	- Total number of nodal points	240
	- Number of different porous materials	1
KPROP	- Van Genuchten or Brooks and Corey	1
IMSHGM	- Spatial discretization option	1
MVFLAYR	- Number of layers in flow model	1

OPTIONS CHOSEN

Van Genuchten functional coefficients
 User defined coordinate system

1

Layer information

LAYER NO.	LAYER THICKNESS	MATERIAL PROPERTY
1	31.80	1

DATA FOR MATERIAL 1

VADOSE ZONE MATERIAL VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Saturated hydraulic conductivity	cm/hr	CONSTANT	0.360	-999.	0.100E-10	0.100E+05
Unsaturated zone porosity	--	CONSTANT	0.430	-999.	0.100E-08	0.990
Air entry pressure head	m	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Depth of the unsaturated zone	m	CONSTANT	31.8	-999.	0.100E-08	-999.

DATA FOR MATERIAL 1

VADOSE ZONE FUNCTION VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Residual water content	--	CONSTANT	0.700E-01	-999.	0.100E-08	1.00
Brook and Corey exponent, EN	--	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
ALFA coefficient	1/cm	CONSTANT	0.500E-02	-999.	0.000E+00	1.00
Van Genuchten exponent, ENN	--	CONSTANT	1.09	-999.	1.00	5.00

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UNSATURATED ZONE TRANSPORT MODEL PARAMETERS

NLAY	- Number of different layers used	1
NTSTPS	- Number of time values concentration calc	40
DUMMY	- Not presently used	1
ISOL	- Type of scheme used in unsaturated zone	1
N	- Stehfest terms or number of increments	18
NTEL	- Points in Lagrangian interpolation	3
NGPTS	- Number of Gauss points	104
NIT	- Convolution integral segments	2
IBOUND	- Type of boundary condition	2
ITSGEN	- Time values generated or input	1
TMAX	- Max simulation time	-- 0.0
WTFUM	- Weighting factor	-- 1.2

OPTIONS CHOSEN

Stehfest numerical inversion algorithm
 Nondecaying pulse source
 Computer generated times for computing concentrations

DATA FOR LAYER 1

VADOSE TRANSPORT VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Thickness of layer	m	CONSTANT	31.8	-999.	0.100E-08	-999.
Longitudinal dispersivity of layer	m	DERIVED	-999.	-999.	0.100E-02	0.100E+05
Percent organic matter	--	CONSTANT	1.00	-999.	0.000E+00	100.
Bulk density of soil for layer	g/cc	CONSTANT	1.60	-999.	0.100E-01	5.00
Biological decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.

CHEMICAL SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Solid phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Dissolved phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Overall chemical decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Acid catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Neutral hydrolysis rate constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Base catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Reference temperature	C	CONSTANT	25.0	-999.	0.000E+00	100.
Normalized distribution coefficient	ml/g	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Distribution coefficient	--	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Biodegradation coefficient (sat. zone)	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Air diffusion coefficient	cm ² /s	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
Reference temperature for air diffusion	C	CONSTANT	25.0	-999.	0.000E+00	100.
Molecular weight	g/M	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Mole fraction of solute	--	CONSTANT	0.000E+00	-999.	0.100E-08	1.00
Vapor pressure of solute	mm Hg	CONSTANT	0.000E+00	-999.	0.000E+00	100.
Henry's law constant	atm-m ³ /M	CONSTANT	0.000E+00	-999.	0.100E-09	1.00
Overall 1st order decay sat. zone	1/yr	DERIVED	0.000E+00	0.000E+00	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00

SOURCE SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Infiltration rate	m/yr	CONSTANT	0.273E-05	-999.	0.100E-09	0.100E+11
Area of waste disposal unit	m ²	CONSTANT	0.197E+07	-999.	0.100E-01	-999.
Duration of pulse	yr	CONSTANT	200.	-999.	0.100E-08	-999.
Spread of contaminant source	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Recharge rate	m/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11
Source decay constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Initial concentration at landfill	mg/l	CONSTANT	1.00	-999.	0.000E+00	-999.
Length scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Width scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Near field dilution		DERIVED	1.00	0.000E+00	0.000E+00	1.00

AQUIFER SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Particle diameter	cm	CONSTANT	0.100E-03	-999.	0.100E-08	100.
Aquifer porosity	--	CONSTANT	0.200	-999.	0.100E-08	0.990
Bulk density	g/cc	CONSTANT	1.50	-999.	0.100E-01	5.00
Aquifer thickness	m	CONSTANT	12.2	-999.	0.100E-08	0.100E+06
Source thickness (mixing zone depth)	m	DERIVED	-999.	-999.	0.100E-08	0.100E+06
Conductivity (hydraulic)	m/yr	CONSTANT	100.	-999.	0.100E-06	0.100E+09
Gradient (hydraulic)		CONSTANT	0.500E-02	-999.	0.100E-07	-999.
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Temperature of aquifer	C	CONSTANT	28.0	-999.	0.000E+00	100.
pH	--	CONSTANT	7.50	-999.	0.300	14.0
Organic carbon content (fraction)		CONSTANT	0.100E-02	-999.	0.100E-05	1.00
Well distance from site	m	CONSTANT	15.0	-999.	1.00	-999.
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00

CONCENTRATION AFTER SATURATED ZONE MODEL 0.7725E-05

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U. S. ENVIRONMENTAL PROTECTION AGENCY
 EXPOSURE ASSESSMENT
 MULTIMEDIA MODEL
 MULTIMED (Version 1.01, June 1991)

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Run options

AMARILLO ALTERNATE LINER DEMONSTRATION - transient leakage

alpha VG sensitivity - WHOLE SITE, AVG LEAKAGE 200-year duration
 Chemical simulated is DEFAULT CHEMICAL

Option Chosen	Saturated and unsaturated zone models
Run was	DETERMIN
Infiltration input by user	
Run was transient	
Reject runs if Y coordinate outside plume	
Do not reject runs if Z coordinate outside plume	
Gaussian source used in saturated zone model	

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UNSATURATED ZONE FLOW MODEL PARAMETERS

Input parameter description and value)	
- Total number of nodal points	240
NMAT - Number of different porous materials	1
KPROP - Van Genuchten or Brooks and Corey	1
IMSHGN - Spatial discretization option	1
NVFLAYR - Number of layers in flow model	1

OPTIONS CHOSEN

 Van Genuchten functional coefficients
 User defined coordinate system

1

Layer information

LAYER NO.	LAYER THICKNESS	MATERIAL PROPERTY
1	31.80	1

DATA FOR MATERIAL 1

 VADOSE ZONE MATERIAL VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Saturated hydraulic conductivity	cm/hr	CONSTANT	0.360	-999.	0.100E-10	0.100E+05
Unsaturated zone porosity	--	CONSTANT	0.430	-999.	0.100E-08	0.990
Air entry pressure head	m	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Depth of the unsaturated zone	m	CONSTANT	31.8	-999.	0.100E-08	-999.

DATA FOR MATERIAL 1

 VADOSE ZONE FUNCTION VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Residual water content	--	CONSTANT	0.700E-01	-999.	0.100E-08	1.00
Brook and Corey exponent, EN	--	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
ALFA coefficient	1/cm	CONSTANT	0.500E-02	-999.	0.000E+00	1.00
Van Genuchten exponent, ENN	--	CONSTANT	1.09	-999.	1.00	5.00

UNSATURATED ZONE TRANSPORT MODEL PARAMETERS

NLAY	- Number of different layers used	1
NTSTPS	- Number of time values concentration calc	40
DUMMY	- Not presently used	1
ISOL	- Type of scheme used in unsaturated zone	1
N	- Stehfest terms or number of increments	18
NTEL	- Points in Lagrangian interpolation	3
NGPTS	- Number of Gauss points	104
NIT	- Convolution integral segments	2
IBOUND	- Type of boundary condition	2
ITSGEN	- Time values generated or input	1
TMAX	- Max simulation time	-- 0.0
WTFUN	- Weighting factor	-- 1.2

OPTIONS CHOSEN

 Stehfest numerical inversion algorithm
 Nondecaying pulse source
 Computer generated times for computing concentrations

DATA FOR LAYER 1

VADOSE TRANSPORT VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Thickness of layer	m	CONSTANT	31.8	-999.	0.100E-08	-999.
Longitudinal dispersivity of layer	m	DERIVED	-999.	-999.	0.100E-02	0.100E+05
Percent organic matter	--	CONSTANT	1.00	-999.	0.000E+00	100.
Bulk density of soil for layer	g/cc	CONSTANT	1.60	-999.	0.100E-01	5.00
Biological decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.

CHEMICAL SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Solid phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Dissolved phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Overall chemical decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Acid catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Neutral hydrolysis rate constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Base catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Reference temperature	C	CONSTANT	25.0	-999.	0.000E+00	100.
Normalized distribution coefficient	ml/g	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Distribution coefficient	--	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Biodegradation coefficient (sat. zone)	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Air diffusion coefficient	cm ² /s	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
Reference temperature for air diffusion	C	CONSTANT	25.0	-999.	0.000E+00	100.
Molecular weight	g/M	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Mole fraction of solute	--	CONSTANT	0.000E+00	-999.	0.100E-08	1.00
Vapor pressure of solute	mm Hg	CONSTANT	0.000E+00	-999.	0.000E+00	100.
Henry's law constant	atm·m ³ /M	CONSTANT	0.000E+00	-999.	0.100E-09	1.00
Overall 1st order decay sat. zone	1/yr	DERIVED	0.000E+00	0.000E+00	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00

SOURCE SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Infiltration rate	m/yr	CONSTANT	0.273E-03	-999.	0.100E-09	0.100E+11
Area of waste disposal unit	m ²	CONSTANT	0.197E+07	-999.	0.100E-01	-999.
Duration of pulse	yr	CONSTANT	200.	-999.	0.100E-08	-999.
Spread of contaminant source	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Recharge rate	m/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11
Source decay constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Initial concentration at landfill	mg/l	CONSTANT	1.00	-999.	0.000E+00	-999.
Length scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Width scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Near field dilution		DERIVED	1.00	0.000E+00	0.000E+00	1.00

AQUIFER SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Particle diameter	cm	CONSTANT	0.100E-03	-999.	0.100E-08	100.
Aquifer porosity	--	CONSTANT	0.200	-999.	0.100E-08	0.990
Bulk density	g/cc	CONSTANT	1.50	-999.	0.100E-01	5.00
Aquifer thickness	m	CONSTANT	12.2	-999.	0.100E-08	0.100E+06
Source thickness (mixing zone depth)	m	DERIVED	-999.	-999.	0.100E-08	0.100E+06
Conductivity (hydraulic)	m/yr	CONSTANT	100.	-999.	0.100E-06	0.100E+09
Gradient (hydraulic)		CONSTANT	0.500E-02	-999.	0.100E-07	-999.
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Temperature of aquifer	C	CONSTANT	28.0	-999.	0.000E+00	100.
pH	--	CONSTANT	7.50	-999.	0.300	14.0
Organic carbon content (fraction)		CONSTANT	0.100E-02	-999.	0.100E-05	1.00
Well distance from site	m	CONSTANT	15.0	-999.	1.00	-999.
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00

CONCENTRATION AFTER SATURATED ZONE MODEL 0.1059E-02

OPTIONS CHOSEN

 Van Genuchten functional coefficients
 User defined coordinate system

1

Layer information

LAYER NO.	LAYER THICKNESS	MATERIAL PROPERTY
1	31.80	1

DATA FOR MATERIAL 1

 VADOSE ZONE MATERIAL VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Saturated hydraulic conductivity	cm/hr	CONSTANT	0.360	-999.	0.100E-10	0.100E+05
Unsaturated zone porosity	--	CONSTANT	0.430	-999.	0.100E-08	0.990
Air entry pressure head	m	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Depth of the unsaturated zone	m	CONSTANT	31.8	-999.	0.100E-08	-999.

DATA FOR MATERIAL 1

 VADOSE ZONE FUNCTION VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Residual water content	--	CONSTANT	0.700E-01	-999.	0.100E-08	1.00
Brook and Corey exponent, EN	--	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
ALFA coefficient	1/cm	CONSTANT	0.145	-999.	0.000E+00	1.00
Van Genuchten exponent, ENN	--	CONSTANT	1.09	-999.	1.00	5.00

UNSATURATED ZONE TRANSPORT MODEL PARAMETERS

NLAY	- Number of different layers used	1
NTSTPS	- Number of time values concentration calc	40
DUMMY	- Not presently used	1
ISOL	- Type of scheme used in unsaturated zone	1
N	- Stehfest terms or number of increments	18
NTEL	- Points in Lagrangian interpolation	3
NGPTS	- Number of Gauss points	104
NIT	- Convolution integral segments	2
IBOUND	- Type of boundary condition	2
ITSGEN	- Time values generated or input	1
TMAX	- Max simulation time	-- 0.0
WTFUN	- Weighting factor	-- 1.2

OPTIONS CHOSEN

 Stehfest numerical inversion algorithm
 Nondecaying pulse source
 Computer generated times for computing concentrations

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Particle diameter	cm	CONSTANT	0.100E-03	-999.	0.100E-08	100.
Aquifer porosity	--	CONSTANT	0.200	-999.	0.100E-08	0.990
Bulk density	g/cc	CONSTANT	1.50	-999.	0.100E-01	5.00
Aquifer thickness	m	CONSTANT	12.2	-999.	0.100E-08	0.100E+06
Source thickness (mixing zone depth)	m	DERIVED	-999.	-999.	0.100E-08	0.100E+06
Conductivity (hydraulic)	m/yr	CONSTANT	100.	-999.	0.100E-06	0.100E+09
Gradient (hydraulic)		CONSTANT	0.500E-02	-999.	0.100E-07	-999.
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Temperature of aquifer	C	CONSTANT	28.0	-999.	0.000E+00	100.
pH	--	CONSTANT	7.50	-999.	0.300	14.0
Organic carbon content (fraction)		CONSTANT	0.100E-02	-999.	0.100E-05	1.00
Well distance from site	m	CONSTANT	15.0	-999.	1.00	-999.
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00

CONCENTRATION AFTER SATURATED ZONE MODEL 0.1208E-04

U. S. ENVIRONMENTAL PROTECTION AGENCY
 EXPOSURE ASSESSMENT
 MULTIMEDIA MODEL
 MULTIMED (Version 1.01, June 1991)

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Run options

AMARILLO ALTERNATE LINER DEMONSTRATION - transient leakage

Betaa VG sensitivity - WHOLE SITE, AVG LEAKAGE 200-year duration
 Chemical simulated is DEFAULT CHEMICAL

Option Chosen	Saturated and unsaturated zone models
Run was	DETERMIN
Infiltration input by user	
Run was transient	
Reject runs if Y coordinate outside plume	
Do not reject runs if Z coordinate outside plume	
Gaussian source used in saturated zone model	

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UNSATURATED ZONE FLOW MODEL PARAMETERS		
(input parameter description and value)		
NP	- Total number of nodal points	240
NMAT	- Number of different porous materials	1
KPROP	- Van Genuchten or Brooks and Corey	1
IMSHGN	- Spatial discretization option	1
NVFLAYR	- Number of layers in flow model	1

OPTIONS CHOSEN

Van Genuchten functional coefficients
 in defined coordinate system

Layer information

LAYER NO.	LAYER THICKNESS	MATERIAL PROPERTY
1	31.80	1

DATA FOR MATERIAL 1

VADOSE ZONE MATERIAL VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Saturated hydraulic conductivity	cm/hr	CONSTANT	0.360	-999.	0.100E-10	0.100E+05
Unsaturated zone porosity	--	CONSTANT	0.430	-999.	0.100E-08	0.990
Air entry pressure head	m	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Depth of the unsaturated zone	m	CONSTANT	31.8	-999.	0.100E-08	-999.

DATA FOR MATERIAL 1

VADOSE ZONE FUNCTION VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Residual water content	--	CONSTANT	0.700E-01	-999.	0.100E-08	1.00
Brook and Corey exponent, EN	--	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
ALFA coefficient	1/cm	CONSTANT	0.500E-02	-999.	0.000E+00	1.00
Van Genuchten exponent, ENN	--	CONSTANT	1.23	-999.	1.00	5.00

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UNSATURATED ZONE TRANSPORT MODEL PARAMETERS

NLAY	- Number of different layers used	1
NTSTPS	- Number of time values concentration calc	40
DUMMY	- Not presently used	1
ISOL	- Type of scheme used in unsaturated zone	1
N	- Stehfest terms or number of increments	18
NTEL	- Points in Lagrangian interpolation	3
NGPTS	- Number of Gauss points	104
NIT	- Convolution integral segments	2
IBOUND	- Type of boundary condition	2
ITSGEN	- Time values generated or input	1
TMAX	- Max simulation time	-- 0.0
WTFUN	- Weighting factor	-- 1.2

OPTIONS CHOSEN

Stehfest numerical inversion algorithm
 Nondecaying pulse source
 Computer generated times for computing concentrations

DATA FOR LAYER 1

 VADOSE TRANSPORT VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Thickness of layer	m	CONSTANT	31.8	-999.	0.100E-08	-999.
Longitudinal dispersivity of layer	m	DERIVED	-999.	-999.	0.100E-02	0.100E+05
Percent organic matter	--	CONSTANT	1.00	-999.	0.000E+00	100.
Bulk density of soil for layer	g/cc	CONSTANT	1.60	-999.	0.100E-01	5.00
Biological decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.

CHEMICAL SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Solid phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Dissolved phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Overall chemical decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Acid catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Neutral hydrolysis rate constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Base catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Reference temperature	C	CONSTANT	25.0	-999.	0.000E+00	100.
Normalized distribution coefficient	ml/g	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Distribution coefficient	--	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Biodegradation coefficient (sat. zone)	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Air diffusion coefficient	cm ² /s	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
Reference temperature for air diffusion	C	CONSTANT	25.0	-999.	0.000E+00	100.
Molecular weight	g/M	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Mole fraction of solute	--	CONSTANT	0.000E+00	-999.	0.100E-08	1.00
Vapor pressure of solute	mm Hg	CONSTANT	0.000E+00	-999.	0.000E+00	100.
Henry's law constant	atm-m ³ /M	CONSTANT	0.000E+00	-999.	0.100E-09	1.00
Overall 1st order decay sat. zone	1/yr	DERIVED	0.000E+00	0.000E+00	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00

SOURCE SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Infiltration rate	m/yr	CONSTANT	0.273E-04	-999.	0.100E-09	0.100E+11
Area of waste disposal unit	m ²	CONSTANT	0.197E+07	-999.	0.100E-01	-999.
Duration of pulse	yr	CONSTANT	200.	-999.	0.100E-08	-999.
Spread of contaminant source	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Recharge rate	m/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11
Source decay constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Initial concentration at landfill	mg/l	CONSTANT	1.00	-999.	0.000E+00	-999.
Length scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Width scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Near field dilution		DERIVED	1.00	0.000E+00	0.000E+00	1.00

AQUIFER SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Particle diameter	cm	CONSTANT	0.100E-03	-999.	0.100E-08	100.
Aquifer porosity	--	CONSTANT	0.200	-999.	0.100E-08	0.990
Bulk density	g/cc	CONSTANT	1.50	-999.	0.100E-01	5.00
Aquifer thickness	m	CONSTANT	12.2	-999.	0.100E-08	0.100E+06
Source thickness (mixing zone depth)	m	DERIVED	-999.	-999.	0.100E-08	0.100E+06
Conductivity (hydraulic)	m/yr	CONSTANT	100.	-999.	0.100E-06	0.100E+09
Gradient (hydraulic)		CONSTANT	0.500E-02	-999.	0.100E-07	-999.
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Temperature of aquifer	C	CONSTANT	28.0	-999.	0.000E+00	100.
pH	--	CONSTANT	7.50	-999.	0.300	14.0
Organic carbon content (fraction)		CONSTANT	0.100E-02	-999.	0.100E-05	1.00
Well distance from site	m	CONSTANT	15.0	-999.	1.00	-999.
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00

CONCENTRATION AFTER SATURATED ZONE MODEL 0.1285E-04

AMR BETA 2

U. S. ENVIRONMENTAL PROTECTION AGENCY
 EXPOSURE ASSESSMENT
 MULTIMEDIA MODEL
 MULTIMED (Version 1.01, June 1991)

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Run options

AMARILLO ALTERNATE LINER DEMONSTRATION - transient leakage

Betaa VG sensitivity - WHOLE SITE, AVG LEAKAGE 200-year duration
 Chemical simulated is DEFAULT CHEMICAL

Option Chosen	Saturated and unsaturated zone models
Run was	DETERMIN
Infiltration input by user	
Run was transient	
Reject runs if Y coordinate outside plume	
Do not reject runs if Z coordinate outside plume	
Gaussian source used in saturated zone model	

1

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UNSATURATED ZONE FLOW MODEL PARAMETERS
 (input parameter description and value)

NP	- Total number of nodal points	240
NMAT	- Number of different porous materials	1
KPROP	- Van Genuchten or Brooks and Corey	1
IMSHGN	- Spatial discretization option	1
NVFLAYR	- Number of layers in flow model	1

OPTIONS CHOSEN

Van Genuchten functional coefficients
 or defined coordinate system

Layer information

LAYER NO.	LAYER THICKNESS	MATERIAL PROPERTY
1	31.80	1

DATA FOR MATERIAL 1

VADOSE ZONE MATERIAL VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Saturated hydraulic conductivity	cm/hr	CONSTANT	0.360	-999.	0.100E-10	0.100E+05
Unsaturated zone porosity	--	CONSTANT	0.430	-999.	0.100E-08	0.990
Air entry pressure head	m	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Depth of the unsaturated zone	m	CONSTANT	31.8	-999.	0.100E-08	-999.

DATA FOR MATERIAL 1

VADOSE ZONE FUNCTION VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Residual water content	--	CONSTANT	0.700E-01	-999.	0.100E-08	1.00
Brook and Corey exponent, EN	--	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
ALFA coefficient	1/cm	CONSTANT	0.500E-02	-999.	0.000E+00	1.00
Van Genuchten exponent, ENN	--	CONSTANT	2.68	-999.	1.00	5.00

UNSATURATED ZONE TRANSPORT MODEL PARAMETERS

NLAY	- Number of different layers used	1
NTSTPS	- Number of time values concentration calc	40
DUMMY	- Not presently used	1
ISOL	- Type of scheme used in unsaturated zone	1
N	- Stehfest terms or number of increments	18
NTEL	- Points in Lagrangian interpolation	3
NGPTS	- Number of Gauss points	104
NIT	- Convolution integral segments	2
IBOUND	- Type of boundary condition	2
ITSGEN	- Time values generated or input	1
TMAX	- Max simulation time	-- 0.0
WTFUN	- Weighting factor	-- 1.2

OPTIONS CHOSEN

Stehfest numerical inversion algorithm
 Nondecaying pulse source
 Computer generated times for computing concentrations

DATA FOR LAYER 1

 VAPOSE TRANSPORT VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Thickness of layer	m	CONSTANT	31.8	-999.	0.100E-08	-999.
Longitudinal dispersivity of layer	m	DERIVED	-999.	-999.	0.100E-02	0.100E+05
Percent organic matter	--	CONSTANT	1.00	-999.	0.000E+00	100.
Bulk density of soil for layer	g/cc	CONSTANT	1.60	-999.	0.100E-01	5.00
Biological decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.

CHEMICAL SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Solid phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Dissolved phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Overall chemical decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Acid catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Neutral hydrolysis rate constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Base catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Reference temperature	C	CONSTANT	25.0	-999.	0.000E+00	100.
Normalized distribution coefficient	ml/g	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Distribution coefficient	--	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Biodegradation coefficient (sat. zone)	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Air diffusion coefficient	cm ² /s	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
Reference temperature for air diffusion	C	CONSTANT	25.0	-999.	0.000E+00	100.
Molecular weight	g/M	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Mole fraction of solute	--	CONSTANT	0.000E+00	-999.	0.100E-08	1.00
Vapor pressure of solute	mm Hg	CONSTANT	0.000E+00	-999.	0.000E+00	100.
Henry's law constant	atm-m ³ /M	CONSTANT	0.000E+00	-999.	0.100E-09	1.00
Overall 1st order decay sat. zone	1/yr	DERIVED	0.000E+00	0.000E+00	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00

SOURCE SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Infiltration rate	m/yr	CONSTANT	0.273E-04	-999.	0.100E-09	0.100E+11
Area of waste disposal unit	m ²	CONSTANT	0.197E+07	-999.	0.100E-01	-999.
Duration of pulse	yr	CONSTANT	200.	-999.	0.100E-08	-999.
Spread of contaminant source	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Recharge rate	m/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11
Source decay constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Initial concentration at landfill	mg/l	CONSTANT	1.00	-999.	0.000E+00	-999.
Length scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Width scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Near field dilution		DERIVED	1.00	0.000E+00	0.000E+00	1.00

AQUIFER SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Particle diameter	cm	CONSTANT	0.100E-03	-999.	0.100E-08	100.
Aquifer porosity	--	CONSTANT	0.200	-999.	0.100E-08	0.990
Bulk density	g/cc	CONSTANT	1.50	-999.	0.100E-01	5.00
Aquifer thickness	m	CONSTANT	12.2	-999.	0.100E-08	0.100E+06
Source thickness (mixing zone depth)	m	DERIVED	-999.	-999.	0.100E-08	0.100E+06
Conductivity (hydraulic)	m/yr	CONSTANT	100.	-999.	0.100E-06	0.100E+09
Gradient (hydraulic)		CONSTANT	0.500E-02	-999.	0.100E-07	-999.
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Temperature of aquifer	C	CONSTANT	28.0	-999.	0.000E+00	100.
pH	--	CONSTANT	7.50	-999.	0.300	14.0
Organic carbon content (fraction)		CONSTANT	0.100E-02	-999.	0.100E-05	1.00
Well distance from site	m	CONSTANT	15.0	-999.	1.00	-999.
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00

CONCENTRATION AFTER SATURATED ZONE MODEL 0.3240E-04

AM BOTH VG

U. S. ENVIRONMENTAL PROTECTION AGENCY
 EXPOSURE ASSESSMENT
 MULTIMEDIA MODEL
 MULTIMED (Version 1.01, June 1991)

1

Run options

AMARILLO ALTERNATE LINER DEMONSTRATION - transient leakage

Dual VG sensitivity - WHOLE SITE, AVG LEAKAGE 200-year duration
 Chemical simulated is DEFAULT CHEMICAL

Option Chosen	Saturated and unsaturated zone models
Run was	DETERMIN
Infiltration input by user	
Run was transient	
Reject runs if Y coordinate outside plume	
Do not reject runs if Z coordinate outside plume	
Gaussian source used in saturated zone model	

1

1

UNSATURATED ZONE FLOW MODEL PARAMETERS

(input parameter description and value)

NP	- Total number of nodal points	240
NMAT	- Number of different porous materials	1
KPROP	- Van Genuchten or Brooks and Corey	1
IMSHGN	- Spatial discretization option	1
NVFLAYR	- Number of layers in flow model	1

OPTIONS CHOSEN

Van Genuchten functional coefficients
 for defined coordinate system

Layer information

LAYER NO.	LAYER THICKNESS	MATERIAL PROPERTY
1	31.80	1

DATA FOR MATERIAL 1

VADOSE ZONE MATERIAL VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Saturated hydraulic conductivity	cm/hr	CONSTANT	0.360	-999.	0.100E-10	0.100E+05
Unsaturated zone porosity	--	CONSTANT	0.430	-999.	0.100E-08	0.990
Air entry pressure head	m	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Depth of the unsaturated zone	m	CONSTANT	31.8	-999.	0.100E-08	-999.

DATA FOR MATERIAL 1

VADOSE ZONE FUNCTION VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Residual water content	--	CONSTANT	0.700E-01	-999.	0.100E-08	1.00
Brook and Corey exponent, EN	--	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
ALFA coefficient	1/cm	CONSTANT	0.145	-999.	0.000E+00	1.00
Van Genuchten exponent, ENN	--	CONSTANT	2.68	-999.	1.00	5.00

UNSATURATED ZONE TRANSPORT MODEL PARAMETERS

NLAY	- Number of different layers used	1
NTSTPS	- Number of time values concentration calc	40
DUMMY	- Not presently used	1
ISOL	- Type of scheme used in unsaturated zone	1
N	- Stehfest terms or number of increments	18
NTEL	- Points in Lagrangian interpolation	3
NGPTS	- Number of Gauss points	104
NIT	- Convolution integral segments	2
IBOUND	- Type of boundary condition	2
ITSGEN	- Time values generated or input	1
TMAX	- Max simulation time	-- 0.0
WTFUN	- Weighting factor	-- 1.2

OPTIONS CHOSEN

Stehfest numerical inversion algorithm
 Nondecaying pulse source
 Computer generated times for computing concentrations

DATA FOR LAYER 1

VADOSE TRANSPORT VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Thickness of layer	m	CONSTANT	31.8	-999.	0.100E-08	-999.
Longitudinal dispersivity of layer	m	DERIVED	-999.	-999.	0.100E-02	0.100E+05
Percent organic matter	--	CONSTANT	1.00	-999.	0.000E+00	100.
Bulk density of soil for layer	g/cc	CONSTANT	1.60	-999.	0.100E-01	5.00
Biological decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.

CHEMICAL SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Solid phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Dissolved phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Overall chemical decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Acid catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Neutral hydrolysis rate constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Base catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Reference temperature	C	CONSTANT	25.0	-999.	0.000E+00	100.
Normalized distribution coefficient	ml/g	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Distribution coefficient	--	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Biodegradation coefficient (sat. zone)	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Air diffusion coefficient	cm ² /s	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
Reference temperature for air diffusion	C	CONSTANT	25.0	-999.	0.000E+00	100.
Molecular weight	g/M	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Mole fraction of solute	--	CONSTANT	0.000E+00	-999.	0.100E-08	1.00
Vapor pressure of solute	mm Hg	CONSTANT	0.000E+00	-999.	0.000E+00	100.
Henry's law constant	atm-m ³ /M	CONSTANT	0.000E+00	-999.	0.100E-09	1.00
Overall 1st order decay sat. zone	1/yr	DERIVED	0.000E+00	0.000E+00	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00

SOURCE SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Infiltration rate	m/yr	CONSTANT	0.273E-04	-999.	0.100E-09	0.100E+11
Area of waste disposal unit	m ²	CONSTANT	0.197E+07	-999.	0.100E-01	-999.
Duration of pulse	yr	CONSTANT	200.	-999.	0.100E-08	-999.
Spread of contaminant source	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Recharge rate	m/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11
Source decay constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Initial concentration at landfill	mg/l	CONSTANT	1.00	-999.	0.000E+00	-999.
Length scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Width scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Near field dilution		DERIVED	1.00	0.000E+00	0.000E+00	1.00

AQUIFER SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Particle diameter	cm	CONSTANT	0.100E-03	-999.	0.100E-08	100.
Aquifer porosity	--	CONSTANT	0.200	-999.	0.100E-08	0.990
Bulk density	g/cc	CONSTANT	1.50	-999.	0.100E-01	5.00
Aquifer thickness	m	CONSTANT	12.2	-999.	0.100E-08	0.100E+06
Source thickness (mixing zone depth)	m	DERIVED	-999.	-999.	0.100E-08	0.100E+06
Conductivity (hydraulic)	m/yr	CONSTANT	100.	-999.	0.100E-06	0.100E+09
Gradient (hydraulic)		CONSTANT	0.500E-02	-999.	0.100E-07	-999.
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Temperature of aquifer	C	CONSTANT	28.0	-999.	0.000E+00	100.
pH	--	CONSTANT	7.50	-999.	0.300	14.0
Organic carbon content (fraction)		CONSTANT	0.100E-02	-999.	0.100E-05	1.00
Well distance from site	m	CONSTANT	15.0	-999.	1.00	-999.
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00

CONCENTRATION AFTER SATURATED ZONE MODEL 0.4639E-04

OPTIONS CHOSEN

Van Genuchten functional coefficients
 for defined coordinate system

Layer information

LAYER NO.	LAYER THICKNESS	MATERIAL PROPERTY
1	31.80	1

DATA FOR MATERIAL 1

VADOSE ZONE MATERIAL VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Saturated hydraulic conductivity	cm/hr	CONSTANT	0.360	-999.	0.100E-10	0.100E+05
Unsaturated zone porosity	--	CONSTANT	0.430	-999.	0.100E-08	0.990
Air entry pressure head	m	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Depth of the unsaturated zone	m	CONSTANT	31.8	-999.	0.100E-08	-999.

DATA FOR MATERIAL 1

VADOSE ZONE FUNCTION VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Residual water content	--	CONSTANT	0.700E-01	-999.	0.100E-08	1.00
Brook and Corey exponent, EN	--	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
ALFA coefficient	1/cm	CONSTANT	0.500E-02	-999.	0.000E+00	1.00
Van Genuchten exponent, ENN	--	CONSTANT	1.09	-999.	1.00	5.00

UNSATURATED ZONE TRANSPORT MODEL PARAMETERS

NLAY	- Number of different layers used	1
NTSTPS	- Number of time values concentration calc	40
DUMMY	- Not presently used	1
ISOL	- Type of scheme used in unsaturated zone	1
N	- Stehfest terms or number of increments	18
NTEL	- Points in Lagrangian interpolation	3
NGPTS	- Number of Gauss points	104
NIT	- Convolution integral segments	2
IBOUND	- Type of boundary condition	2
ITSGEN	- Time values generated or input	1
TMAX	- Max simulation time	-- 0.0
WTFUN	- Weighting factor	-- 1.2

OPTIONS CHOSEN

Stehfest numerical inversion algorithm
 Nondecaying pulse source
 Computer generated times for computing concentrations

DATA FOR LAYER 1

VADOSE TRANSPORT VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Thickness of layer	m	CONSTANT	31.8	-999.	0.100E-08	-999.
Longitudinal dispersivity of layer	m	DERIVED	-999.	-999.	0.100E-02	0.100E+05
Percent organic matter	--	CONSTANT	1.00	-999.	0.000E+00	100.
Bulk density of soil for layer	g/cc	CONSTANT	1.60	-999.	0.100E-01	5.00
Biological decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.

CHEMICAL SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Solid phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Dissolved phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Overall chemical decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Acid catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Neutral hydrolysis rate constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Base catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Reference temperature	C	CONSTANT	25.0	-999.	0.000E+00	100.
Normalized distribution coefficient	ml/g	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Distribution coefficient	--	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Biodegradation coefficient (sat. zone)	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Air diffusion coefficient	cm ² /s	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
Reference temperature for air diffusion	C	CONSTANT	25.0	-999.	0.000E+00	100.
Molecular weight	g/M	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Mole fraction of solute	--	CONSTANT	0.000E+00	-999.	0.100E-08	1.00
Vapor pressure of solute	mm Hg	CONSTANT	0.000E+00	-999.	0.000E+00	100.
Henry's law constant	atm-m ³ /M	CONSTANT	0.000E+00	-999.	0.100E-09	1.00
Overall 1st order decay sat. zone	1/yr	DERIVED	0.000E+00	0.000E+00	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00

SOURCE SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Infiltration rate	m/yr	CONSTANT	0.273E-04	-999.	0.100E-09	0.100E+11
Area of waste disposal unit	m ²	CONSTANT	0.197E+07	-999.	0.100E-01	-999.
Duration of pulse	yr	CONSTANT	200.	-999.	0.100E-08	-999.
Spread of contaminant source	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Recharge rate	m/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11
Source decay constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Initial concentration at landfill	mg/l	CONSTANT	1.00	-999.	0.000E+00	-999.
Length scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Width scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Near field dilution		DERIVED	1.00	0.000E+00	0.000E+00	1.00

AQUIFER SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Particle diameter	cm	CONSTANT	0.100E-03	-999.	0.100E-08	100.
Aquifer porosity	--	CONSTANT	0.400	-999.	0.100E-08	0.990
Bulk density	g/cc	CONSTANT	1.50	-999.	0.100E-01	5.00
Aquifer thickness	m	CONSTANT	12.2	-999.	0.100E-08	0.100E+06
Source thickness (mixing zone depth)	m	DERIVED	-999.	-999.	0.100E-08	0.100E+06
Conductivity (hydraulic)	m/yr	CONSTANT	100.	-999.	0.100E-06	0.100E+09
Gradient (hydraulic)		CONSTANT	0.500E-02	-999.	0.100E-07	-999.
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Temperature of aquifer	C	CONSTANT	28.0	-999.	0.000E+00	100.
pH	--	CONSTANT	7.50	-999.	0.300	14.0
Organic carbon content (fraction)		CONSTANT	0.100E-02	-999.	0.100E-05	1.00
Well distance from site	m	CONSTANT	15.0	-999.	1.00	-999.
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00

CONCENTRATION AFTER SATURATED ZONE MODEL 0.1052E-04

OPTIONS CHOSEN

Van Genuchten functional coefficients
 r defined coordinate system

Layer information

LAYER NO.	LAYER THICKNESS	MATERIAL PROPERTY
1	31.80	1

DATA FOR MATERIAL 1

VADOSE ZONE MATERIAL VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Saturated hydraulic conductivity	cm/hr	CONSTANT	0.360	-999.	0.100E-10	0.100E+05
Unsaturated zone porosity	--	CONSTANT	0.430	-999.	0.100E-08	0.990
Air entry pressure head	m	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Depth of the unsaturated zone	m	CONSTANT	31.8	-999.	0.100E-08	-999.

DATA FOR MATERIAL 1

VADOSE ZONE FUNCTION VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Residual water content	--	CONSTANT	0.700E-01	-999.	0.100E-08	1.00
Brook and Corey exponent, EN	--	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
ALFA coefficient	1/cm	CONSTANT	0.500E-02	-999.	0.000E+00	1.00
Van Genuchten exponent, ENN	--	CONSTANT	1.09	-999.	1.00	5.00

UNSATURATED ZONE TRANSPORT MODEL PARAMETERS

NLAY	- Number of different layers used	1
NTSTPS	- Number of time values concentration calc	40
DUMMY	- Not presently used	1
ISOL	- Type of scheme used in unsaturated zone	1
N	- Stehfest terms or number of increments	18
NTEL	- Points in Lagrangian interpolation	3
NGPTS	- Number of Gauss points	104
NIT	- Convolution integral segments	2
IBOUND	- Type of boundary condition	2
ITSGEN	- Time values generated or input	1
TMAX	- Max simulation time	-- 0.0
WTFUN	- Weighting factor	-- 1.2

OPTIONS CHOSEN

Stehfest numerical inversion algorithm
 Nondecaying pulse source
 Computer generated times for computing concentrations

DATA FOR LAYER 1

VADOSE TRANSPORT VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Thickness of layer	m	CONSTANT	31.8	-999.	0.100E-08	-999.
Longitudinal dispersivity of layer	m	DERIVED	-999.	-999.	0.100E-02	0.100E+05
Percent organic matter	--	CONSTANT	1.00	-999.	0.000E+00	100.
Bulk density of soil for layer	g/cc	CONSTANT	1.60	-999.	0.100E-01	5.00
Biological decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.

CHEMICAL SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Solid phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Dissolved phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Overall chemical decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Acid catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Neutral hydrolysis rate constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Base catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Reference temperature	C	CONSTANT	25.0	-999.	0.000E+00	100.
Normalized distribution coefficient	ml/g	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Distribution coefficient	--	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Biodegradation coefficient (sat. zone)	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Air diffusion coefficient	cm ² /s	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
Reference temperature for air diffusion	C	CONSTANT	25.0	-999.	0.000E+00	100.
Molecular weight	g/M	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Mole fraction of solute	--	CONSTANT	0.000E+00	-999.	0.100E-08	1.00
Vapor pressure of solute	mm Hg	CONSTANT	0.000E+00	-999.	0.000E+00	100.
Henry's law constant	atm-m ³ /M	CONSTANT	0.000E+00	-999.	0.100E-09	1.00
Overall 1st order decay sat. zone	1/yr	DERIVED	0.000E+00	0.000E+00	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00

SOURCE SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Infiltration rate	m/yr	CONSTANT	0.273E-04	-999.	0.100E-09	0.100E+11
Area of waste disposal unit	m ²	CONSTANT	0.197E+07	-999.	0.100E-01	-999.
Duration of pulse	yr	CONSTANT	200.	-999.	0.100E-08	-999.
Spread of contaminant source	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Recharge rate	m/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11
Source decay constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Initial concentration at landfill	mg/l	CONSTANT	1.00	-999.	0.000E+00	-999.
Length scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Width scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Near field dilution		DERIVED	1.00	0.000E+00	0.000E+00	1.00

AQUIFER SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Particle diameter	cm	CONSTANT	0.100E-03	-999.	0.100E-08	100.
Aquifer porosity	--	CONSTANT	0.200	-999.	0.100E-08	0.990
Bulk density	g/cc	CONSTANT	1.50	-999.	0.100E-01	5.00
Aquifer thickness	m	CONSTANT	12.2	-999.	0.100E-08	0.100E+06
Source thickness (mixing zone depth)	m	DERIVED	-999.	-999.	0.100E-08	0.100E+06
Conductivity (hydraulic)	m/yr	CONSTANT	0.100E+04	-999.	0.100E-06	0.100E+09
Gradient (hydraulic)		CONSTANT	0.500E-02	-999.	0.100E-07	-999.
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Temperature of aquifer	C	CONSTANT	28.0	-999.	0.000E+00	100.
pH	--	CONSTANT	7.50	-999.	0.300	14.0
Organic carbon content (fraction)		CONSTANT	0.100E-02	-999.	0.100E-05	1.00
Well distance from site	m	CONSTANT	15.0	-999.	1.00	-999.
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00

CONCENTRATION AFTER SATURATED ZONE MODEL 0.1052E-05

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STEDYBAS

U. S. ENVIRONMENTAL PROTECTION AGENCY
EXPOSURE ASSESSMENT
MULTIMEDIA MODEL
MULTIMED (Version 1.01, June 1991)

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Run options

AMARILLO ALTERNATE LINER DEMONSTRATION - STEADY STATE MODEL

BASE MODEL - 20 ACRES, AVG LEAKAGE
Chemical simulated is DEFAULT CHEMICAL

Option Chosen Saturated zone model
Run was DETERMIN
Infiltration input by user
Run was steady-state
Reject runs if Y coordinate outside plume
Do not reject runs if Z coordinate outside plume
Gaussian source used in saturated zone model

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CHEMICAL SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Solid phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11

Dissolved phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Overall chemical decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Acid catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Neutral hydrolysis rate constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Base catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Reference temperature	C	CONSTANT	25.0	-999.	0.000E+00	100.
Normalized distribution coefficient	ml/g	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Distribution coefficient	--	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Biodegradation coefficient (sat. zone)	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Air diffusion coefficient	cm ² /s	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
Reference temperature for air diffusion	C	CONSTANT	25.0	-999.	0.000E+00	100.
Molecular weight	g/M	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Mole fraction of solute	--	CONSTANT	0.000E+00	-999.	0.100E-08	1.00
Vapor pressure of solute	mm Hg	CONSTANT	0.000E+00	-999.	0.000E+00	100.
Henry's law constant	atm-m ³ /M	CONSTANT	0.000E+00	-999.	0.100E-09	1.00
Overall 1st order decay sat. zone	1/yr	DERIVED	0.000E+00	0.000E+00	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00

SOURCE SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Infiltration rate	m/yr	CONSTANT	0.273E-04	-999.	0.100E-09	0.100E+11
Area of waste disposal unit	m ²	CONSTANT	0.810E+05	-999.	0.100E-01	-999.
Duration of pulse	yr	CONSTANT	200.	-999.	0.100E-08	-999.
Spread of contaminant source	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Recharge rate	m/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11
Source decay constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Initial concentration at landfill	mg/l	CONSTANT	1.00	-999.	0.000E+00	-999.
Length scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Width scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Near field dilution		DERIVED	1.00	0.000E+00	0.000E+00	1.00

AQUIFER SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Particle diameter	cm	CONSTANT	0.100E-03	-999.	0.100E-08	100.
Aquifer porosity	--	CONSTANT	0.400	-999.	0.100E-08	0.990
Bulk density	g/cc	CONSTANT	1.50	-999.	0.100E-01	5.00
Aquifer thickness	m	CONSTANT	12.2	-999.	0.100E-08	0.100E+06
Source thickness (mixing zone depth)	m	DERIVED	-999.	-999.	0.100E-08	0.100E+06
Conductivity (hydraulic)	m/yr	CONSTANT	100.	-999.	0.100E-06	0.100E+09
Gradient (hydraulic)		CONSTANT	0.500E-02	-999.	0.100E-07	-999.
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Temperature of aquifer	C	CONSTANT	28.0	-999.	0.000E+00	100.
pH	--	CONSTANT	7.50	-999.	0.300	14.0
Organic carbon content (fraction)		CONSTANT	0.100E-02	-999.	0.100E-05	1.00
Well distance from site	m	CONSTANT	30.0	-999.	1.00	-999.
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00

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U. S. ENVIRONMENTAL PROTECTION AGENCY
EXPOSURE ASSESSMENT
MULTIMEDIA MODEL
MULTIMED (Version 1.01, June 1991)

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Run options

AMARILLO ALTERNATE LINER DEMONSTRATION - STEADY STATE MODEL

BASE MODEL - 20 ACRES, AVG LEAKAGE
Chemical simulated is DEFAULT CHEMICAL

Option Chosen Saturated zone model
Run was DETERMIN
Infiltration input by user
Run was steady-state
Reject runs if Y coordinate outside plume
Do not reject runs if Z coordinate outside plume
Gaussian source used in saturated zone model

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CHEMICAL SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Solid phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11

Dissolved phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Overall chemical decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Acid catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Neutral hydrolysis rate constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Base catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Reference temperature	C	CONSTANT	25.0	-999.	0.000E+00	100.
Normalized distribution coefficient	ml/g	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Distribution coefficient	--	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Biodegradation coefficient (sat. zone)	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Air diffusion coefficient	cm ² /s	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
Reference temperature for air diffusion	C	CONSTANT	25.0	-999.	0.000E+00	100.
Molecular weight	g/M	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Mole fraction of solute	--	CONSTANT	0.000E+00	-999.	0.100E-08	1.00
Vapor pressure of solute	mm Hg	CONSTANT	0.000E+00	-999.	0.000E+00	100.
Henry's law constant	atm-m ³ /M	CONSTANT	0.000E+00	-999.	0.100E-09	1.00
Overall 1st order decay sat. zone	1/yr	DERIVED	0.000E+00	0.000E+00	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00

SOURCE SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Infiltration rate	m/yr	CONSTANT	0.273E-04	-999.	0.100E-09	0.100E+11
Area of waste disposal unit	m ²	CONSTANT	0.810E+05	-999.	0.100E-01	-999.
Duration of pulse	yr	CONSTANT	200.	-999.	0.100E-08	-999.
Spread of contaminant source	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Recharge rate	m/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11
Source decay constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Initial concentration at landfill	mg/l	CONSTANT	1.00	-999.	0.000E+00	-999.
Length scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Width scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Near field dilution		DERIVED	1.00	0.000E+00	0.000E+00	1.00

AQUIFER SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Particle diameter	cm	CONSTANT	0.100E-03	-999.	0.100E-08	100.
Aquifer porosity	--	CONSTANT	0.400	-999.	0.100E-08	0.990
Bulk density	g/cc	CONSTANT	1.50	-999.	0.100E-01	5.00
Aquifer thickness	m	CONSTANT	12.2	-999.	0.100E-08	0.100E+06
Source thickness (mixing zone depth)	m	DERIVED	-999.	-999.	0.100E-08	0.100E+06
Conductivity (hydraulic)	m/yr	CONSTANT	100.	-999.	0.100E-06	0.100E+09
Gradient (hydraulic)		CONSTANT	0.500E-02	-999.	0.100E-07	-999.
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Temperature of aquifer	C	CONSTANT	28.0	-999.	0.000E+00	100.
pH	--	CONSTANT	7.50	-999.	0.300	14.0
Organic carbon content (fraction)		CONSTANT	0.100E-02	-999.	0.100E-05	1.00
Well distance from site	m	CONSTANT	470.	-999.	1.00	-999.
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00

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U. S. ENVIRONMENTAL PROTECTION AGENCY
 EXPOSURE ASSESSMENT
 MULTIMEDIA MODEL
 MULTIMED (Version 1.01, June 1991)

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Run options

AMARILLO ALTERNATE LINER DEMONSTRATION - STEADY STATE MODEL

aquifer hydraulic conductivity - 20 ACRES, AVG LEAKAGE
 Chemical simulated is DEFAULT CHEMICAL

Option Chosen Saturated zone model
 Run was DETERMIN
 Infiltration input by user
 Run was steady-state
 Reject runs if Y coordinate outside plume
 Do not reject runs if Z coordinate outside plume
 Gaussian source used in saturated zone model

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CHEMICAL SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Solid phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11

Dissolved phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Overall chemical decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Acid catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Neutral hydrolysis rate constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Base catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Reference temperature	C	CONSTANT	25.0	-999.	0.000E+00	100.
Normalized distribution coefficient	ml/g	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Distribution coefficient	--	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Biodegradation coefficient (sat. zone)	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Air diffusion coefficient	cm ² /s	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
Reference temperature for air diffusion	C	CONSTANT	25.0	-999.	0.000E+00	100.
Molecular weight	g/M	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Mole fraction of solute	--	CONSTANT	0.000E+00	-999.	0.100E-08	1.00
Vapor pressure of solute	mm Hg	CONSTANT	0.000E+00	-999.	0.000E+00	100.
Henry's law constant	atm-m ³ /M	CONSTANT	0.000E+00	-999.	0.100E-09	1.00
Overall 1st order decay sat. zone	1/yr	DERIVED	0.000E+00	0.000E+00	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00

SOURCE SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Infiltration rate	m/yr	CONSTANT	0.273E-04	-999.	0.100E-09	0.100E+11
Area of waste disposal unit	m ²	CONSTANT	0.810E+05	-999.	0.100E-01	-999.
Duration of pulse	yr	CONSTANT	200.	-999.	0.100E-08	-999.
Spread of contaminant source	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Recharge rate	m/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11
Source decay constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Initial concentration at landfill	mg/l	CONSTANT	1.00	-999.	0.000E+00	-999.
Length scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Width scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Near field dilution		DERIVED	1.00	0.000E+00	0.000E+00	1.00

AQUIFER SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Particle diameter	cm	CONSTANT	0.100E-03	-999.	0.100E-08	100.
Aquifer porosity	--	CONSTANT	0.400	-999.	0.100E-08	0.990
Bulk density	g/cc	CONSTANT	1.50	-999.	0.100E-01	5.00
Aquifer thickness	m	CONSTANT	12.2	-999.	0.100E-08	0.100E+06
Source thickness (mixing zone depth)	m	DERIVED	-999.	-999.	0.100E-08	0.100E+06
Conductivity (hydraulic)	m/yr	CONSTANT	0.100E+04	-999.	0.100E-06	0.100E+09
Gradient (hydraulic)		CONSTANT	0.500E-02	-999.	0.100E-07	-999.
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Temperature of aquifer	C	CONSTANT	28.0	-999.	0.000E+00	100.
pH	--	CONSTANT	7.50	-999.	0.300	14.0
Organic carbon content (fraction)		CONSTANT	0.100E-02	-999.	0.100E-05	1.00
Well distance from site	m	CONSTANT	30.0	-999.	1.00	-999.
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00

U. S. ENVIRONMENTAL PROTECTION AGENCY
EXPOSURE ASSESSMENT
MULTIMEDIA MODEL
MULTIMED (Version 1.01, June 1991)

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Run options

AMARILLO ALTERNATE LINER DEMONSTRATION - STEADY STATE MODEL

Hydraulic Gradient - 20 ACRES, AVG LEAKAGE
Chemical simulated is DEFAULT CHEMICAL

Option Chosen Saturated zone model
Run was DETERMIN
Infiltration input by user
Run was steady-state
Reject runs if Y coordinate outside plume
Do not reject runs if Z coordinate outside plume
Gaussian source used in saturated zone model

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CHEMICAL SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Solid phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11

Dissolved phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Overall chemical decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Acid catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Neutral hydrolysis rate constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Base catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Reference temperature	C	CONSTANT	25.0	-999.	0.000E+00	100.
Normalized distribution coefficient	ml/g	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Distribution coefficient	--	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Biodegradation coefficient (sat. zone)	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Air diffusion coefficient	cm ² /s	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
Reference temperature for air diffusion	C	CONSTANT	25.0	-999.	0.000E+00	100.
Molecular weight	g/M	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Mole fraction of solute	--	CONSTANT	0.000E+00	-999.	0.100E-08	1.00
Vapor pressure of solute	mm Hg	CONSTANT	0.000E+00	-999.	0.000E+00	100.
Henry's law constant	atm-m ³ /M	CONSTANT	0.000E+00	-999.	0.100E-09	1.00
Overall 1st order decay sat. zone	1/yr	DERIVED	0.000E+00	0.000E+00	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00

SOURCE SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Infiltration rate	m/yr	CONSTANT	0.273E-04	-999.	0.100E-09	0.100E+11
Area of waste disposal unit	m ²	CONSTANT	0.810E+05	-999.	0.100E-01	-999.
Duration of pulse	yr	CONSTANT	200.	-999.	0.100E-08	-999.
Spread of contaminant source	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Recharge rate	m/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11
Source decay constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Initial concentration at landfill	mg/l	CONSTANT	1.00	-999.	0.000E+00	-999.
Length scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Width scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Near field dilution		DERIVED	1.00	0.000E+00	0.000E+00	1.00

AQUIFER SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Particle diameter	cm	CONSTANT	0.100E-03	-999.	0.100E-08	100.
Aquifer porosity	--	CONSTANT	0.400	-999.	0.100E-08	0.990
Bulk density	g/cc	CONSTANT	1.50	-999.	0.100E-01	5.00
Aquifer thickness	m	CONSTANT	12.2	-999.	0.100E-08	0.100E+06
Source thickness (mixing zone depth)	m	DERIVED	-999.	-999.	0.100E-08	0.100E+06
Conductivity (hydraulic)	m/yr	CONSTANT	100.	-999.	0.100E-06	0.100E+09
Gradient (hydraulic)		CONSTANT	0.700E-02	-999.	0.100E-07	-999.
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Temperature of aquifer	C	CONSTANT	28.0	-999.	0.000E+00	100.
pH	--	CONSTANT	7.50	-999.	0.300	14.0
Organic carbon content (fraction)		CONSTANT	0.100E-02	-999.	0.100E-05	1.00
Well distance from site	m	CONSTANT	30.0	-999.	1.00	-999.
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00

AMSS MIX

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U. S. ENVIRONMENTAL PROTECTION AGENCY
 EXPOSURE ASSESSMENT
 MULTIMEDIA MODEL
 MULTIMED (Version 1.01, June 1991)

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Run options

AMARILLO ALTERNATE LINER DEMONSTRATION - STEADY STATE MODEL

12.2m mixing zone - 20 ACRES, AVG LEAKAGE
 Chemical simulated is DEFAULT CHEMICAL

Option Chosen Saturated zone model
 Run was DETERMIN
 Infiltration input by user
 Run was steady-state
 Reject runs if Y coordinate outside plume
 Do not reject runs if Z coordinate outside plume
 Gaussian source used in saturated zone model

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CHEMICAL SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Solid phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11

Dissolved phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Overall chemical decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Acid catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Neutral hydrolysis rate constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Base catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Reference temperature	C	CONSTANT	25.0	-999.	0.000E+00	100.
Normalized distribution coefficient	ml/g	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Distribution coefficient	--	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Biodegradation coefficient (sat. zone)	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Air diffusion coefficient	cm ² /s	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
Reference temperature for air diffusion	C	CONSTANT	25.0	-999.	0.000E+00	100.
Molecular weight	g/M	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Mole fraction of solute	--	CONSTANT	0.000E+00	-999.	0.100E-08	1.00
Vapor pressure of solute	mm Hg	CONSTANT	0.000E+00	-999.	0.000E+00	100.
Henry's law constant	atm-m ³ /M	CONSTANT	0.000E+00	-999.	0.100E-09	1.00
Overall 1st order decay sat. zone	1/yr	DERIVED	0.000E+00	0.000E+00	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00

SOURCE SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Infiltration rate	m/yr	CONSTANT	0.273E-04	-999.	0.100E-09	0.100E+11
Area of waste disposal unit	m ²	CONSTANT	0.810E+05	-999.	0.100E-01	-999.
Duration of pulse	yr	CONSTANT	200.	-999.	0.100E-08	-999.
Spread of contaminant source	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Recharge rate	m/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11
Source decay constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Initial concentration at landfill	mg/l	CONSTANT	1.00	-999.	0.000E+00	-999.
Length scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Width scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Near field dilution		DERIVED	1.00	0.000E+00	0.000E+00	1.00

AQUIFER SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Particle diameter	cm	CONSTANT	0.100E-03	-999.	0.100E-08	100.
Aquifer porosity	--	CONSTANT	0.400	-999.	0.100E-08	0.990
Bulk density	g/cc	CONSTANT	1.50	-999.	0.100E-01	5.00
Aquifer thickness	m	CONSTANT	12.2	-999.	0.100E-08	0.100E+06
Source thickness (mixing zone depth)	m	CONSTANT	12.2	-999.	0.100E-08	0.100E+06
Conductivity (hydraulic)	m/yr	CONSTANT	100.	-999.	0.100E-06	0.100E+09
Gradient (hydraulic)		CONSTANT	0.500E-02	-999.	0.100E-07	-999.
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Temperature of aquifer	C	CONSTANT	28.0	-999.	0.000E+00	100.
pH	--	CONSTANT	7.50	-999.	0.300	14.0
Organic carbon content (fraction)		CONSTANT	0.100E-02	-999.	0.100E-05	1.00
Well distance from site	m	CONSTANT	30.0	-999.	1.00	-999.
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00

AMSSPORZ

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U. S. ENVIRONMENTAL PROTECTION AGENCY
 EXPOSURE ASSESSMENT
 MULTIMEDIA MODEL
 MULTIMED (Version 1.01, June 1991)

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 Run options

AMARILLO ALTERNATE LINER DEMONSTRATION - STEADY STATE MODEL

Porosity = 0.2 - 20 ACRES, AVG LEAKAGE
 Chemical simulated is DEFAULT CHEMICAL

Option Chosen Saturated zone model
 Run was DETERMIN
 Infiltration input by user
 Run was steady-state
 Reject runs if Y coordinate outside plume
 Do not reject runs if Z coordinate outside plume
 Gaussian source used in saturated zone model

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CHEMICAL SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Solid phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11

Dissolved phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Overall chemical decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Acid catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Neutral hydrolysis rate constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Base catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Reference temperature	C	CONSTANT	25.0	-999.	0.000E+00	100.
Normalized distribution coefficient	ml/g	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Distribution coefficient	--	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Biodegradation coefficient (sat. zone)	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Air diffusion coefficient	cm ² /s	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
Reference temperature for air diffusion	C	CONSTANT	25.0	-999.	0.000E+00	100.
Molecular weight	g/M	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Mole fraction of solute	--	CONSTANT	0.000E+00	-999.	0.100E-08	1.00
Vapor pressure of solute	mm Hg	CONSTANT	0.000E+00	-999.	0.000E+00	100.
Henry's law constant	atm-m ³ /M	CONSTANT	0.000E+00	-999.	0.100E-09	1.00
Overall 1st order decay sat. zone	1/yr	DERIVED	0.000E+00	0.000E+00	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00

SOURCE SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Infiltration rate	m/yr	CONSTANT	0.273E-04	-999.	0.100E-09	0.100E+11
Area of waste disposal unit	m ²	CONSTANT	0.810E+05	-999.	0.100E-01	-999.
Duration of pulse	yr	CONSTANT	200.	-999.	0.100E-08	-999.
Spread of contaminant source	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Recharge rate	m/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11
Source decay constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Initial concentration at landfill	mg/l	CONSTANT	1.00	-999.	0.000E+00	-999.
Length scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Width scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Near field dilution		DERIVED	1.00	0.000E+00	0.000E+00	1.00

AQUIFER SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Particle diameter	cm	CONSTANT	0.100E-03	-999.	0.100E-08	100.
Aquifer porosity	--	CONSTANT	0.200	-999.	0.100E-08	0.990
Bulk density	g/cc	CONSTANT	1.50	-999.	0.100E-01	5.00
Aquifer thickness	m	CONSTANT	12.2	-999.	0.100E-08	0.100E+06
Source thickness (mixing zone depth)	m	DERIVED	-999.	-999.	0.100E-08	0.100E+06
Conductivity (hydraulic)	m/yr	CONSTANT	100.	-999.	0.100E-06	0.100E+09
Gradient (hydraulic)		CONSTANT	0.500E-02	-999.	0.100E-07	-999.
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Temperature of aquifer	C	CONSTANT	28.0	-999.	0.000E+00	100.
pH	--	CONSTANT	7.50	-999.	0.300	14.0
Organic carbon content (fraction)		CONSTANT	0.100E-02	-999.	0.100E-05	1.00
Well distance from site	m	CONSTANT	30.0	-999.	1.00	-999.
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00

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U. S. ENVIRONMENTAL PROTECTION AGENCY
 EXPOSURE ASSESSMENT
 MULTIMEDIA MODEL
 MULTIMED (Version 1.01, June 1991)

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Run options

AMARILLO ALTERNATE LINER DEMONSTRATION - STEADY STATE MODEL

300m to POC - 20 ACRES, AVG LEAKAGE
 Chemical simulated is DEFAULT CHEMICAL

Option Chosen Saturated zone model
 Run was DETERMIN
 Infiltration input by user
 Run was steady-state
 Reject runs if Y coordinate outside plume
 Do not reject runs if Z coordinate outside plume
 Gaussian source used in saturated zone model

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CHEMICAL SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Solid phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11

Dissolved phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Overall chemical decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Acid catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Neutral hydrolysis rate constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Base catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Reference temperature	C	CONSTANT	25.0	-999.	0.000E+00	100.
Normalized distribution coefficient	ml/g	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Distribution coefficient	--	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Biodegradation coefficient (sat. zone)	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Air diffusion coefficient	cm ² /s	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
Reference temperature for air diffusion	C	CONSTANT	25.0	-999.	0.000E+00	100.
Molecular weight	g/M	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Mole fraction of solute	--	CONSTANT	0.000E+00	-999.	0.100E-08	1.00
Vapor pressure of solute	mm Hg	CONSTANT	0.000E+00	-999.	0.000E+00	100.
Henry's law constant	atm-m ³ /M	CONSTANT	0.000E+00	-999.	0.100E-09	1.00
Overall 1st order decay sat. zone	1/yr	DERIVED	0.000E+00	0.000E+00	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00

SOURCE SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Infiltration rate	m/yr	CONSTANT	0.273E-04	-999.	0.100E-09	0.100E+11
Area of waste disposal unit	m ²	CONSTANT	0.810E+05	-999.	0.100E-01	-999.
Duration of pulse	yr	CONSTANT	200.	-999.	0.100E-08	-999.
Spread of contaminant source	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Recharge rate	m/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11
Source decay constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Initial concentration at landfill	mg/l	CONSTANT	1.00	-999.	0.000E+00	-999.
Length scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Width scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Near field dilution		DERIVED	1.00	0.000E+00	0.000E+00	1.00

AQUIFER SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Particle diameter	cm	CONSTANT	0.100E-03	-999.	0.100E-08	100.
Aquifer porosity	--	CONSTANT	0.400	-999.	0.100E-08	0.990
Bulk density	g/cc	CONSTANT	1.50	-999.	0.100E-01	5.00
Aquifer thickness	m	CONSTANT	12.2	-999.	0.100E-08	0.100E+06
Source thickness (mixing zone depth)	m	DERIVED	-999.	-999.	0.100E-08	0.100E+06
Conductivity (hydraulic)	m/yr	CONSTANT	100.	-999.	0.100E-06	0.100E+09
Gradient (hydraulic)		CONSTANT	0.500E-02	-999.	0.100E-07	-999.
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Temperature of aquifer	C	CONSTANT	28.0	-999.	0.000E+00	100.
pH	--	CONSTANT	7.50	-999.	0.300	14.0
Organic carbon content (fraction)		CONSTANT	0.100E-02	-999.	0.100E-05	1.00
Well distance from site	m	CONSTANT	300.	-999.	1.00	-999.
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00

U. S. ENVIRONMENTAL PROTECTION AGENCY
 EXPOSURE ASSESSMENT
 MULTIMEDIA MODEL
 MULTIMED (Version 1.01, June 1991)

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Run options

AMARILLO ALTERNATE LINER DEMONSTRATION - STEADY STATE MODEL

BASE MODEL - 487 ACRES, AVG LEAKAGE
 Chemical simulated is DEFAULT CHEMICAL

Option Chosen Saturated zone model
 Run was DETERMIN
 Infiltration input by user
 Run was steady-state
 Reject runs if Y coordinate outside plume
 Do not reject runs if Z coordinate outside plume
 Gaussian source used in saturated zone model

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CHEMICAL SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Solid phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11

Dissolved phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Overall chemical decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Acid catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Neutral hydrolysis rate constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Base catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Reference temperature	C	CONSTANT	25.0	-999.	0.000E+00	100.
Normalized distribution coefficient	ml/g	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Distribution coefficient	--	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Biodegradation coefficient (sat. zone)	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Air diffusion coefficient	cm ² /s	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
Reference temperature for air diffusion	C	CONSTANT	25.0	-999.	0.000E+00	100.
Molecular weight	g/M	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Mole fraction of solute	--	CONSTANT	0.000E+00	-999.	0.100E-08	1.00
Vapor pressure of solute	mm Hg	CONSTANT	0.000E+00	-999.	0.000E+00	100.
Henry's law constant	atm-m ³ /M	CONSTANT	0.000E+00	-999.	0.100E-09	1.00
Overall 1st order decay sat. zone	1/yr	DERIVED	0.000E+00	0.000E+00	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00

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SOURCE SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Infiltration rate	m/yr	CONSTANT	0.273E-04	-999.	0.100E-09	0.100E+11
Area of waste disposal unit	m ²	CONSTANT	0.197E+07	-999.	0.100E-01	-999.
Duration of pulse	yr	CONSTANT	200.	-999.	0.100E-08	-999.
Spread of contaminant source	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Recharge rate	m/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11
Source decay constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Initial concentration at landfill	mg/l	CONSTANT	1.00	-999.	0.000E+00	-999.
Length scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Width scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Near field dilution		DERIVED	1.00	0.000E+00	0.000E+00	1.00

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AQUIFER SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Particle diameter	cm	CONSTANT	0.100E-03	-999.	0.100E-08	100.
Aquifer porosity	--	CONSTANT	0.400	-999.	0.100E-08	0.990
Bulk density	g/cc	CONSTANT	1.50	-999.	0.100E-01	5.00
Aquifer thickness	m	CONSTANT	12.2	-999.	0.100E-08	0.100E+06
Source thickness (mixing zone depth)	m	DERIVED	-999.	-999.	0.100E-08	0.100E+06
Conductivity (hydraulic)	m/yr	CONSTANT	100.	-999.	0.100E-06	0.100E+09
Gradient (hydraulic)		CONSTANT	0.500E-02	-999.	0.100E-07	-999.
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Temperature of aquifer	C	CONSTANT	28.0	-999.	0.000E+00	100.
pH	--	CONSTANT	7.50	-999.	0.300	14.0
Organic carbon content (fraction)		CONSTANT	0.100E-02	-999.	0.100E-05	1.00
Well distance from site	m	CONSTANT	30.0	-999.	1.00	-999.
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00

Dissolved phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Overall chemical decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Acid catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Neutral hydrolysis rate constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Base catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Reference temperature	C	CONSTANT	25.0	-999.	0.000E+00	100.
Normalized distribution coefficient	ml/g	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Distribution coefficient	--	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Biodegradation coefficient (sat. zone)	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Air diffusion coefficient	cm ² /s	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
Reference temperature for air diffusion	C	CONSTANT	25.0	-999.	0.000E+00	100.
Molecular weight	g/M	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Mole fraction of solute	--	CONSTANT	0.000E+00	-999.	0.100E-08	1.00
Vapor pressure of solute	mm Hg	CONSTANT	0.000E+00	-999.	0.000E+00	100.
Henry's law constant	atm-m ³ /M	CONSTANT	0.000E+00	-999.	0.100E-09	1.00
Overall 1st order decay sat. zone	1/yr	DERIVED	0.000E+00	0.000E+00	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00

SOURCE SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Infiltration rate	m/yr	CONSTANT	0.273E-04	-999.	0.100E-09	0.100E+11
Area of waste disposal unit	m ²	CONSTANT	0.197E+07	-999.	0.100E-01	-999.
Duration of pulse	yr	CONSTANT	200.	-999.	0.100E-08	-999.
Spread of contaminant source	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Recharge rate	m/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11
Source decay constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Initial concentration at landfill	mg/l	CONSTANT	1.00	-999.	0.000E+00	-999.
Length scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Width scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Near field dilution		DERIVED	1.00	0.000E+00	0.000E+00	1.00

AQUIFER SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Particle diameter	cm	CONSTANT	0.100E-03	-999.	0.100E-08	100.
Aquifer porosity	--	CONSTANT	0.200	-999.	0.100E-08	0.990
Bulk density	g/cc	CONSTANT	1.50	-999.	0.100E-01	5.00
Aquifer thickness	m	CONSTANT	12.2	-999.	0.100E-08	0.100E+06
Source thickness (mixing zone depth)	m	DERIVED	-999.	-999.	0.100E-08	0.100E+06
Conductivity (hydraulic)	m/yr	CONSTANT	100.	-999.	0.100E-06	0.100E+09
Gradient (hydraulic)		CONSTANT	0.500E-02	-999.	0.100E-07	-999.
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Temperature of aquifer	C	CONSTANT	28.0	-999.	0.000E+00	100.
pH	--	CONSTANT	7.50	-999.	0.300	14.0
Organic carbon content (fraction)		CONSTANT	0.100E-02	-999.	0.100E-05	1.00
Well distance from site	m	CONSTANT	30.0	-999.	1.00	-999.
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00

U. S. ENVIRONMENTAL PROTECTION AGENCY
 EXPOSURE ASSESSMENT
 MULTIMEDIA MODEL
 MULTIMED (Version 1.01, June 1991)

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Run options

AMARILLO ALTERNATE LINER DEMONSTRATION - STEADY STATE MODEL

gradient - 487 ACRES, AVG LEAKAGE
 Chemical simulated is DEFAULT CHEMICAL

Option Chosen Saturated zone model
 Run was DETERMIN
 Infiltration input by user
 Run was steady-state
 Reject runs if Y coordinate outside plume
 Do not reject runs if Z coordinate outside plume
 Gaussian source used in saturated zone model

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CHEMICAL SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Solid phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11

Dissolved phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Overall chemical decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Acid catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Neutral hydrolysis rate constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Base catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Reference temperature	C	CONSTANT	25.0	-999.	0.000E+00	100.
Normalized distribution coefficient	ml/g	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Distribution coefficient	--	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Biodegradation coefficient (sat. zone)	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Air diffusion coefficient	cm ² /s	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
Reference temperature for air diffusion	C	CONSTANT	25.0	-999.	0.000E+00	100.
Molecular weight	g/M	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Mole fraction of solute	--	CONSTANT	0.000E+00	-999.	0.100E-08	1.00
Vapor pressure of solute	mm Hg	CONSTANT	0.000E+00	-999.	0.000E+00	100.
Henry's law constant	atm-m ³ /M	CONSTANT	0.000E+00	-999.	0.100E-09	1.00
Overall 1st order decay sat. zone	1/yr	DERIVED	0.000E+00	0.000E+00	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00

SOURCE SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Infiltration rate	m/yr	CONSTANT	0.273E-04	-999.	0.100E-09	0.100E+11
Area of waste disposal unit	m ²	CONSTANT	0.197E+07	-999.	0.100E-01	-999.
Duration of pulse	yr	CONSTANT	200.	-999.	0.100E-08	-999.
Spread of contaminant source	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Recharge rate	m/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11
Source decay constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Initial concentration at landfill	mg/l	CONSTANT	1.00	-999.	0.000E+00	-999.
Length scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Width scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Near field dilution		DERIVED	1.00	0.000E+00	0.000E+00	1.00

AQUIFER SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Particle diameter	cm	CONSTANT	0.100E-03	-999.	0.100E-08	100.
Aquifer porosity	--	CONSTANT	0.400	-999.	0.100E-08	0.990
Bulk density	g/cc	CONSTANT	1.50	-999.	0.100E-01	5.00
Aquifer thickness	m	CONSTANT	12.2	-999.	0.100E-08	0.100E+06
Source thickness (mixing zone depth)	m	DERIVED	-999.	-999.	0.100E-08	0.100E+06
Conductivity (hydraulic)	m/yr	CONSTANT	100.	-999.	0.100E-06	0.100E+09
Gradient (hydraulic)		CONSTANT	0.700E-02	-999.	0.100E-07	-999.
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Temperature of aquifer	C	CONSTANT	28.0	-999.	0.000E+00	100.
pH	--	CONSTANT	7.50	-999.	0.300	14.0
Organic carbon content (fraction)		CONSTANT	0.100E-02	-999.	0.100E-05	1.00
Well distance from site	m	CONSTANT	30.0	-999.	1.00	-999.
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00

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U. S. ENVIRONMENTAL PROTECTION AGENCY
EXPOSURE ASSESSMENT
MULTIMEDIA MODEL
MULTIMED (Version 1.01, June 1991)

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Run options

AMARILLO ALTERNATE LINER DEMONSTRATION - STEADY STATE MODEL

hydraulic conductivity - 487 ACRES, AVG LEAKAGE
Chemical simulated is DEFAULT CHEMICAL

Option Chosen Saturated zone model
Run was DETERMIN
Infiltration input by user
Run was steady-state
Reject runs if Y coordinate outside plume
Do not reject runs if Z coordinate outside plume
Gaussian source used in saturated zone model

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CHEMICAL SPECIFIC VARIABLES -

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Solid phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11

Dissolved phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Overall chemical decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Acid catalyzed hydrolysis rate	L/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Neutral hydrolysis rate constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Base catalyzed hydrolysis rate	L/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Reference temperature	C	CONSTANT	25.0	-999.	0.000E+00	100.
Normalized distribution coefficient	ml/g	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Distribution coefficient	--	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Biodegradation coefficient (sat. zone)	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Air diffusion coefficient	cm ² /s	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
Reference temperature for air diffusion	C	CONSTANT	25.0	-999.	0.000E+00	100.
Molecular weight	g/M	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Mole fraction of solute	--	CONSTANT	0.000E+00	-999.	0.100E-08	1.00
Vapor pressure of solute	mm Hg	CONSTANT	0.000E+00	-999.	0.000E+00	100.
Henry's law constant	atm-m ³ /M	CONSTANT	0.000E+00	-999.	0.100E-09	1.00
Overall 1st order decay sat. zone	1/yr	DERIVED	0.000E+00	0.000E+00	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00

SOURCE SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Infiltration rate	m/yr	CONSTANT	0.273E-04	-999.	0.100E-09	0.100E+11
Area of waste disposal unit	m ²	CONSTANT	0.197E+07	-999.	0.100E-01	-999.
Duration of pulse	yr	CONSTANT	200.	-999.	0.100E-08	-999.
Spread of contaminant source	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Recharge rate	m/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11
Source decay constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Initial concentration at landfill	mg/l	CONSTANT	1.00	-999.	0.000E+00	-999.
Length scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Width scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Near field dilution		DERIVED	1.00	0.000E+00	0.000E+00	1.00

AQUIFER SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Particle diameter	cm	CONSTANT	0.100E-03	-999.	0.100E-08	100.
Aquifer porosity	--	CONSTANT	0.400	-999.	0.100E-08	0.990
Bulk density	g/cc	CONSTANT	1.50	-999.	0.100E-01	5.00
Aquifer thickness	m	CONSTANT	12.2	-999.	0.100E-08	0.100E+06
Source thickness (mixing zone depth)	m	DERIVED	-999.	-999.	0.100E-08	0.100E+06
Conductivity (hydraulic)	m/yr	CONSTANT	0.100E+04	-999.	0.100E-06	0.100E+09
Gradient (hydraulic)		CONSTANT	0.500E-02	-999.	0.100E-07	-999.
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Temperature of aquifer	C	CONSTANT	28.0	-999.	0.000E+00	100.
pH	--	CONSTANT	7.50	-999.	0.300	14.0
Organic carbon content (fraction)		CONSTANT	0.100E-02	-999.	0.100E-05	1.00
Well distance from site	m	CONSTANT	30.0	-999.	1.00	-999.
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00

U. S. ENVIRONMENTAL PROTECTION AGENCY
 EXPOSURE ASSESSMENT
 MULTIMEDIA MODEL
 MULTIMED (Version 1.01, June 1991)

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 Run options

AMARILLO ALTERNATE LINER DEMONSTRATION - STEADY STATE MODEL

300m to POC - 487 ACRES, AVG LEAKAGE
 Chemical simulated is DEFAULT CHEMICAL

Option Chosen Saturated zone model
 Run was DETERMIN
 Infiltration input by user
 Run was steady-state
 Reject runs if Y coordinate outside plume
 Do not reject runs if Z coordinate outside plume
 Gaussian source used in saturated zone model

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CHEMICAL SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Solid phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11

Dissolved phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Overall chemical decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Acid catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Neutral hydrolysis rate constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Base catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Reference temperature	C	CONSTANT	25.0	-999.	0.000E+00	100.
Normalized distribution coefficient	ml/g	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Distribution coefficient	--	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Biodegradation coefficient (sat. zone)	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Air diffusion coefficient	cm ² /s	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
Reference temperature for air diffusion	C	CONSTANT	25.0	-999.	0.000E+00	100.
Molecular weight	g/M	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Mole fraction of solute	--	CONSTANT	0.000E+00	-999.	0.100E-08	1.00
Vapor pressure of solute	mm Hg	CONSTANT	0.000E+00	-999.	0.000E+00	100.
Henry's law constant	atm-m ³ /M	CONSTANT	0.000E+00	-999.	0.100E-09	1.00
Overall 1st order decay sat. zone	1/yr	DERIVED	0.000E+00	0.000E+00	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00

SOURCE SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Infiltration rate	m/yr	CONSTANT	0.273E-04	-999.	0.100E-09	0.100E+11
Area of waste disposal unit	m ²	CONSTANT	0.197E+07	-999.	0.100E-01	-999.
Duration of pulse	yr	CONSTANT	200.	-999.	0.100E-08	-999.
Spread of contaminant source	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Recharge rate	m/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11
Source decay constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Initial concentration at landfill	mg/l	CONSTANT	1.00	-999.	0.000E+00	-999.
Length scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Width scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Near field dilution		DERIVED	1.00	0.000E+00	0.000E+00	1.00

AQUIFER SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Particle diameter	cm	CONSTANT	0.100E-03	-999.	0.100E-08	100.
Aquifer porosity	--	CONSTANT	0.400	-999.	0.100E-08	0.990
Bulk density	g/cc	CONSTANT	1.50	-999.	0.100E-01	5.00
Aquifer thickness	m	CONSTANT	12.2	-999.	0.100E-08	0.100E+06
Source thickness (mixing zone depth)	m	DERIVED	-999.	-999.	0.100E-08	0.100E+06
Conductivity (hydraulic)	m/yr	CONSTANT	100.	-999.	0.100E-06	0.100E+09
Gradient (hydraulic)		CONSTANT	0.500E-02	-999.	0.100E-07	-999.
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Temperature of aquifer	C	CONSTANT	28.0	-999.	0.000E+00	100.
pH	--	CONSTANT	7.50	-999.	0.300	14.0
Organic carbon content (fraction)		CONSTANT	0.100E-02	-999.	0.100E-05	1.00
Well distance from site	m	CONSTANT	300.	-999.	1.00	-999.
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00

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NO	NAME	UNIT	VALUE
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U. S. ENVIRONMENTAL PROTECTION AGENCY
 EXPOSURE ASSESSMENT
 MULTIMEDIA MODEL
 MULTIMED (Version 1.01, June 1991)

1
 Run options

 AMARILLO ALTERNATE LINER DEMONSTRATION - STEADY STATE MODEL

12m mixing zone - 487 ACRES, AVG LEAKAGE
 Chemical simulated is DEFAULT CHEMICAL
 Option Chosen 1 Saturated zone model
 Run was 0 DETERMIN.
 Infiltration input by user
 Run was steady-state
 Reject runs if Y coordinate outside plume
 Do not reject runs if Z coordinate outside plume
 Gaussian source used in saturated zone model

1
 1
 CHEMICAL SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Solid phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11

Dissolved phase decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Overall chemical decay coefficient	1/yr	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Acid catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Neutral hydrolysis rate constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Base catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Reference temperature	C	CONSTANT	25.0	-999.	0.000E+00	100.
Normalized distribution coefficient	ml/g	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Distribution coefficient	--	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Biodegradation coefficient (sat. zone)	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Air diffusion coefficient	cm ² /s	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
Reference temperature for air diffusion	C	CONSTANT	25.0	-999.	0.000E+00	100.
Molecular weight	g/M	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Mole fraction of solute	--	CONSTANT	0.000E+00	-999.	0.100E-08	1.00
Vapor pressure of solute	mm Hg	CONSTANT	0.000E+00	-999.	0.000E+00	100.
Henry's law constant	atm-m ³ /M	CONSTANT	0.000E+00	-999.	0.100E-09	1.00
Overall 1st order decay sat. zone	1/yr	DERIVED	0.000E+00	0.000E+00	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00

SOURCE SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Infiltration rate	m/yr	CONSTANT	0.273E-04	-999.	0.100E-09	0.100E+11
Area of waste disposal unit	m ²	CONSTANT	0.197E+07	-999.	0.100E-01	-999.
Duration of pulse	yr	CONSTANT	200.	-999.	0.100E-08	-999.
Spread of contaminant source	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Recharge rate	m/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11
Source decay constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Initial concentration at landfill	mg/l	CONSTANT	1.00	-999.	0.000E+00	-999.
Length scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Width scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Near field dilution		DERIVED	1.00E-04	0.000E+00	0.000E+00	1.00

AQUIFER SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Particle diameter	cm	CONSTANT	0.100E-03	-999.	0.100E-08	100.
Aquifer porosity	--	CONSTANT	0.400	-999.	0.100E-08	0.990
Bulk density	g/cc	CONSTANT	1.50	-999.	0.100E-01	5.00
Aquifer thickness	m	CONSTANT	12.2	-999.	0.100E-08	0.100E+06
Source thickness (mixing zone depth)	m	CONSTANT	12.2	-999.	0.100E-08	0.100E+06
Conductivity (hydraulic)	m/yr	CONSTANT	100.	-999.	0.100E-06	0.100E+09
Gradient (hydraulic)		CONSTANT	0.500E-02	-999.	0.100E-07	-999.
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Temperature of aquifer	C	CONSTANT	28.0	-999.	0.000E+00	100.
pH	--	CONSTANT	7.50	-999.	0.300	14.0
Organic carbon content (fraction)		CONSTANT	0.100E-02	-999.	0.100E-05	1.00
Well distance from site	m	CONSTANT	30.0	-999.	1.00	-999.
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00

APPENDIX 4B

2005 Updated Slope Stability Analysis and Liner System Design
Monitoring Well Groundwater Elevation Summary

Prepared By: DRW
Date: 12/15/05

City of Amarillo Landfill
Slope Stability Analysis

Checked By: UMS
Date: 12-15-05

**City of Amarillo Landfill
Potter County, Texas
Slope Stability Analysis**

Determine that the landfill slopes are theoretically stable with an acceptable factor of safety.

Procedures:

1. Verify slope stability for landfill excavation.
2. Verify liner system design by determining tensile stresses in the liner elements, verify liner system stability using infinite slope analysis, and verify anchor trench design.
3. Determine factor of safety for the interim fill slope.
4. Using a critical slope configuration for the final slope, calculate the final slope stability factor of safety.

The landfill excavation slope was analyzed in the previous permit documents. The previous analysis remains valid, and no technical issues have varied since that determination. Excavation slopes within the natural soils have been made and are stable during construction and subsequent landfill operations.

**City of Amarillo Landfill
Potter County, Texas
Interim Slope Stability Analysis**

Procedure:

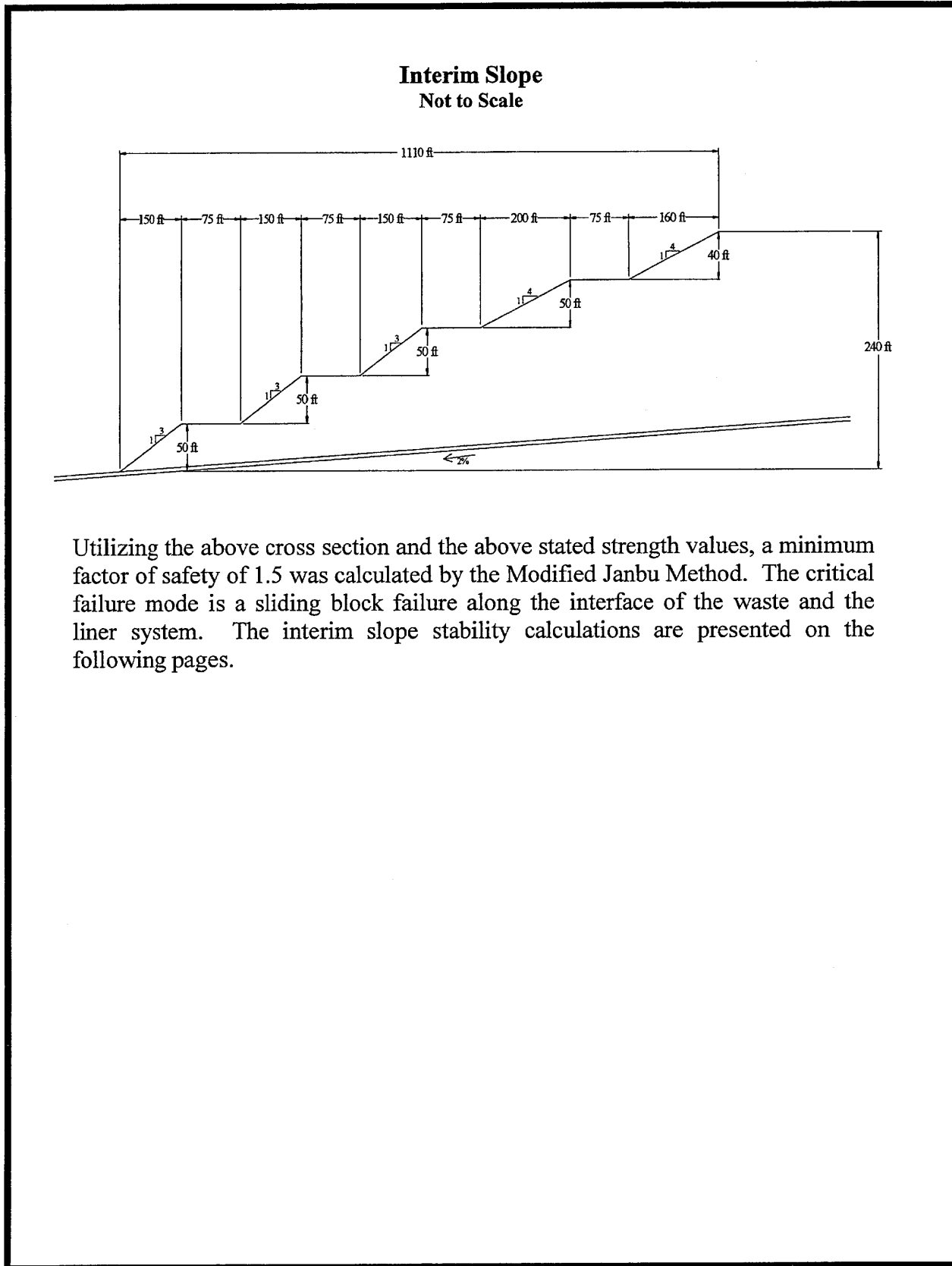
The interim solid waste fill slope has been analyzed using the computer code PCSTABL, University of Wisconsin-Madison and Purdue University. The computer modeling has utilized a wedge type failure that calculates slippage along the surface of the liner system as waste is placed and compacted within the landfill. The critical failure mode during waste deposition occurs along one of the liner elements where the interim waste fill can be limited to maintain an acceptable interim slope stability factor of safety.

The soil strength and properties used for the analysis are as follows:

Material	Unit Weight, pcf	Cohesion, psf	Friction Angle, degrees
Waste ⁽¹⁾	70	400	20
Liner ⁽²⁾	125	100	10
Natural Soil	125	1000	30

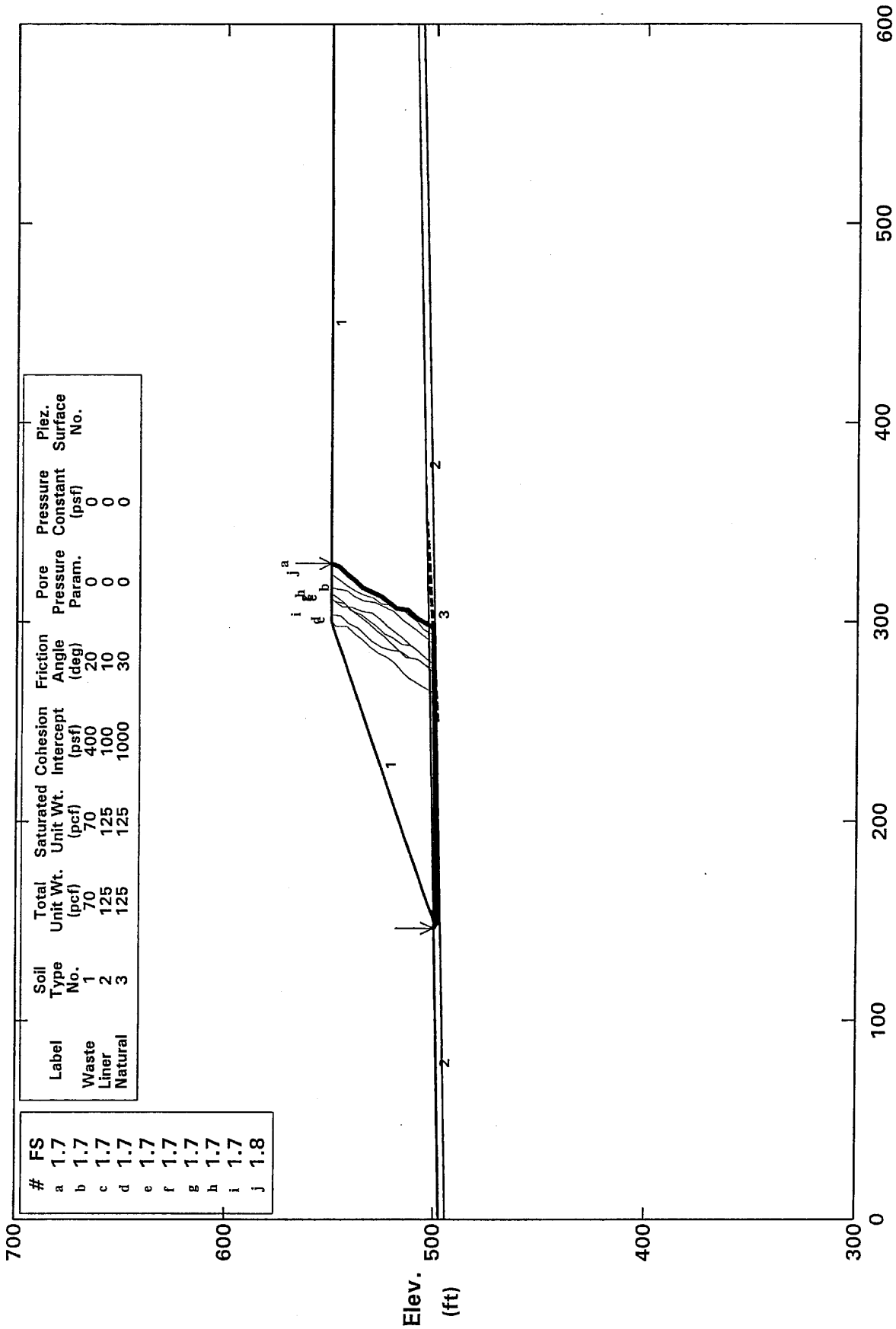
- (1) Solid waste shear strength selected to be conservative.
- (2) The critical interface layer within the liner system is between the geomembrane and geosynthetic clay layers. This critical interface provides the lower strength values of the liner system for the stability analysis. Bottom membrane to be textured 60 mil HDPE and the selected liner shear values as modeled are considered to be conservative, that is, interface values are probably greater than values modeled.

The interim slope stability calculations have utilized waste slopes on five benches within the 240-foot waste height. Each bench is 75 feet wide. The following figure shows the cross section of the interim slope used in calculations.



Utilizing the above cross section and the above stated strength values, a minimum factor of safety of 1.5 was calculated by the Modified Janbu Method. The critical failure mode is a sliding block failure along the interface of the waste and the liner system. The interim slope stability calculations are presented on the following pages.

57815-City of Amarillo Landfill, Interim Slope with 50' Height
 Ten Most Critical. U:INT50.PLT By: PRW 07-01-05 2:36pm

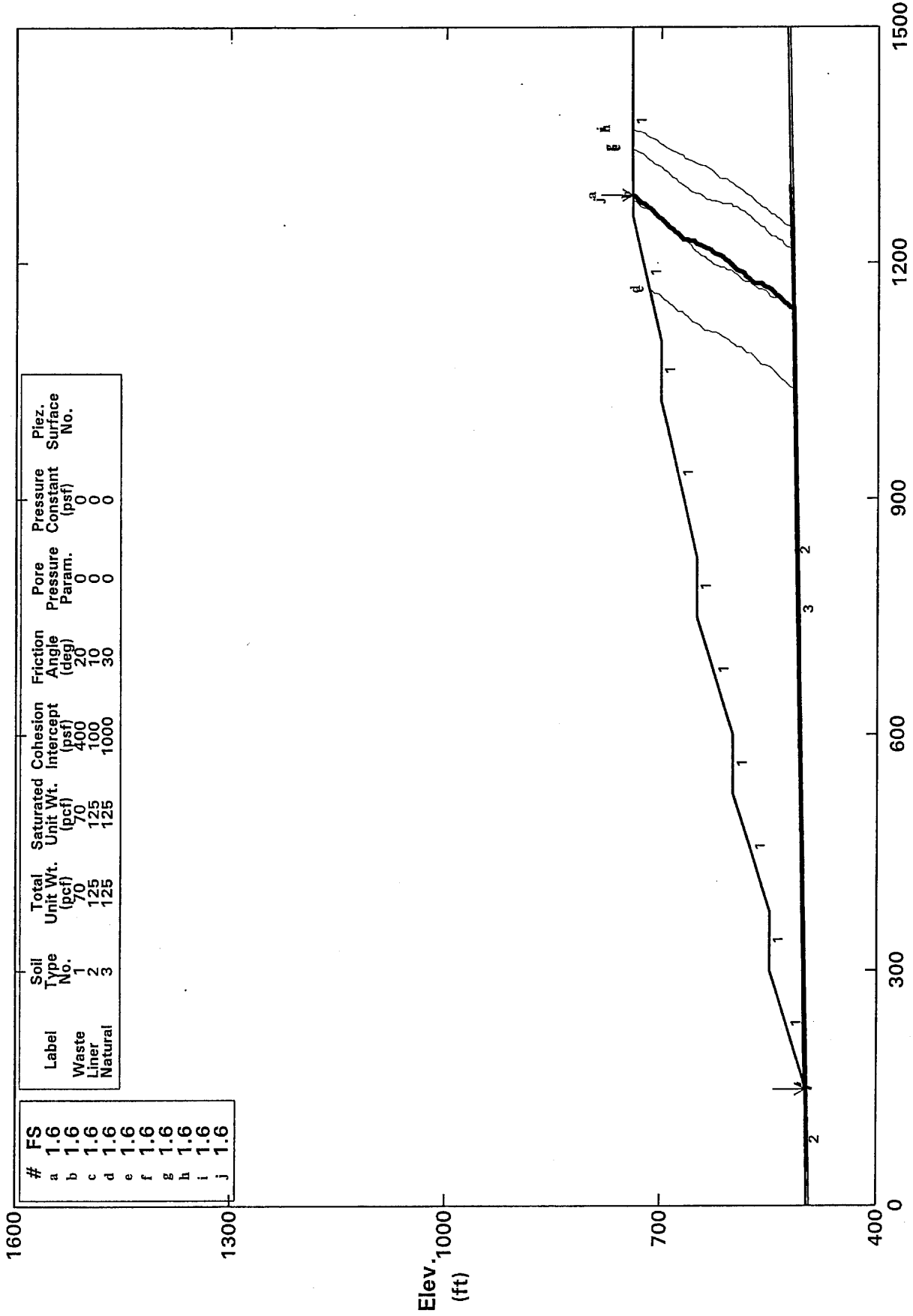


Label	Soil Type No.	Total Unit Wt. (pcf)	Saturated Unit Wt. (pcf)	Cohesion Intercept (psf)	Friction Angle (deg)	Pore Pressure Param. (psf)	Pressure Constant (psf)	Piez. Surface No.
Waste	1	70	70	400	20	0	0	
Liner	2	125	125	100	10	0	0	
Natural	3	125	125	1000	30	0	0	

#	FS
a	1.7
b	1.7
c	1.7
d	1.7
e	1.7
f	1.7
g	1.7
h	1.7
i	1.7
j	1.8

PCSTABL5M/SI FSmin = 1.7 X-Axis (ft)
 Factors Of Safety Calculated By The Modified Janbu Method

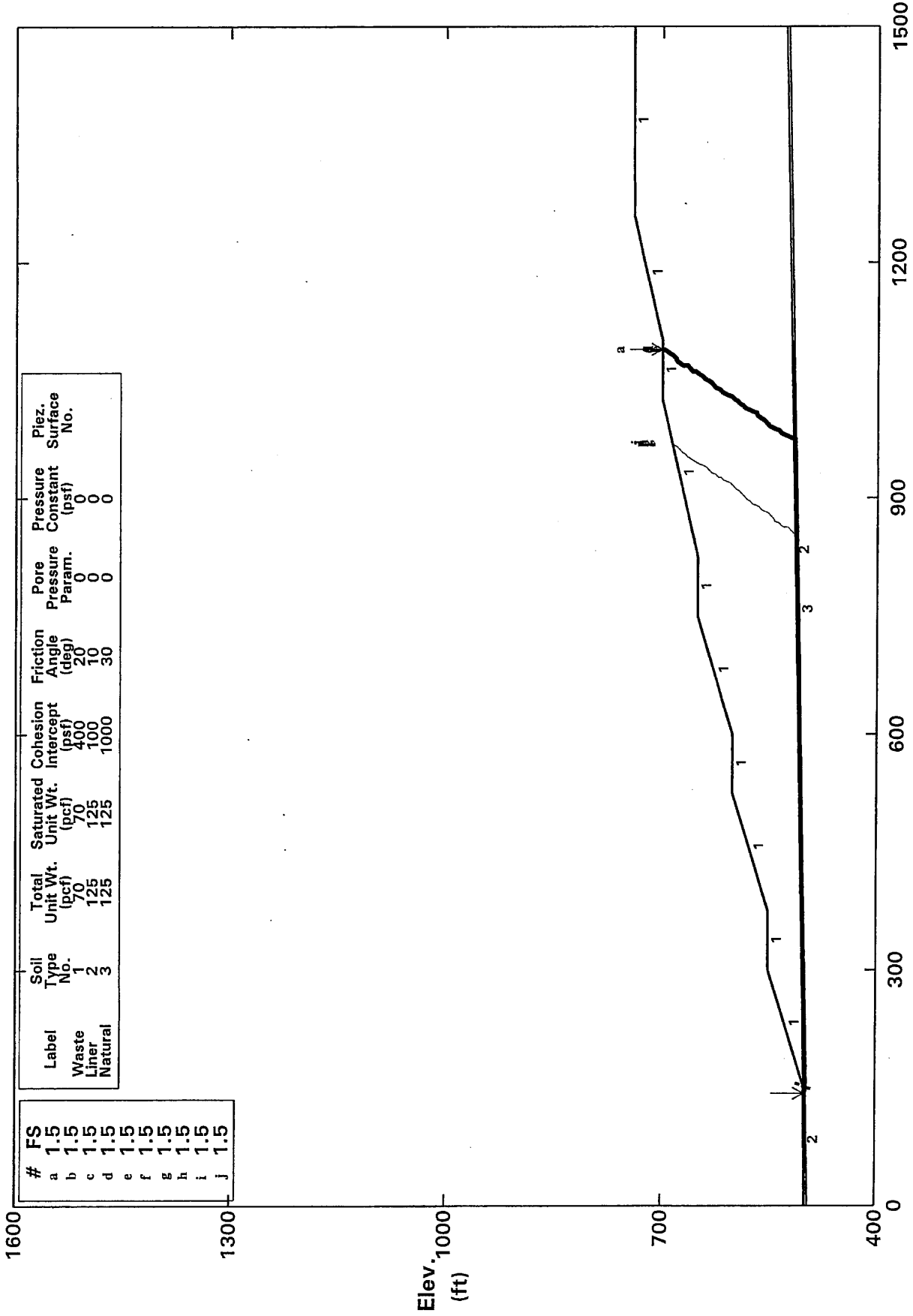
57815-City of Amarillo Landfill, Interim Slope, Benched
 Ten Most Critical. U:INTERIM.PLT By: PRW 07-13-05 3:26pm



Label	Soil Type No.	Total Unit Wt. (pcf)	Saturated Unit Wt. (pcf)	Cohesion Intercept (psf)	Friction Angle (deg)	Pore Pressure Param.	Pressure Constant (psf)	Piez. Surface No.
Waste	1	70	70	400	20	0	0	
Liner	2	125	125	100	10	0	0	
Natural	3	125	125	1000	30	0	0	

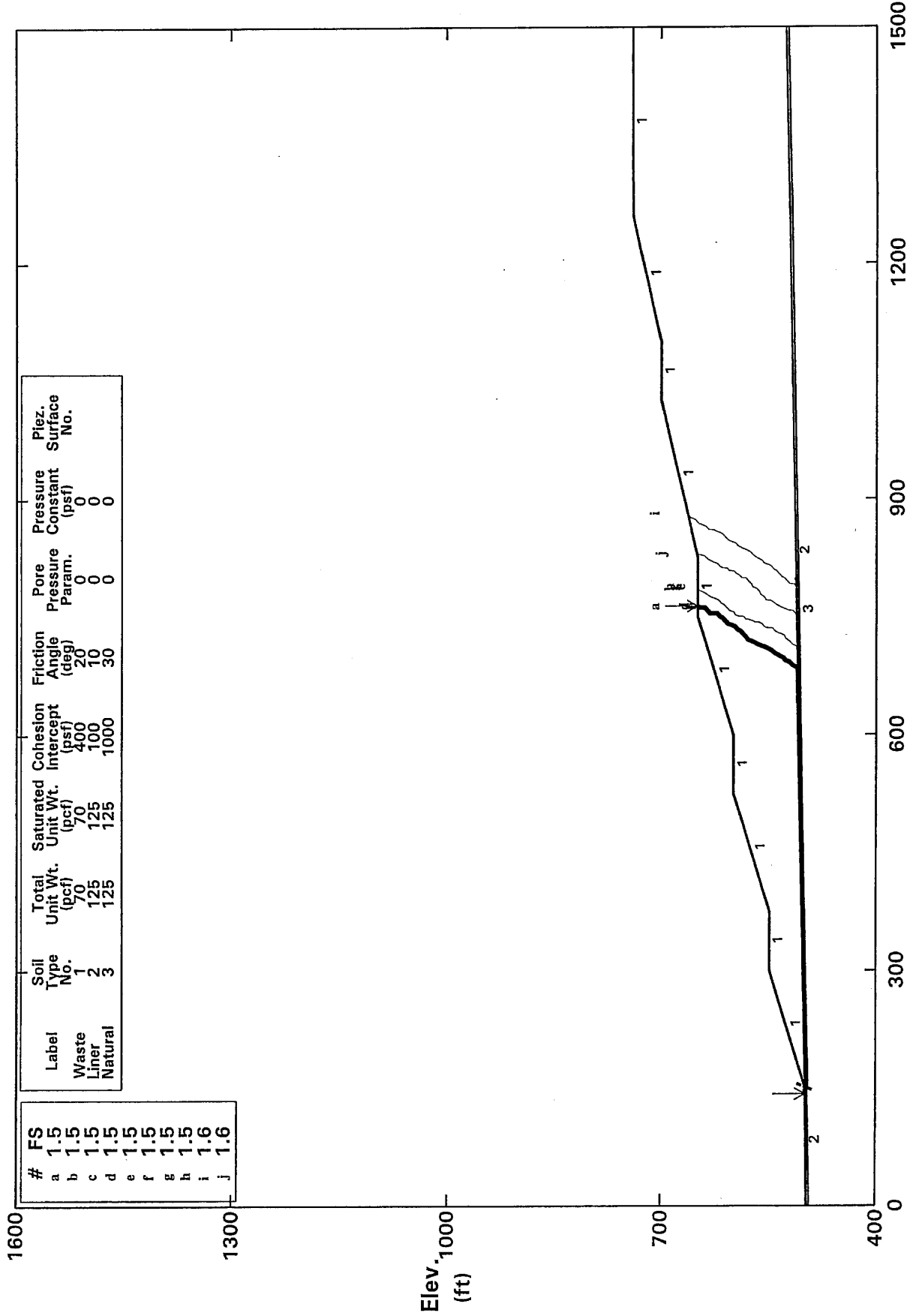
PCSTABL5M/SI FSmin = 1.6 X-Axis (ft)
 Factors Of Safety Calculated By The Modified Janbu Method

57815-City of Amarillo Landfill, Interim Slope, Benched
 Ten Most Critical. U:INTERIM2.PLT By: PRW 07-13-05 3:30pm



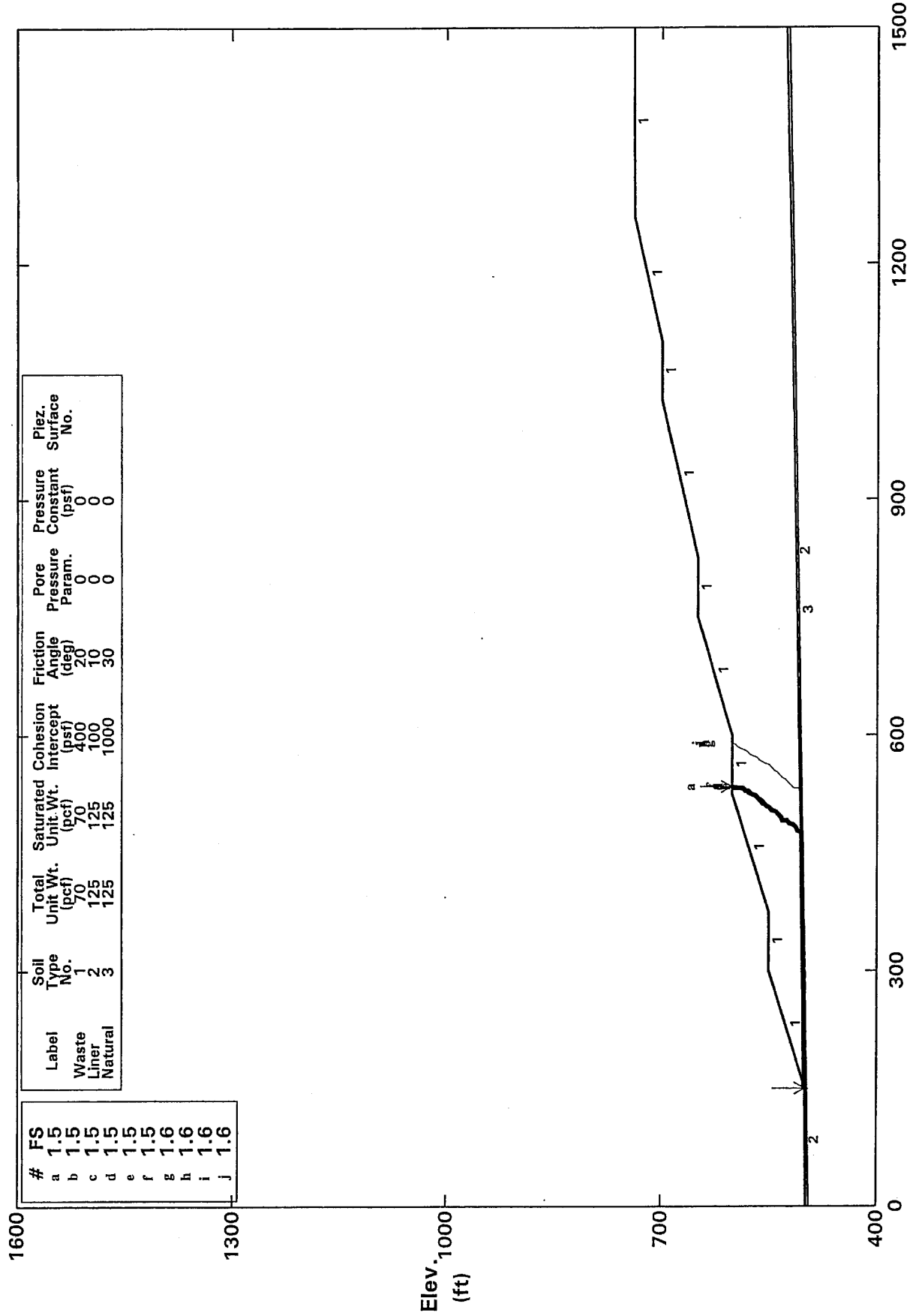
PCSTABL5M/SI FSmin = 1.5 X-Axis (ft)
 Factors Of Safety Calculated By The Modified Janbu Method

57815-City of Amarillo Landfill, Interim Slope, Benched
 Ten Most Critical. U:INTERIM3.PLT By: PRW 07-13-05 3:42pm



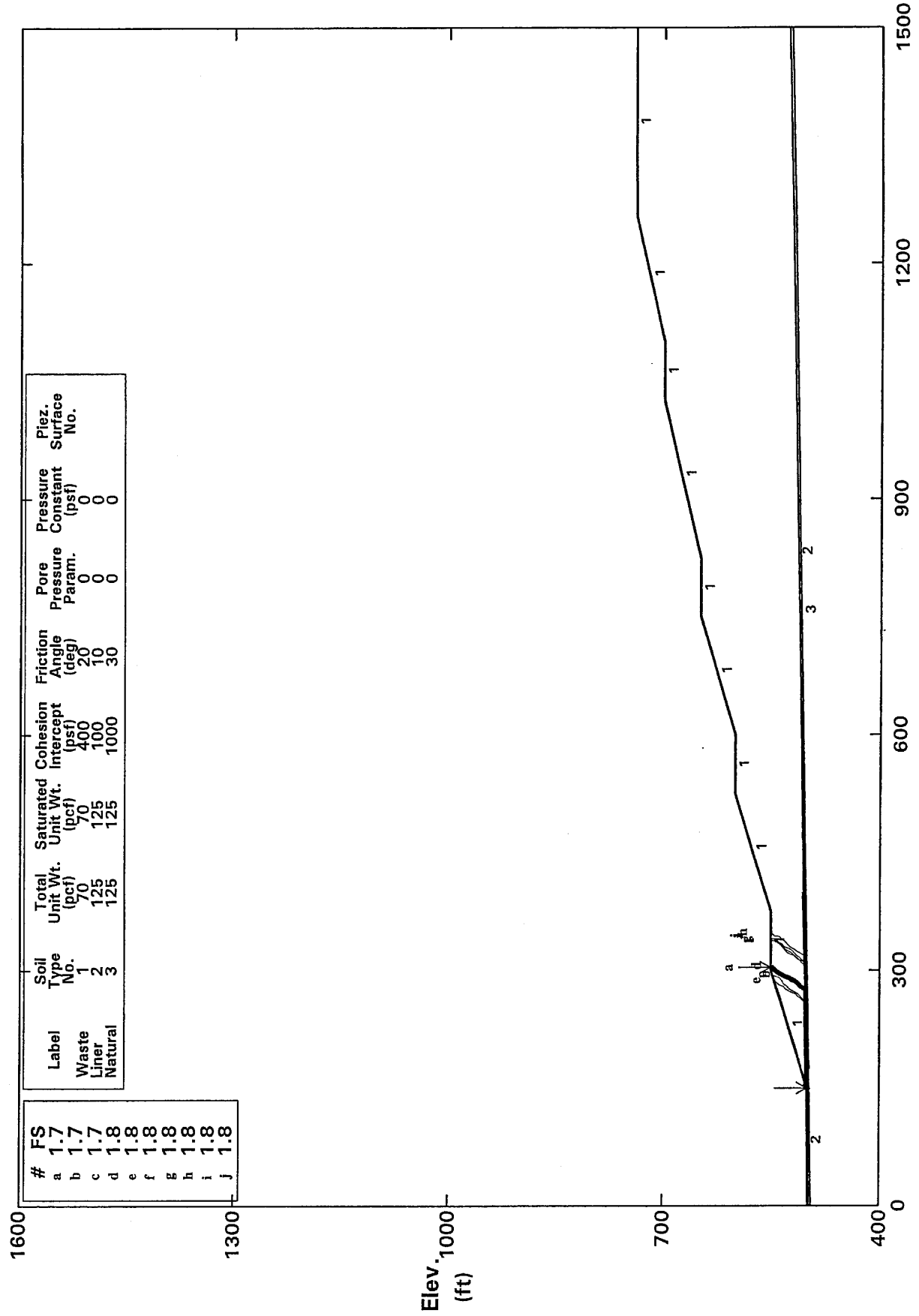
PCSTABL5M/SI FSmin = 1.5 X-Axis (ft)
 Factors Of Safety Calculated By The Modified Janbu Method

57815-City of Amarillo Landfill, Interim Slope, Benched
 Ten Most Critical. U:INTERIM4.PLT By: PRW 07-13-05 3:43pm



PCSTABL5M/SI FSmin = 1.5 X-Axis (ft)
 Factors Of Safety Calculated By The Modified Janbu Method

57815-City of Amarillo Landfill, Interim Slope, Benched
 Ten Most Critical. U:INTERIM5.PLT By: PRW 07-13-05 3:44pm



PCSTABL5M/SI FSmin = 1.7 X-Axis (ft)

Factors Of Safety Calculated By The Modified Janbu Method

**City of Amarillo Landfill
Potter County, Texas
Final Slope Stability Analysis**

Procedure:

The critical or the highest slope will occur along the western edge of the landfill. The waste will be filled to the top of the excavated area, which is about 70 feet deep, then will be placed on a 4H:1V slope up to the crest for a total waste thickness of 240 feet on the western side of the landfill.

The soil strength and properties used for the analysis are as follows:

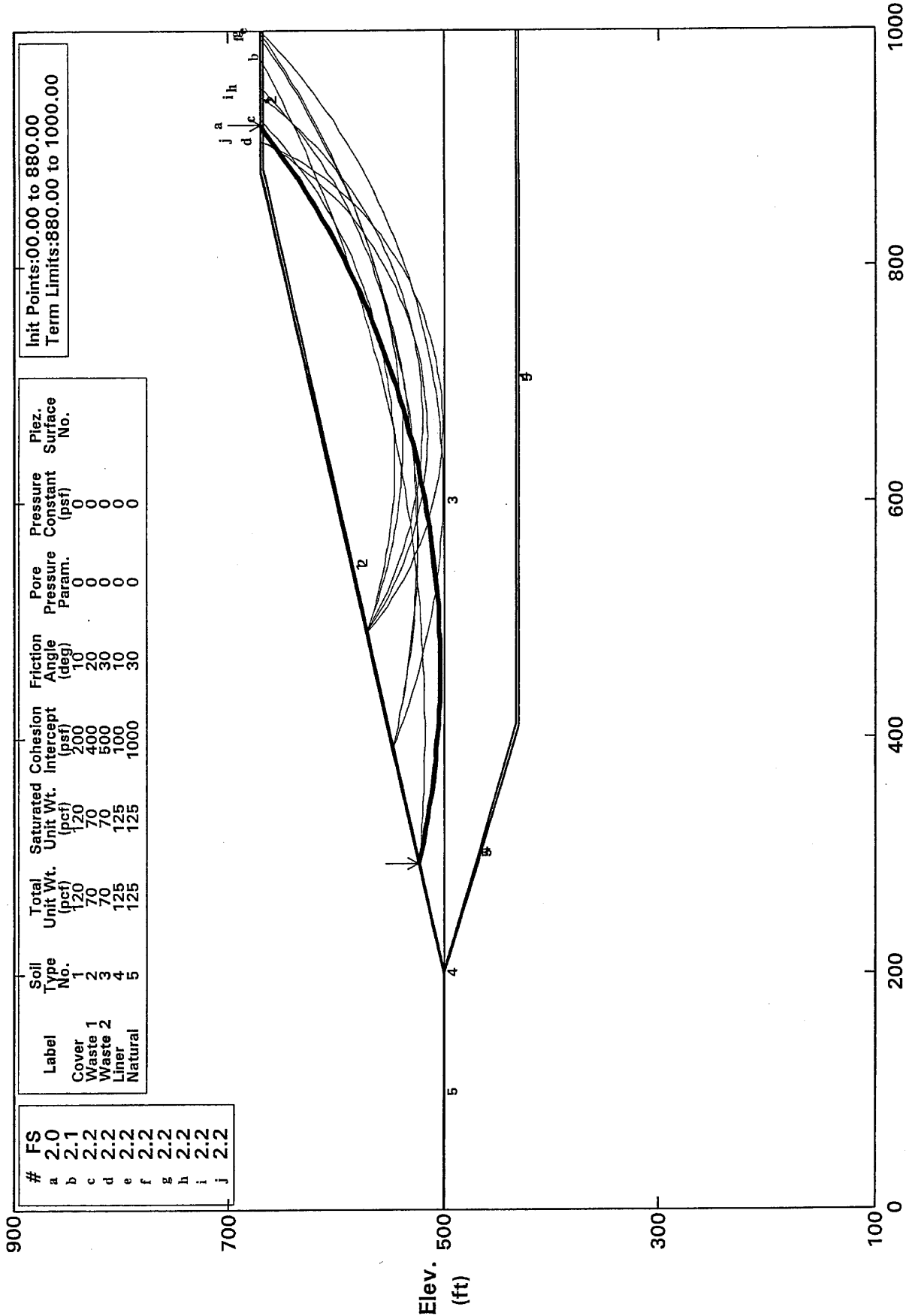
Material	Unit Weight, pcf	Cohesion, psf	Friction Angle, degrees
Final Cover	120	200	10
Solid Waste, upper	70	400	20
Solid Waste, lower	70	500	30
Liner	125	100	10
Natural Soil	125	1000	30

For the solid waste placed first (Cells 1-3), at elevations below the top of the excavated area (natural grade), the waste will have gained additional strength due to the length of time the waste has been in place and the weight of the overlying waste having continued to compress the underlying waste layer. This strengthening influence has been modeled by slightly increasing the strength of the solid waste in the lower lifts as shown in the table, above.

A circular failure surface has been calculated. Based on the calculation, the resulting final slope factor of safety meets or exceeds acceptable values. The following plate shows the calculated factor of safety.

57815-Amarillo Landfill Final Slope

Ten Most Critical. U:FINAL1.PLT By: PRW 07-01-05 2:57pm



PCSTABL5M/SI FSmin = 2.0 X-Axis (ft)

Factors Of Safety Calculated By The Modified Janbu Method

**City of Amarillo Landfill
Potter County, Texas
Excavation Slope Stability Analysis**

Procedure:

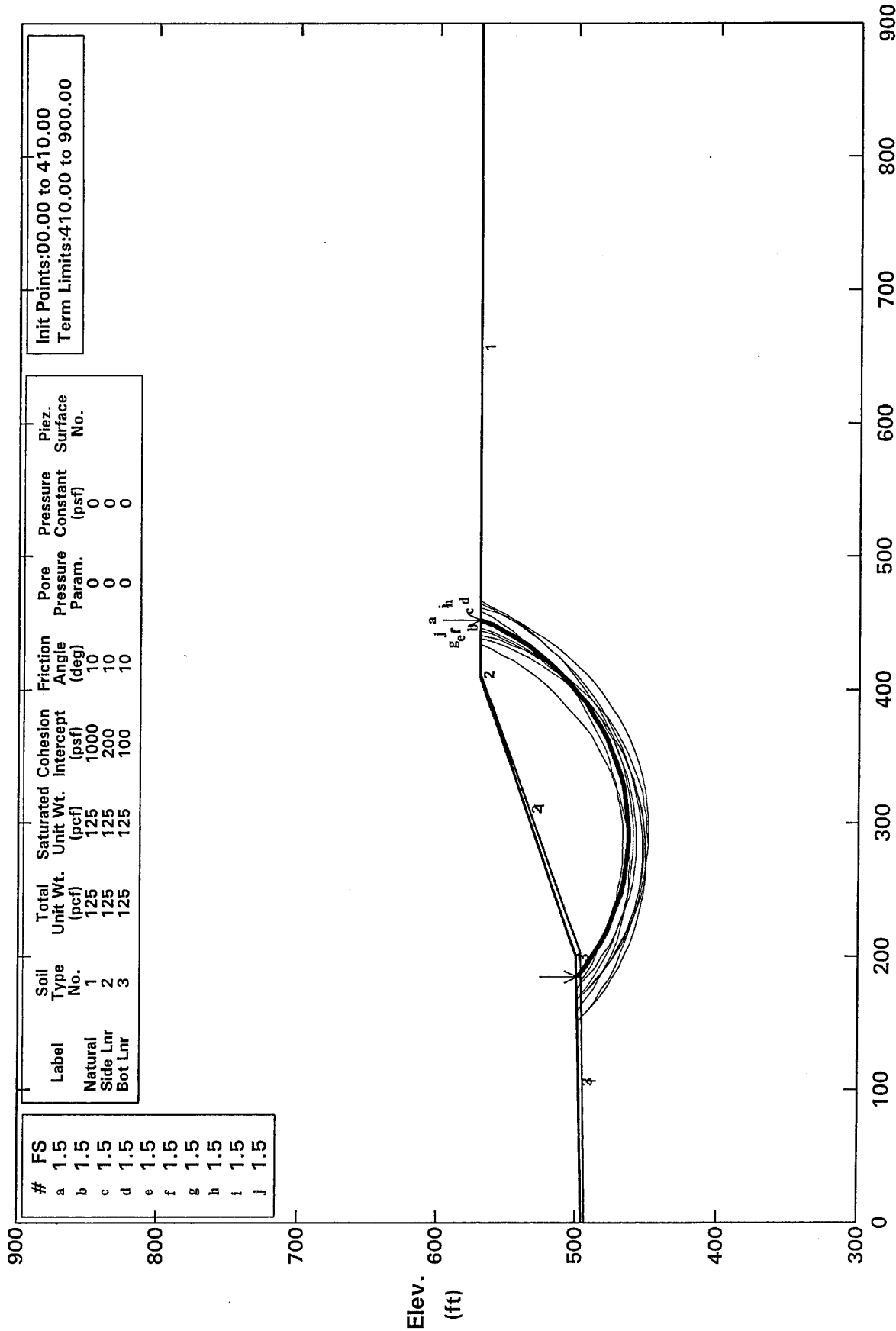
The excavated area is 70 feet deep with side slopes of 3H:1V. A slope stability analysis was completed for the 1994 permit modifications. Since the excavation has been opened, the soils may have changed shear strength values due to drying. Typically, the apparent cohesion decreases and the apparent friction angle increases with time for an effective stress analysis. The excavation slope has been reviewed with slightly altered shear strength values as a check on effective stress. The soil strength and properties used for this analysis are as follows:

Material	Unit Weight, pcf	Cohesion, psf	Friction Angle, degrees
Natural Soil	125	1000	10
Side Slope Liner	125	200	10
Bottom Liner	125	100	10

A circular failure surface has been calculated. Based on the calculation, the resulting excavation slope factor of safety is 1.5. The following plate shows the calculated factor of safety.

57815-Excavation Slope

Ten Most Critical. U:EXCCLP.PLT By: PRW 07-13-05 3:48pm



PCSTABL5M/SI FSmin = 1.5 X-Axis (ft)

Factors Of Safety Calculated By The Modified Janbu Method

City of Amarillo Landfill Potter County, Texas Liner System Design

Procedure:

1. Verify tensile stresses in the liner system with geocomposite (geonet/geotextile), over textured 60 mil HDPE geomembrane, over geosynthetic clay liner (GCL) by calculating shear forces in the liner system.
2. Verify liner system stability using infinite slope stability analysis. (Ref. 1, 3, and 4)
3. Verify final cover system using infinite slope stability.
4. Verify anchor trench design for pull-out of liner system components. (Ref 2, 3, and 4)

Calculations:

1. Tensile Forces of Liner System

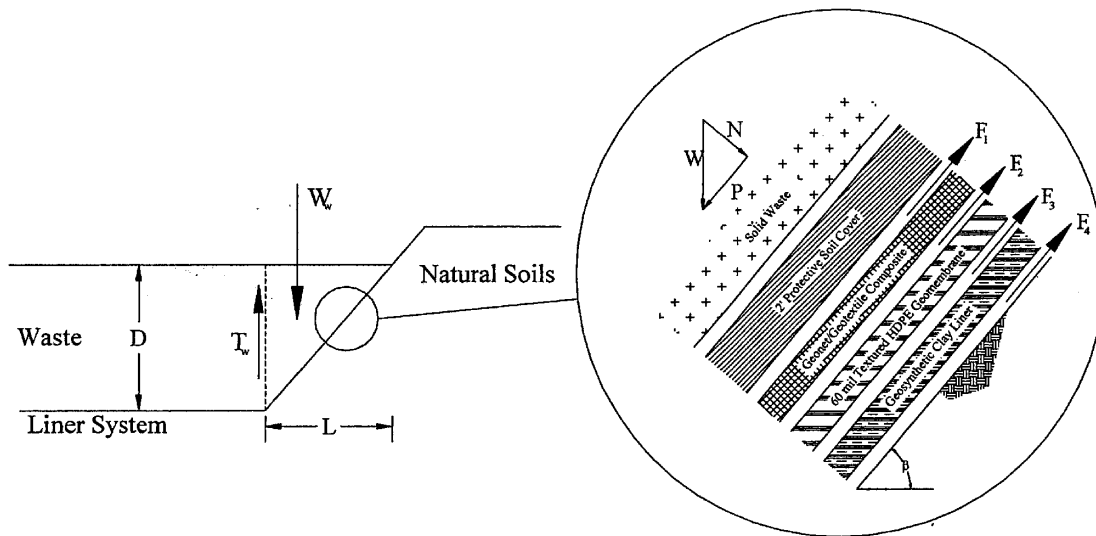


Figure 1

Definitions of terms and variables:

- W_w = Weight of solid waste
 T_w = Friction force on edge of waste
 β = Slope angle
 W = Net force of waste on liner system
 N = $W \cos \beta$ = Normal force on liner system
 P = $W \sin \beta$ = Shearing force on liner system
- F_1 = $N \tan A_1 + C_1(L/\cos \beta)$
 F_2 = $N \tan A_2 + C_2(L/\cos \beta)$
 F_3 = $N \tan A_3 + C_3(L/\cos \beta)$
 F_4 = $N \tan A_4 + C_4(L/\cos \beta)$
- A_1 = Interface friction angle between protective soil cover and geonet/geotextile composite
 C_1 = Cohesion/adhesion intercept between protective soil cover and geonet/geotextile composite
 A_2 = Interface friction angle between geonet/geotextile composite and 60-mil HDPE geomembrane (textured)
 C_2 = Cohesion/adhesion intercept between geonet/geotextile composite and 60 mil HDPE geomembrane (textured)
 A_3 = Interface friction angle between 60 mil HDPE geomembrane (textured) and geosynthetic clay liner
 C_3 = Cohesion/adhesion intercept between 60 mil HDPE geomembrane (textured) and geosynthetic clay liner
 A_4 = Interface friction angle between geosynthetic clay liner and natural ground
 C_4 = Cohesion/adhesion intercept between geosynthetic clay liner and natural subgrade
 D = Individual waste lift height
 L = Horizontal length of solid waste lift along slope
 γ_{waste} = Unit weight of solid waste
 ϕ_{waste} = Internal friction angle of solid waste

Parameters:

$A_1 = 10^\circ$	$A_3 = 12^\circ$	$D = 20 \text{ ft}$
$C_1 = 200 \text{ psf}$	$C_3 = 200 \text{ psf}$	$\beta = 18.43^\circ \text{ (3:1 slope)}$
$A_2 = 15^\circ$	$A_4 = 20^\circ$	$L = 60 \text{ feet (3:1 slope)}$
$C_2 = 200 \text{ psf}$	$C_4 = 150 \text{ psf}$	$\gamma_{\text{waste}} = \frac{(40_i + 70_f)}{2} = 55 \text{ pcf}$
		$\phi_{\text{waste}} = 20^\circ$
		$c_{\text{waste}} = 400 \text{ psf}$

Calculate:

Weight of solid waste for 20-foot lift placed along a 3:1 slope

$$W_w = \frac{DL\gamma_{\text{waste}}}{2} \quad \text{(See Figure 1)}$$

$$W_w = \frac{(20')(60')(55 \text{ pcf})}{2}$$

$$W_w = 33,000 \text{ lb/ft}$$

Friction force on edge of waste

$$T_w = k_o \sigma_v \tan \phi_{\text{waste}} D \quad \text{(See Figure 1)}$$

where $k_o = 1 - \sin \phi_{\text{waste}} = 0.66$

$$\sigma_v = \frac{D\gamma_{\text{waste}}}{2} = \frac{(20')(55 \text{ pcf})}{2} = 550 \text{ psf}$$

$$T_w = (0.66)(550 \text{ psf})(\tan 20^\circ)(20')$$

$$T_w = 2,642 \text{ lb/ft}$$

Net force of waste on liner system

$$W = W_w - T_w$$

$$W = 33,000 - 2,642 = 30,358 \text{ lb/ft}$$

$$N = W \cos \beta = 30,358 \cos 18.43^\circ = 28,800 \text{ lb/ft}$$

$$P = W \sin \beta = 30,358 \sin 18.43^\circ = 9,598 \text{ lb/ft}$$

Resistance of protective soil cover and geonet/geotextile composite interface

$$F_1 = N \tan A_1 + C_1 \left(\frac{L}{\cos \beta} \right)$$

$$F_1 = 28,800(\tan 10^\circ) + 200 \left(\frac{60}{\cos 18.43^\circ} \right)$$

$$F_1 = 5,078 + 12,648$$

$$F_1 = 17,726 \text{ lb/ft}$$

$P < F_1$, therefore the protective soil cover is stable on the geocomposite

Resistance of geocomposite and 60 mil HDPE (textured) geomembrane interface

$$F_2 = N \tan A_2 + C_2 \left(\frac{L}{\cos \beta} \right)$$

$$F_2 = 28,800(\tan 15^\circ) + 200 \left(\frac{60}{\cos 18.43^\circ} \right)$$

$$F_2 = 7,716 + 12,649$$

$$F_2 = 20,365 \text{ lb/ft}$$

$P < F_2$, therefore the geocomposite is stable on the geomembrane

Resistance of 60-mil HDPE (textured) geomembrane and geosynthetic clay liner (GCL) interface

$$F_3 = N \tan A_3 + C_3 \left(\frac{L}{\cos \beta} \right)$$

$$F_3 = 28,800(\tan 12^\circ) + 200 \left(\frac{60}{\cos 18.43^\circ} \right)$$

$$F_3 = 6,121 + 12,649$$

$$F_3 = 18,770 \text{ lb/ft}$$

$P < F_3$, therefore the geomembrane is stable on the GCL

Resistance of GCL and natural subgrade interface

$$F_4 = N \tan A_4 + C_4 \left(\frac{L}{\cos \beta} \right)$$

$$F_4 = 28,800(\tan 20^\circ) + 150 \left(\frac{60}{\cos 18.43^\circ} \right)$$

$$F_4 = 10,482 + 9,486$$

$$F_4 = 19,968 \text{ lb/ft}$$

$P < F_4$, therefore the GCL is stable on the natural subgrade

Therefore, the individual liner components are not subjected to any external forces caused by the shearing of the waste placed over the liner system.

Normal Stress on Liner (bottom liner system)

$$\sigma_n = \gamma_{waste} H_{waste}$$

Where: $H_{waste} = 240$ feet (maximum depth)
 $\gamma_{waste} = 70$ pcf

$$\sigma_n = (70 \text{ pcf})(240 \text{ ft})$$
$$\sigma_n = 16,800 \text{ psf}$$

The geocomposite layer is the critical layer because water must flow through the geocomposite to the leachate collection system.

Geocomposite normal pressure = 20,000+ psf

$$FS = \frac{20,000}{16,800} = 1.2$$

- Cohesion neglected along waste thickness (D) for conservative calculation.
- The maximum uncompacted waste lift depth placed against the sidewall liner is 20 feet. The liner calculations have considered as much as 20 feet of waste placed and compacted along the sloping liner system, resulting in a severe loading condition and conservative FS calculations for the liner components.
- Factors used in the calculations have been made from referenced publications and previous experience.

2. Infinite Slope Analysis of Liner System

$$FS = A \frac{\tan \phi}{\tan \beta} + B \frac{c}{\gamma H} \quad (\text{Ref. 3})$$

Protective soil cover and geocomposite interface

$$\begin{aligned} \phi &= 10^\circ \\ c &= 200 \text{ psf} \\ \beta &= 18.43^\circ \\ A &= 0.45 && (\text{see attached charts, Ref. 3}) \\ B &= 3.3 && (\text{see attached charts, Ref. 3}) \\ \gamma &= 120 \text{ pcf} \\ H &= 2 \text{ feet} \end{aligned}$$

$$FS = 0.45 \left(\frac{\tan 10^\circ}{\tan 18.43^\circ} \right) + 3.3 \left[\frac{200}{(120)(2)} \right]$$
$$FS = 2.9$$

Geocomposite and 60-mil HDPE geomembrane (textured) interface

$$\begin{aligned} \phi &= 15^\circ \\ c &= 200 \text{ psf} \\ \beta &= 18.43^\circ \\ A &= 0.45 && (\text{see attached charts, Ref. 3}) \\ B &= 3.3 && (\text{see attached charts, Ref. 3}) \\ \gamma &= 120 \text{ pcf} \\ H &= 2 \text{ feet} \end{aligned}$$

$$FS = 0.45 \left(\frac{\tan 15^\circ}{\tan 18.43^\circ} \right) + 3.3 \left[\frac{200}{(120)(2)} \right]$$
$$FS = 3.1$$

60 mil HDPE geomembrane (textured) and GCL interface

ϕ	= 12°	
c	= 200 psf	
β	= 18.43°	
A	= 0.45	(see attached charts, Ref. 3)
B	= 3.3	(see attached charts, Ref. 3)
γ	= 120 pcf	
H	= 2 feet	

$$FS = 0.45 \left(\frac{\tan 12^\circ}{\tan 18.43^\circ} \right) + 3.3 \left[\frac{200}{(120)(2)} \right]$$
$$FS = 3.0$$

GCL and natural soil interface

ϕ	= 20°	
c	= 150 psf	
β	= 18.43°	
A	= 0.45	(see attached charts, Ref. 3)
B	= 3.3	(see attached charts, Ref. 3)
γ	= 120 pcf	
H	= 2 feet	

$$FS = 0.45 \left(\frac{\tan 20^\circ}{\tan 18.43^\circ} \right) + 3.3 \left[\frac{150}{(120)(2)} \right]$$
$$FS = 2.5$$

The GCL and natural soil interface should provide the lowest interface factor of safety for the liner system. A factor of safety of at least 1.5 is considered acceptable for short and long-term stability. Therefore the liner system is stable as designed. Interface testing of the liner system components should be conducted prior to construction to verify that the liner system will be stable for site-specific conditions.

3. Infinite Slope Analysis of Cover System

The critical cover system will occur on the 4H:1V side slope.

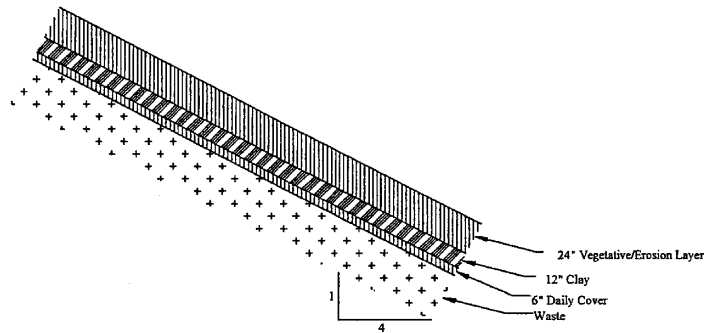


Figure 2.

Erosion layer and clay interface

- ϕ = 10°
- c = 200 psf
- β = 14.04°
- A = 1 (see attached charts, Ref. 3)
- B = 4.2 (see attached charts, Ref. 3)
- γ = 120 pcf
- H = 2 feet

$$FS = 1 \left(\frac{\tan 10^\circ}{\tan 14.04^\circ} \right) + 4.2 \left[\frac{200}{(120)(2)} \right]$$

$$FS = 4.2$$

Clay and daily cover interface

- ϕ = 10°
- c = 200 psf
- β = 14.04°
- A = 0.85 (see attached charts, Ref. 3)
- B = 4.2 (see attached charts, Ref. 3)
- γ = 120 pcf
- H = 3 feet

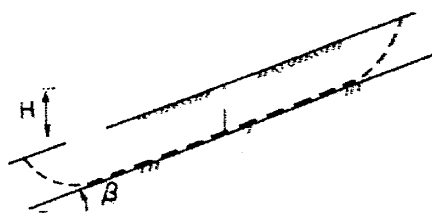
Prepared By: PRW
Date: 12/15/05

City of Amarillo Landfill
Liner System Design

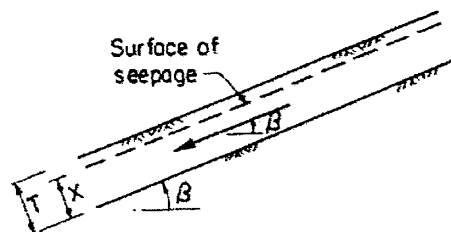
Checked By: MMG
Date: 12-15-05

$$FS = 0.85 \left(\frac{\tan 10^\circ}{\tan 14.04^\circ} \right) + 4.2 \left[\frac{200}{(120)(3)} \right]$$
$$FS = 2.9$$

The final cover system will be stable as designed. The clay and daily cover interface has the lowest factor of safety. Interface testing should be conducted prior to construction to verify that the liner system will be stable for site-specific conditions.

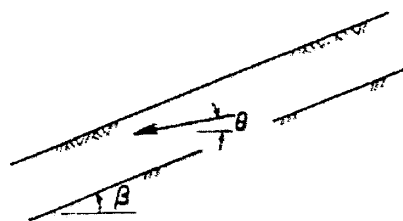


γ = total unit weight of soil
 γ_w = unit weight of water
 c' = cohesion intercept
 ϕ' = friction angle } Effective Stress
 r_u = pore pressure ratio = $\frac{u}{\gamma H}$
 u = pore pressure at depth H



Seepage parallel to slope

$$r_u = \frac{x}{T} \frac{\gamma_w}{\gamma} \cos^2 \beta$$



Seepage emerging from slope

$$r_u = \frac{\gamma_w}{\gamma} \frac{1}{1 + \tan \beta \tan \theta}$$

Steps:

- ① Determine r_u from measured pore pressures or formulas at right
- ② Determine A and B from charts below
- ③ Calculate $F = A \frac{\tan \phi'}{\tan \beta} + B \frac{c'}{\gamma H}$

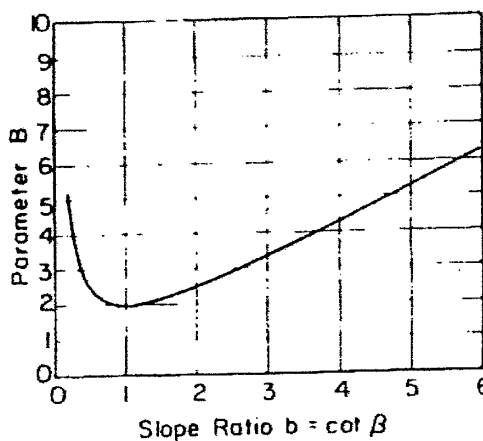
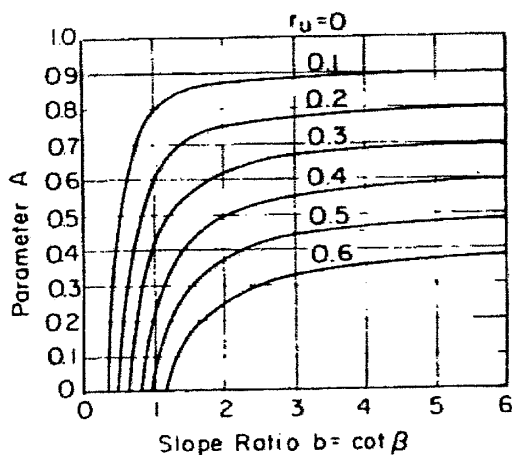
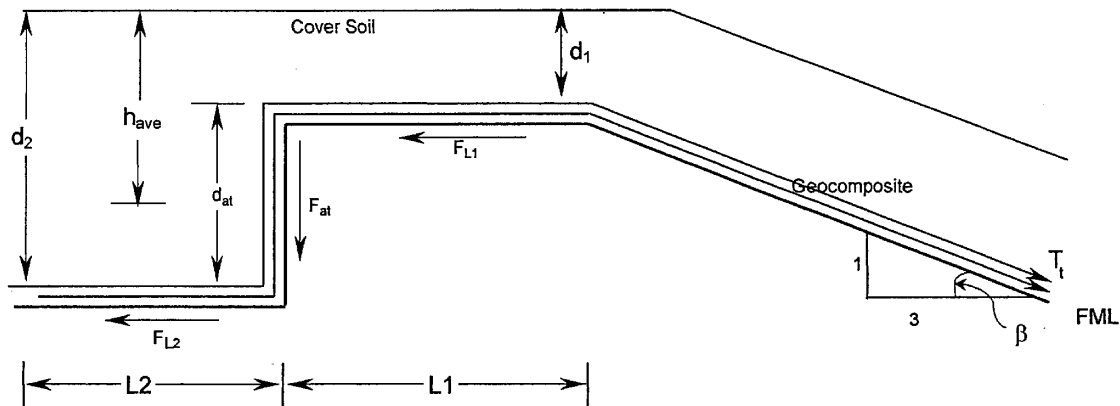


Fig. 10 STABILITY CHARTS FOR INFINITE SLOPES.

4. Anchor Trench Design



$T_t = F_{L1} + F_{at} + F_{L2}$	T_t	=	Force required for pull-out of FML
	$q_1 = d_1 \gamma_{soil}$	=	Surcharge pressure, psf
$F_{L1} = (q_1 \tan A_1) L_1 + C L_1$	d_1	=	Depth of cover soil, ft.
	γ_{soil}	=	Unit weight of soil, pcf
$F_{at} = (V \tan A_2) d_{at} + C d_{at}$	A	=	Interface friction angle between liner components
$F_{L2} = (q_2 \tan A_3) L_2 + C L_2$	L_1	=	Length of runout, ft.
	L_2	=	Length of trench bottom
	C	=	Cohesion/adhesion intercept between liner components
	$V = k_o y$	=	Average horizontal stress
	k_o	=	$1 - \sin \phi$
	ϕ	=	Internal friction angle of cover soil
	y	=	$\gamma_{soil} h_{ave}$
	h_{ave}	=	Average depth of trench with cover soil
	d_{at}	=	Depth of trench

Parameters:

Cover / Geocomposite	$A_1 = 10^\circ$ $C_1 = 200 \text{ psf}$	Geomembrane / GCL	$A_3 = 12^\circ$ $C_3 = 200 \text{ psf}$
Geocomposite / Geomembrane	$A_2 = 15^\circ$ $C_2 = 200 \text{ psf}$	GCL / Natural Soil	$A_4 = 20^\circ$ $C_4 = 120 \text{ psf}$

$$\begin{aligned}\gamma_{soil} &= 120 \text{ psf} \\ \phi &= 15^\circ \\ d_1 &= 2 \text{ ft} \\ d_2 &= 4 \text{ ft} \\ d_{at} &= 2 \text{ ft} \\ h_{ave} &= 3 \text{ ft} \\ L_1 &= 2 \text{ ft} \\ L_2 &= 2 \text{ ft}\end{aligned}$$

Calculate:

$$\begin{aligned}q_1 &= d_1 \gamma_{soil} = (2)(120) = 240 \text{ psf} \\ V &= k_o y \\ V &= (1 - \sin 15^\circ)(120)(3) = 266.8 \text{ psf} \\ q_2 &= d_2 \gamma_{soil} = (4)(120) = 480 \text{ psf}\end{aligned}$$

T_t for Cover / Geocomposite

$$\begin{aligned}F_{L_1} &= (240) \tan 10^\circ (2) + 200(2) \\ &= 485 \text{ lb/ft width}\end{aligned}$$

$$\begin{aligned}F_{at} &= (266.8) \tan 10^\circ (2) + 200(2) \\ &= 494 \text{ lb/ft width}\end{aligned}$$

$$\begin{aligned}F_{L_2} &= (480) \tan 10^\circ (2) + 200(2) \\ &= 569 \text{ lb/ft width}\end{aligned}$$

$$T_t = 485 + 494 + 569 = 1,548 \text{ lb/ft width}$$

T_t for Geocomposite / Geomembrane (textured)

$$F_{L_1} = (240)\tan 15^\circ(2) + 200(2) \\ = 529 \text{ lb/ft width}$$

$$F_{L_1} = (266.8)\tan 15^\circ(2) + 200(2) \\ = 543 \text{ lb/ft width}$$

$$F_{L_2} = (480)\tan 15^\circ(2) + 200(2) \\ = 657 \text{ lb/ft width}$$

$$T_t = 529 + 543 + 657 = 1,729 \text{ lb/ft width}$$

T_t for Geomembrane (textured) / GCL

$$F_{L_1} = (240)\tan 12^\circ(2) + 200(2) \\ = 502 \text{ lb/ft width}$$

$$F_{L_1} = (266.8)\tan 12^\circ(2) + 200(2) \\ = 513 \text{ lb/ft width}$$

$$F_{L_2} = (480)\tan 12^\circ(2) + 200(2) \\ = 604 \text{ lb/ft width}$$

$$T_t = 502 + 513 + 604 = 1,619 \text{ lb/ft width}$$

T_t for GCL / Natural soil

$$F_{L_1} = (240)\tan 20^\circ(2) + 150(2) \\ = 475 \text{ lb/ft width}$$

$$F_{L_1} = (266.8)\tan 20^\circ(2) + 150(2) \\ = 494 \text{ lb/ft width}$$

$$F_{L_1} = (480)\tan 20^\circ(2) + 150(2) \\ = 649 \text{ lb/ft width}$$

$$T_t = 475 + 494 + 649 = 1,618 \text{ lb/ft width}$$

The lowest resistance is from the cover / geocomposite interface. Therefore, additional strength gained from anchor trench is 1,548 pounds per foot of width.

For 60 mil HDPE textured geomembrane:

$$\begin{aligned} \text{Yield Strength} &= 126 \text{ lb/in.} \quad (\text{Ref. 7}) \\ \text{Break Strength} &= 90 \text{ lb/in.} \quad (\text{Ref. 7}) \end{aligned}$$

$$\text{Break Strength, } T = 90 \frac{\text{lb}}{\text{in.}} \left(\frac{1 \text{ sheet}}{0.060 \text{ in.}} \right) = 1,500 \text{ psi}$$

$$\sigma_{all} = \frac{T}{FS} = \frac{1,500}{3} = 500 \text{ psi} \quad \text{FS} = 3$$

$$\sigma_{all} = \frac{T}{FS} = \frac{1,500}{2} = 750 \text{ psi} \quad \text{FS} = 2$$

To calculate anchorage resistance value:

σ_{all} = allowable mobilized stress

$$\sigma_{all} = 500 \text{ psi} \left(144 \frac{\text{in.}^2}{\text{ft}^2} \right) \left(\frac{0.06 \text{ in.}}{12 \text{ in / ft}} \right)$$

$$\sigma_{all} = 360 \text{ lb/ft}$$

$$\sigma_{all} \cos \beta = 360 \cos 18.43^\circ = 341 \text{ lb/ft (horizontal)}$$

$$\sigma_{Break} = 1,023 \text{ lb/ft (horizontal component)}$$

$$\sigma_{Yield} = 1,435 \text{ lb/ft (horizontal component)}$$

T_i = Resistance from anchor trench = 1,548 lbs for weakest interface

For current dimension and run out length, anchor trench will secure geomembrane, with geomembrane failure at yield and break strengths before anchor trench pull-out.

Prepared By: PRW
Date: 12/15/05

City of Amarillo Landfill
Liner System Design

Checked By: JMM⁹
Date: 12-15-05

Liner System Design Summary

Calculations for the liner system shear forces indicate the individual liner components are not subject to external forces when loaded with 20 feet of solid waste. The infinite slope analysis further indicates that the liner system is stable along the slope prior to waste deposition.

Anchor trench design will provide additional strength to liner system for resisting pull-out or liner slippage down the slope, should it occur.

Interface testing between the liner system components should be conducted prior to construction to verify that the liner system will be stable for site-specific conditions.

**City of Amarillo Landfill
Potter County, Texas
Foundation Settlement Analysis**

Determine settlement of the subsurface strata when landfill has maximum load.

Procedure:

Generalize subsurface strata as one layer of clayey sand, based on information gathered from previous borings and four additional borings drilled by Kleinfelder.

Conduct a consolidation test on a sample from Boring 201 at a depth of 35 to 36½ feet below the existing ground surface (results presented on Plate 37, discussion located in text).

Use results of the consolidation test to determine parameters for settlement calculation.

The foundation settlement can be calculated using the equation:

$$S_c = \frac{C_r H_c}{1 + e_o} \log \frac{p_c}{p_o} + \frac{C_c H_c}{1 + e_o} \log \frac{p_o + \Delta p}{p_c}$$

Where: S_c = Settlement (*ft*)
 H_c = Height of Soil Layer (*ft*)
 e_o = Initial void ratio
 C_r = Recompression Index
 C_c = Compression Index
 p_o = Present Overburden Pressure (*psf*)
 p_c = Preconsolidation Pressure (*psf*)
 Δp = Change in Overburden Pressure (*psf*)

The unit weights of soil and solid waste used for the settlement calculation are 125 and 70 *pcf*, respectively.

The maximum depth of solid waste is 240 feet. This includes a 70-foot excavation below natural grade and 170 feet of fill above natural grade.

Solution:

1. Calculate the present overburden pressure at the midpoint of the subgrade layer.

$$p_o = \gamma_{soil} \frac{H_c}{2}$$

$$p_o = (125 \text{ pcf}) \frac{50 \text{ ft}}{2}$$

$$p_o = 3125 \text{ psf}$$

2. Calculate the change in overburden pressure.

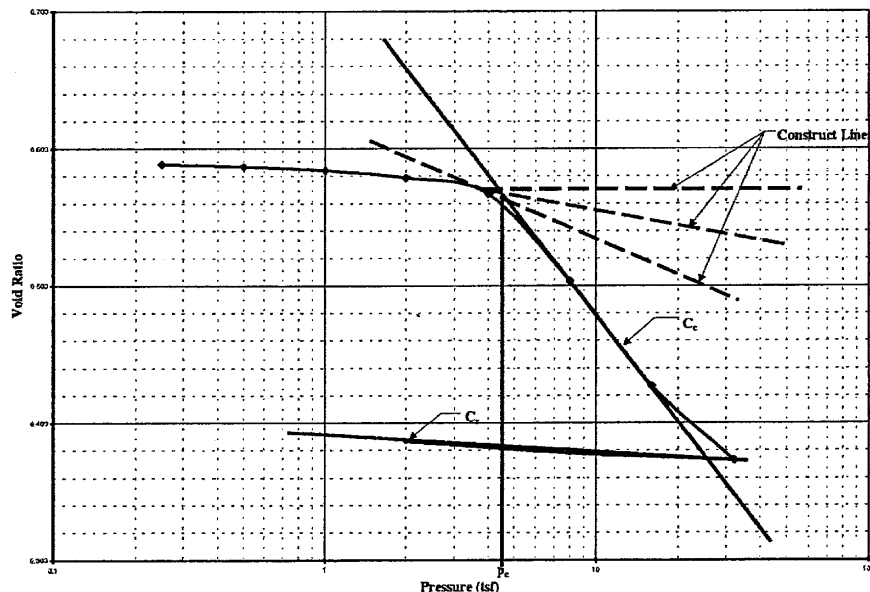
$\Delta p = \text{Pressure of Solid Waste} - \text{Pressure of Excavated Material}$

$$\Delta p = (70 \text{ pcf})(240 \text{ ft}) - (125 \text{ pcf})(70 \text{ ft})$$

$$\Delta p = 8050 \text{ psf}$$

3. From the consolidation test results:

Using Casagrande's construct, determine p_c



$$p_c \approx 4.4 \text{ tsf} = 8800 \text{ psf}$$

The Compression Index is the slope of the straight-line portion of the consolidation curve.

$$C_c = \frac{e_1 - e_2}{\log\left(\frac{p_2}{p_1}\right)}$$

Where (e_1, p_1) and (e_2, p_2) are points along the straight/line portion of the consolidation curve.

$$C_c \approx 0.25$$

The Recompression Index is the slope of the straight-line portion of the rebound curve.

$$C_r = \frac{e_3 - e_4}{\log\left(\frac{p_4}{p_3}\right)}$$

Where (e_3, p_3) and (e_4, p_4) are points along the straight/line portion of the consolidation curve.

$$C_r \approx 0.01$$

The initial void ratio determined from the consolidation test is:

$$e_o = 0.598$$

4. Substituting into the settlement equation:

$$S_c = \frac{0.01 \cdot 50 \text{ ft}}{1 + 0.598} \log \frac{8800 \text{ psf}}{3125 \text{ psf}} + \frac{0.25 \cdot 50 \text{ ft}}{1 + 0.598} \log \frac{3125 \text{ psf} + 8050 \text{ psf}}{8800 \text{ psf}}$$

$$S_c = 0.141 \text{ ft} + 0.812 \text{ ft}$$

$$S_c = 0.952 \text{ ft}$$

$$S_c = 11.4 \text{ in.}$$

Prepared By: PRW
Date: 10/15/05

City of Amarillo Landfill
Foundation Settlement Analysis

Checked By: MMG
Date: 12/15/05

Conclusion:

The foundation settlement is estimated to be about 1 foot, based on the results of the consolidation test. The estimated settlement should be conservative since only a portion of the landfill will have the 240-foot waste thickness expected. Most of the site will have less waste thickness.

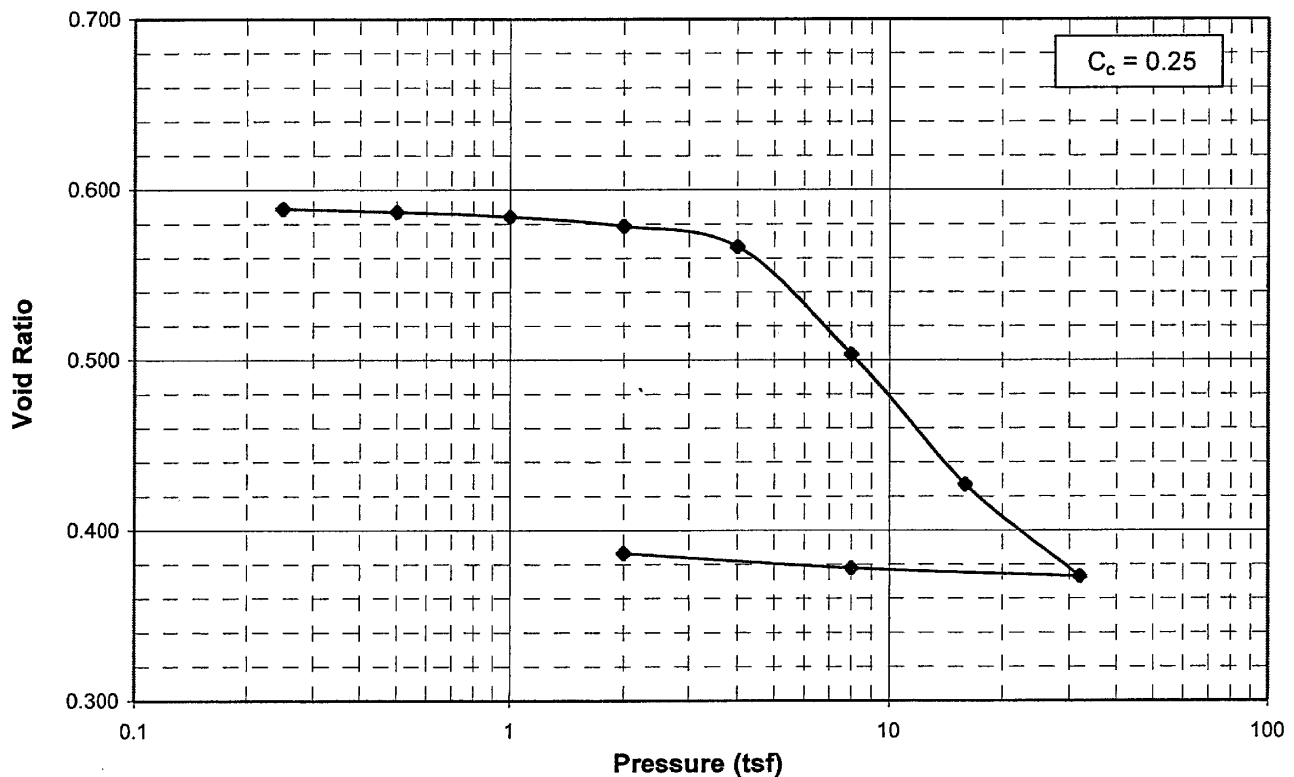


KLEINFELDER
Geotechnical Engineering, Environmental Services, and
Construction Materials Engineering and Testing

One-Dimensional Consolidation Test Results

Project Name:	<u>Amarillo Landfill</u>	Tested By:	<u>D. Green</u>
Location:	<u>Amarillo, Texas</u>	Date Tested:	<u>6/21/2005</u>
Material Description:	<u>CLAYEY SAND, silty, light brown</u>	Consolidometer ID:	<u>G</u>
Project No.:	<u>57815</u>	Assumed Specific Gravity:	<u>2.65</u>
Boring No.:	<u>B-201</u>		
Sample Depth (ft.):	<u>35 to 36.5</u>		
Sample Type:	<u>Undisturbed</u>		

	<u>Initial</u>	<u>Final</u>
Void Ratio =	0.598	0.373
Moisture Content (%) =	7.2	21.2
Wet Unit Weight (pcf) =	111.0	129.2
Dry Unit Weight (pcf) =	103.5	106.6
Saturation (%) =	32.0	100.0



The results shown on this report are for the exclusive use of the client for whom they were obtained and apply only to the samples tested. They are not intended to be indicative of the qualities of apparently identical products. The use of our name must receive prior written approval. Reports must be reproduced in their entirety. Test method generally based on ASTM D 2435.

**City of Amarillo Landfill
Potter County, Texas
Solid Waste Settlement Analysis**

Estimate total settlement in the Type I solid waste due to primary (short-term) and secondary (long-term decomposition) settlement.

Procedure:

1. Calculate total settlement
2. Determine the change in final cover grades due to differential settlement calculations.

Settlement of Type 1 waste can be modeled using consolidation theory for clay soils. Settlement can be calculated using the following equation:

$$S = \frac{H_o \Delta e}{1 + e_o}$$

Where: S = Settlement (ft)
 H_o = Initial waste height (ft) or thickness of waste layer being currently evaluated
 e_o = Initial void ratio
 Δe = Change in void ratio

Primary and secondary consolidation of the waste is then computed by substituting in appropriate expressions for the change in void ratio.

Solution:

1. Primary settlement of solid waste:

Solid waste will undergo primary compression due to its own weight, weight of waste placed above it, final cover, and equipment. Primary compression occurs quickly, generally within the first month after loading. Primary compression occurs due to the weight of the waste lift above the waste layer being evaluated. Primary compression is calculated using soil consolidation theory.

$$\Delta e = C_c \left(\log \frac{\sigma'_o + \Delta \sigma}{\sigma'_o} \right)$$

Where: C_c = Compression index
= 0.15 e_o for fills low in organic content
= 0.55 e_o for fills high in organic content
 $\Delta \sigma$ = Change in loading (psf)
 σ'_o = Effective stress at mid-height of waste (psf)

Height of solids in waste:

$$H_s = \frac{W_s}{AS_G \gamma_w}$$

Where: H_s = Height of solids (ft)
 W_s = Weight of solids = 37 lbs.
 $\gamma_{waste,i}$ and moisture content of 10% (Ref. 9)
 A = Area = 1 ft²
 S_G = Specific gravity of waste = 1.8 (Ref. 9)
 γ_w = Unit weight of water = 62.4 lbs./ft³

$$H_s = 0.33 \text{ ft}$$

The total height of 1 ft³ of material is 1 ft.

$$H_T = 1.00 \text{ ft}$$

Height of voids:

$$H_v = H_T - H_s$$

Where: H_v = Height of voids (ft)
 H_T = Total height of material = 1.00 ft
 H_s = Height of solids = 0.33 ft

$$H_v = 0.67 \text{ ft}$$

Initial void ratio:

$$e_o = \frac{V_v}{V_s} = \frac{H_v A}{H_s A} = \frac{H_v}{H_s}$$

$$H_v = 0.67 \text{ ft}$$

$$H_s = 0.33 \text{ ft}$$

$$e_o = 2.04 \text{ (typical of well compacted waste, Ref. 9)}$$

For this site assume:

$$C_c = 0.35e_o = 0.71 \text{ (fill with a moderate quantity of organic content, Ref. 8)}$$

Substituting the equation for Δe into the settlement equation and solving for settlement:

$$S_p = \frac{H_o C_c}{1 + e_o} \left(\log \frac{\sigma'_o + \Delta\sigma}{\sigma'_o} \right)$$

Where: S_p = Primary settlement (ft)

σ'_o = [0.5 (layer thickness being evaluated) + (overlying waste thickness)] $\times \gamma_s$

$\Delta\sigma$ = $\gamma_{waste} \times$ (waste thickness above waste layer being evaluated)

2. Secondary settlement of solid waste

Secondary settlement continues for periods of time well beyond primary compression. Secondary settlement is a combination of secondary compression, physio-chemical action, and biochemical decay. The settlement-log time relationship is similar to secondary compression of soils and can be expressed by the following equation:

$$\Delta e = \alpha \left(\log \frac{t_2}{t_1} \right) \quad \text{Ref. 9}$$

Where: α = Secondary compression factor
= 0.03 e_o for conditions unfavorable to decay of inert materials
= 0.09 e_o for conditions favorable to decay of inert materials
 t_1 = Initial time of current interval
 t_2 = Time at which settlement is determined (year)

Secondary settlement is calculated as follows:

$$S_c = \frac{H_o}{1 + e_o} \left(\alpha \log \frac{t_2}{t_1} \right)$$

Where: S_c = Secondary settlement (ft)

Variables: e_o = 2.04
 α = $0.06e_o = 0.12$
 $\frac{\alpha}{1 + e_o}$ = 0.04 (range between 0.02 and 0.07, Ref. 8 & 10)

The following tables show the calculations for waste settlement. Table 1 shows the settlement for a portion of the landfill that is filled to 70 feet and then left until there is little or no settlement occurring, and then the additional 170 feet of waste is placed to achieve the total 240 feet of solid waste thickness. Table 2 shows the settlement for a portion of the landfill that is filled to 240 feet with solid waste. The difference between the two settlements calculated in Tables 1 and 2 represent the greatest amount of differential solid waste settlement the landfill should experience. Due to filling techniques and other operational parameters, the actual differential settlement will be less than calculated.

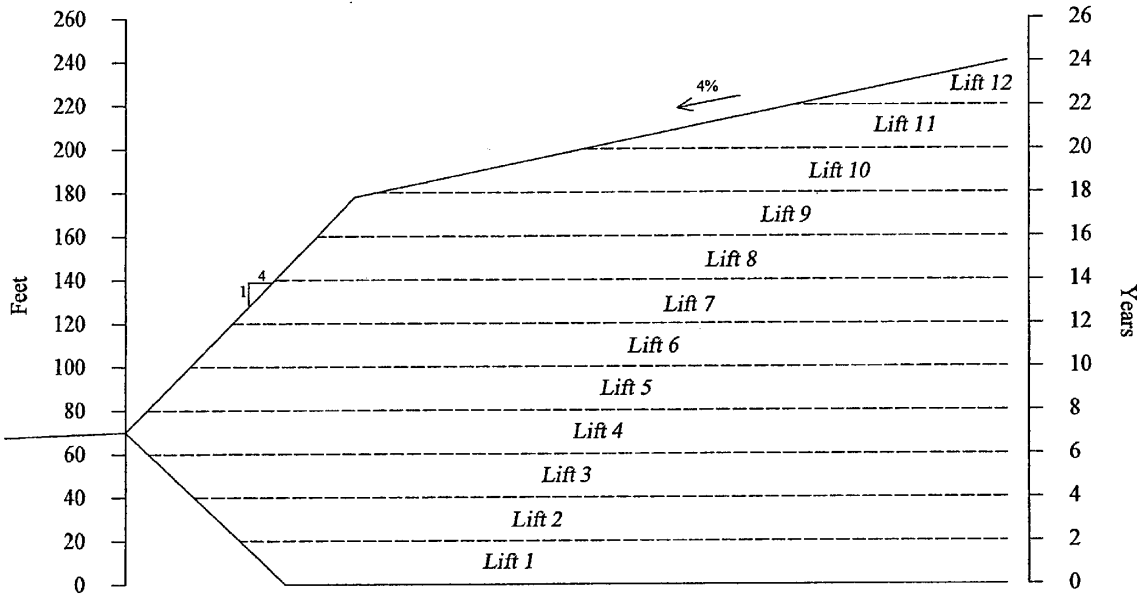
The waste settlement calculations have assumed:

1. The depth of solid waste can achieve 240 feet in thickness
2. The cell will be filled to capacity in about 24 years once waste placement begins

These assumptions are conservative and will result in waste settlement magnitudes that over estimate waste settlement since,

- Daily compaction operations will likely result in more dense waste that is less susceptible to long-term settlement.
- If waste deposition takes longer than the settlement calculations account for, more settlement will have occurred prior to placement of final cover.

Landfill Layers and Time Intervals Used in Waste Settlement Calculations



**City of Amarillo Landfill
Potter County, Texas
Potential Final Cover Differential Settlement Analysis**

Procedure:

1. Assume entire area of Cells 1, 2, and 3 have been filled to a waste depth of 70 feet, prior to waste placement in other cells.
2. Waste thickness in Cells 1, 2 and 3 is not increased for 70 years.
3. Entire waste column of 240 feet is placed next to previously deposited Cells 1, 2, and 3, while aerial fill is placed over Cells 1, 2, and 3.
4. Differential cover settlement is determined.
5. Tensile strain calculated in cover system.

Calculations:

From Table 1:

Settlement at 8 years = 11.09 feet total

Settlement at 70 years = 19.17 feet total

Assume areal fill is placed starting at EOY 70, up to maximum waste thickness of 240 feet, until EOY 86 when maximum thickness is achieved.

Settlement at EOY 86 = 46.28 feet total

Cover System placed

Settlement at EOY 150 = 63.19 feet total

Differential settlement potential over Cell 1, 2, or 3 is

63.19 feet – 46.28 feet = 16.91 feet total

At EOY 62 in Table 1, Solid Waste deposition begins in adjacent cell, to provide waste fill depth of 70 – 80 feet in 8 years as indicated in Table 2 to coincide with EOY without Settlement from Table 1. Fill continues up to maximum waste thickness of 240 feet. EOY 16 in Table 2, corresponds to EOY 86, Table 1.

Therefore Table 2,

Settlement at EOY 24 = 57.39 feet total
and cover system is placed corresponding to cover
system placement at EOY 86, Table 1.

Settlement at EOY 88 = 73.32 feet total
corresponding to EOY 150, Table 1.

73.32 feet – 57.39 feet = 15.93 feet total,
settlement of cover system corresponding with Table 1.

Potential differential settlement of cover systems between Tables 1 and 2.

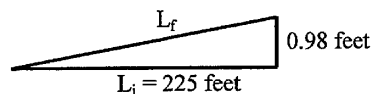
$$16.9 \text{ feet} - 15.93 \text{ feet} = 0.98 \text{ feet total}$$

To calculate tensile strain on cover system, that is, strain induced by
differential settlement

$$\epsilon = (L_f - L_i) / L_i$$

Where L_f and L_i = horizontal distance between two points after settlement and
prior to settlement, respectively (See Section 7.0 REFERENCE No. 11)

Assume settlement occurs over 225 feet, which is the horizontal length over
3:1 slope, 50 feet high or 150 feet horizontal plus a 75-foot horizontal bench
for 225 feet.



$$L_f = ((225)^2 + (0.98)^2)^{1/2}$$

$$L_f = 225.002 \text{ feet}$$

$$\epsilon = 9.9 \times 10^{-4}\% - \text{negligible, ok}$$

Typical strain at failure for compacted clay 0.1 – 4% (See Section 7.0
REFERENCE No. 10)

Compute potential worst-case situation for final cover strain for consecutive
points at the surface.

Prepared By: PRW
Date: 12/15/05

City of Amarillo Landfill
Potential Final Cover Differential Settlement Analysis

Checked By: MBC
Date: 12/15/05

Assume fill up to 240 in 24 years (Table 2)

Waste in place for 10 years, EOY 34, cover system is placed

Settlement at EOY 34 = 67.64 feet total

Settlement at EOY 150 = 76.33 feet total

8.69 feet differential

Settlement over 225 feet (conservative)

$L_f = 225.17$ feet

$\epsilon = 0.075\%$ okay

If settlement occurs over 75 feet (length of bench)

$\epsilon = 0.67\% > 0.1\%$,

which places tensile strain in lower end of failure strain range.

Assume fill to 240 feet at:

EOY 24, Table 2 $S = 57.39$ feet

EOY 150, Table 2 $S = \underline{76.33}$ feet

18.94 feet differential

Settlement over 225 feet (conservative)

$L_f = 225.17$ feet

$\epsilon = 0.35\%$ lower end of failure strain range

Note: Foundation settlement neglected in these calculation since it is a minor amount, distributed on a wide area and will be negligible to these calculations made over a discreet, horizontal distance.

Prepared By: PRW
Date: 12/15/05

City of Amarillo Landfill
Potential Final Cover Differential Settlement Analysis

Checked By: MMG
Date: 12/15/05

Conclusions:

Settlement within the final cover system will occur and potential tensile strain will depend upon waste placement, compaction, and time that waste is in place prior to landfill cover placement and closure. It is more likely that settlement within the solid waste will occur over longer distances than calculated for these estimates. These distance assumptions for L_i imply that solid waste composition would have completely different material properties within short horizontal distances, which is very unlikely. The landfill cover system must be maintained in accordance with the Post-Closure Maintenance Plan since fill settlement will occur. Actual tensile strain failure of the clay final cover is unlikely, so long as the post-closure maintenance is implemented.

CITY OF AMARILLO MUNICIPAL SOLID WASTE LANDFILL

PERMIT NO. 73

Groundwater Elevation Analysis
1994-2005

Date	MW 1	MW 2	MW 3	MW 4	MW 5	MW 6	MW 7	MW 8	MW 9	MW 10	MW 11	MW 12	MW 13	B 203	B 204
09/20/94	3590.24	3590.44	3588.90	3596.26	3613.78	3601.55	3595.12	3594.75	3599.57	N/A	N/A	N/A	N/A	N/A	N/A
09/28/94	3588.65	3587.34	3588.98	3595.69	3613.03	3601.06	3594.51	3594.11	3599.24	N/A	N/A	N/A	N/A	N/A	N/A
10/05/94	3590.32	3590.44	3590.12	3596.51	3613.84	3601.55	3595.20	3594.80	3597.59	N/A	N/A	N/A	N/A	N/A	N/A
10/12/94	3590.27	3590.44	3590.07	3596.56	3613.89	3601.55	3595.01	3594.75	3597.54	N/A	N/A	N/A	N/A	N/A	N/A
10/19/94	3590.32	3590.44	3590.12	3596.51	3613.84	3601.55	3595.11	3594.75	3599.59	N/A	N/A	N/A	N/A	N/A	N/A
10/26/94	3590.27	3590.44	3590.12	3596.66	3613.94	3601.50	3595.16	3594.80	3599.54	N/A	N/A	N/A	N/A	N/A	N/A
10/31/94	3590.22	3590.39	3589.97	3596.66	3613.99	3601.50	3594.96	3594.65	3599.44	N/A	N/A	N/A	N/A	N/A	N/A
11/09/94	3590.17	3590.39	3589.97	3596.76	3614.09	3601.50	3595.01	3594.65	3599.44	N/A	N/A	N/A	N/A	N/A	N/A
11/16/94	3590.22	3590.39	3590.02	3596.81	3614.24	3601.45	3595.06	3594.75	3599.44	N/A	N/A	N/A	N/A	N/A	N/A
11/23/94	3590.22	3590.34	3590.02	3596.91	3614.34	3601.45	3595.11	3594.75	3599.49	N/A	N/A	N/A	N/A	N/A	N/A
11/30/94	3590.92	3590.34	3590.02	3597.06	3614.39	3601.45	3595.01	3594.75	3599.44	N/A	N/A	N/A	N/A	N/A	N/A
12/07/94	3590.12	3590.24	3590.02	3597.06	3614.39	3601.40	3594.65	3594.65	3599.39	N/A	N/A	N/A	N/A	N/A	N/A
12/14/94	3589.87	3590.34	3590.02	3597.11	3614.39	3601.40	3595.01	3594.75	3599.44	N/A	N/A	N/A	N/A	N/A	N/A
02/20/95	3590.65	3590.25	3589.00	3596.65	3614.10	3601.40	3595.02	3594.65	3599.34	N/A	N/A	N/A	N/A	N/A	N/A
03/14/95	3590.22	3590.74	3588.87	3595.86	3614.16	3601.45	3595.21	3595.00	3598.64	N/A	N/A	N/A	N/A	N/A	N/A
04/14/95	3589.82	3590.69	3589.82	3596.56	3614.19	3601.55	3595.11	3594.85	3599.64	N/A	N/A	N/A	N/A	N/A	N/A
05/14/95	3589.77	3590.64	3590.64	3596.36	3614.09	3601.55	3594.61	3594.85	3599.59	N/A	N/A	N/A	N/A	N/A	N/A
06/14/95	3589.82	3590.29	3590.29	3597.01	3614.39	3601.45	3595.11	3594.70	3599.54	N/A	N/A	N/A	N/A	N/A	N/A
07/14/95	3589.82	3590.69	3590.69	3596.46	3614.09	3601.50	3595.11	3594.90	3599.59	N/A	N/A	N/A	N/A	N/A	N/A
08/14/95	3589.67	3590.49	3589.77	3596.31	3614.19	3601.45	3595.06	3594.80	3599.54	N/A	N/A	N/A	N/A	N/A	N/A
09/14/95	3589.67	3590.54	3589.72	3597.46	3614.69	3601.40	3594.91	3594.80	3599.64	N/A	N/A	N/A	N/A	N/A	N/A
10/16/95	3589.65	3589.85	3588.70	3597.25	3614.30	3602.10	3594.67	3594.15	3599.14	N/A	N/A	N/A	N/A	N/A	N/A
11/16/95	3589.55	3589.75	3588.70	3597.40	3614.35	3600.95	3594.52	3594.55	3599.14	N/A	N/A	N/A	N/A	N/A	N/A
12/14/95	3589.65	3589.75	3588.75	3597.40	3614.30	3601.10	3594.57	3594.65	3599.14	N/A	N/A	N/A	N/A	N/A	N/A
01/15/96	3589.70	3589.85	3588.80	3597.45	3614.30	3601.15	3594.62	3594.70	3599.14	N/A	N/A	N/A	N/A	N/A	N/A
02/15/96	3589.45	3589.55	3588.65	3597.10	3614.10	3600.90	3594.42	3594.45	3599.04	N/A	N/A	N/A	N/A	N/A	N/A
04/16/96	3589.35	3589.74	3588.67	3596.63	3613.94	3600.94	3594.60	3594.65	3599.14	N/A	N/A	N/A	N/A	N/A	N/A
05/15/96	3588.45	3589.55	3588.80	3596.30	3613.80	3600.85	3594.32	3594.40	3599.04	N/A	N/A	N/A	N/A	N/A	N/A
06/15/96	3588.36	3589.60	3588.52	3596.15	3613.78	3600.75	3594.80	3594.38	3599.04	N/A	N/A	N/A	N/A	N/A	N/A
07/16/96	3588.10	3589.55	3588.50	3595.95	3613.94	3600.67	3594.72	3594.35	3598.94	N/A	N/A	N/A	N/A	N/A	N/A
08/15/96	3588.00	3589.43	3588.38	3596.10	3613.70	3600.73	3594.47	3594.30	3598.89	N/A	N/A	N/A	N/A	N/A	N/A
09/15/96	3587.88	3589.12	3588.30	3596.05	3613.30	3600.62	3594.17	3594.40	3598.84	N/A	N/A	N/A	N/A	N/A	N/A
10/16/96	3587.78	3588.85	3588.26	3596.00	3614.89	3600.40	3593.97	3594.21	3598.83	N/A	N/A	N/A	N/A	N/A	N/A
11/20/96	3586.92	3588.99	3588.35	3596.13	3614.20	3600.80	3594.07	3594.37	3598.89	N/A	N/A	N/A	N/A	N/A	N/A
12/20/96	3587.45	3589.10	3588.10	3595.75	3614.65	3600.80	3593.87	3594.42	3599.04	N/A	N/A	N/A	N/A	N/A	N/A

CITY OF AMARILLO MUNICIPAL SOLID WASTE LANDFILL

PERMIT NO. 73
Groundwater Elevation Analysis
1994-2005

Date	MW 1	MW 2	MW 3	MW 4	MW 5	MW 6	MW 7	MW 8	MW 9	MW 10	MW 11	MW 12	MW 13	B 203	B 204
01/15/97	3588.18	3588.30	3587.22	3595.21	3614.06	3600.24	3593.51	3594.16	3598.49	N/A	N/A	N/A	N/A	N/A	N/A
02/15/97	3588.31	3588.28	3587.20	3595.14	3613.86	3600.21	3593.54	3594.21	3598.43	N/A	N/A	N/A	N/A	N/A	N/A
03/15/97	3588.32	3588.24	3587.18	3595.08	3613.72	3600.15	3593.52	3594.15	3598.38	N/A	N/A	N/A	N/A	N/A	N/A
04/15/97	3588.28	3588.20	3587.13	3595.00	3613.62	3600.15	3593.56	3594.18	3598.36	N/A	N/A	N/A	N/A	N/A	N/A
05/16/97	3588.28	3588.14	3587.10	3594.90	3613.52	3600.24	3593.49	3594.05	3598.75	N/A	N/A	N/A	N/A	N/A	N/A
06/18/97	3588.27	3588.11	3587.07	3594.85	3613.43	3600.50	3593.46	3594.00	3599.22	N/A	N/A	N/A	N/A	N/A	N/A
10/14/97	3587.45	3587.90	3586.89	3594.55	3614.12	3600.40	3593.31	3593.80	3598.79	N/A	N/A	N/A	N/A	N/A	N/A
11/20/97	3588.18	3587.86	3586.84	3594.45	3614.00	3600.21	3593.23	3593.75	3598.56	N/A	N/A	N/A	N/A	N/A	N/A
04/14/98	3588.30	3587.72	3586.76	3594.23	3613.43	3599.95	3593.21	3593.51	3598.18	N/A	N/A	N/A	N/A	N/A	N/A
10/14/98	3587.29	3587.64	3586.45	3593.77	3613.40	3599.69	3593.09	3593.28	3597.87	N/A	N/A	N/A	N/A	N/A	N/A
04/19/99	3587.68	3587.33	3586.19	3593.41	3613.94	3599.48	3592.57	3592.90	3597.65	N/A	N/A	N/A	N/A	N/A	N/A
10/11/99	3588.02	3587.23	3585.95	3593.26	3614.53	3599.50	3592.63	3592.68	3597.74	N/A	N/A	N/A	N/A	N/A	N/A
04/17/00	3587.91	3587.09	3585.76	3593.00	3613.45	3599.19	3592.53	3592.56	3597.34	3590.68	3590.70	3590.74	3590.76	N/A	N/A
10/16/00	3587.57	3586.96	3585.51	3592.71	3613.25	3598.93	3592.30	3592.40	3596.99	3590.35	3590.47	3590.50	3590.48	N/A	N/A
04/16/01	3587.21	3586.74	3585.26	3592.41	3613.12	3598.66	3592.10	3592.02	3596.69	3590.41	3590.27	3590.32	3590.20	N/A	N/A
10/16/01	3586.37	3586.62	3585.09	3592.29	3613.25	3598.49	3591.78	3591.93	3596.49	3589.52	3590.02	3590.16	3590.06	N/A	N/A
04/15/02	3587.22	3586.50	3584.88	3591.95	3613.07	3598.20	3591.70	3591.71	3596.19	3589.89	3589.98	3590.00	3589.86	N/A	N/A
10/14/02	3587.32	3586.41	3584.73	3591.63	3613.12	3598.02	3591.54	3591.53	3596.09	3589.79	3589.83	3589.88	3589.67	N/A	N/A
04/14/03	3587.85	3586.16	3584.44	3591.30	3613.08	3597.75	3591.32	3591.19	3595.73	3589.72	3589.10	3589.54	3589.43	N/A	N/A
10/14/03	3586.75	3586.04	3584.24	3591.08	3609.34	3597.53	3591.10	3591.02	3595.46	3589.40	3589.45	3589.43	3589.28	N/A	N/A
04/14/04	3586.77	3585.91	3584.08	3590.82	3613.25	3597.34	3591.01	3590.88	3595.23	3589.31	3589.30	3589.21	3589.07	N/A	N/A
10/18/04	3586.76	3585.63	3583.77	3590.59	3613.99	3597.30	3590.75	3590.57	3595.61	3589.16	3589.04	3588.90	3588.92	N/A	N/A
10/18/04	3586.77	3585.63	3583.77	3590.59	3613.99	3597.30	3590.75	3590.57	3595.61	3589.16	3589.04	3588.90	3588.92	N/A	N/A
04/19/05	3586.28	3585.59	3583.69	3590.55	3614.31	3597.51	3590.67	3590.61	3595.76	3588.88	3589.00	3588.98	3588.92	N/A	N/A
09/16/05	3586.17	3585.59	3583.63	3590.47	3614.77	3597.38	3590.58	3590.45	3595.56	3588.86	3588.90	3588.86	3588.80	3592.11	3597.41
10/17/05	3586.09	3585.52	3583.53	3590.41	3614.58	3597.20	3590.51	3590.40	3595.34	3588.69	3588.84	3588.79	3588.68	N/A	N/A
11/18/05	3586.23	3585.48	3585.49	3590.34	3614.36	3597.11	3590.44	3590.31	3595.19	3588.76	3588.79	3588.73	3588.68	3591.91	3597.22
11/29/05	3586.37	3585.43	3583.44	3590.33	3614.25	3597.10	3590.39	3590.31	3595.12	3588.76	3588.72	3588.64	3588.90	3591.89	3597.22

APPENDIX 4C

Site Plan with Boring Locations

Key to Logs of Borings

2005 Logs of Borings B-201 through B-204

1999 Logs of Borings PP-8 through PP-12

1999 Monitoring Wells MW-10 through MW-13

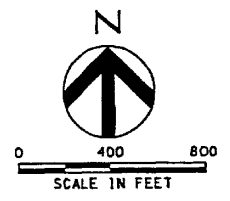
1994 Logs of Borings TB-1 through TB-2

1994 Monitoring Well MW-1 through MW-6

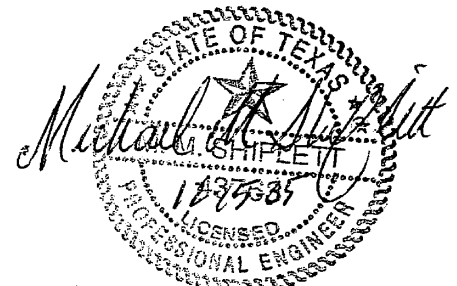
1994 Logs of Borings PZ-1 through PZ-3 (MW 7 – MW-9)

1979 Logs of Borings No. 1 through No. 4

1975 Logs of Borings No. 1 through No. 15



- LEGEND**
- PERMIT BOUNDARY
 - MW-1 ◊ MONITORING WELL LOCATIONS
 - B-07 △ 1975 BORING LOCATIONS
 - UV-1 ⊕ UTILITY VENT LOCATIONS
 - TB-1 △ 1994 BORING LOCATIONS
 - B-202 △ 2005 BORING LOCATIONS
 - PP-11 ⊞ PERIMETER PROBE LOCATIONS



For Borings 201, 202, 203 & 204 only

- NOTES:**
1. THE PROPOSED GRADES REPRESENT THE FINAL CONTOURS.
 2. TOPOGRAPHIC MAP WAS COMPILED BY PHOTOGRAMMETRIC METHODS BY STEWART GEO TECHNOLOGIES, SAN ANTONIO, TEXAS FROM AERIAL PHOTOGRAPHY DATED APRIL 15, 2004. VERTICAL DATUM BASED ON NGVD 29. MAPPING GROUND CONTROL PROVIDED BY THE CITY OF AMARILLO, COMPLETED IN ACCORDANCE WITH NATIONAL MAP ACCURACY STANDARDS.
 3. PROPERTY BOUNDARY INFORMATION BASED ON BOUNDARY SURVEY DATA PROVIDED BY THE CITY OF AMARILLO.
 4. LOCATIONS OF 1979 BORINGS UNKNOWN.

DATE: 2/15/2005
 TIME: 10:03:31 AM
 FILE: \\V79666\mcdavison\AM1104.01.DGN

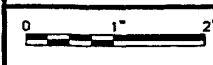


ISSUE	DATE	DESCRIPTION

PROJECT MANAGER	M. DAVISON
CIVIL ENGINEER	M. DAVISON
CHECKED BY	M. ODEN
DESIGNED	S. MILLER
DRAWN BY	B. GREEN
QA/QC	M. ODEN
PROJECT NUMBER	23358-037

**CITY OF AMARILLO LANDFILL
MSW PERMIT NO. 73A
POTTER COUNTY, TEXAS**

BORING LOCATION MAP



FILENAME: ...AM1104.01.DGN
SCALE: _____

SHEET
PLATE 1, APP 4C

2005 – Kleinfelder

Key to Logs of Borings

Logs of Borings B-201 through B-204

KEY TO LOGS OF BORINGS

DRILLING AND SAMPLING SYMBOLS AND TERMS:

- | | |
|---|---|
| <p><input type="checkbox"/> Thin-Walled Tube Sample</p> <p><input type="checkbox"/> Auger Sample/Drilling</p> <p><input type="checkbox"/> Split Spoon Sample and Standard Penetration Test</p> <p><input type="checkbox"/> Continuous Core Sample</p> | <p><input checked="" type="checkbox"/> TxDOT Cone Penetrometer Test</p> <p><input type="checkbox"/> Bag Sample</p> <p><input type="checkbox"/> Water Level Initial Measurement</p> <p><input type="checkbox"/> Water Level Subsequent Measurement</p> |
|---|---|

- Hand Penetrometer : An indicator of fine-grained soils consistency. Reported as tons per square foot, tsf.
- Penetration : An indicator of soil and rock density and consistency, and correlates to the soil strength. Reported as N = blows/6 inches unless otherwise indicated.
- Core Recovered : Length of rock core recovered as a percent of the total continuous core sample length.
- RQD : Rock Quality Designation. A measure of the integrity of the continuous core sample recovered. Reported as the percentage of core recovered in pieces greater than 4 inches in length.

RELATIVE DENSITY OF COARSE-GRAINED SOILS:		CONSISTENCY OF FINE-GRAINED SOILS:	
Penetration Resistance Blows/foot	Relative Density	Hand Penetrometer Readings, tsf	Consistency
0-4	Very Loose	<1	Soft
4-10	Loose	1-2	Firm
10-30	Medium Dense	2-3	Stiff
30-50	Dense	3-4	Very Stiff
over 50	Very Dense	>4.0	Hard

TERMS CHARACTERIZING SOIL STRUCTURE:

- Slickensided : Having inclined planes of weakness that are slick and glossy in appearance.
- Fissured : Containing shrinkage cracks; usually more or less vertical
- Laminated : Composed of thin layers of varying color and texture.
- Interbedded : Composed of alternate layers of different soil types.
- Calcareous : Containing appreciable quantities of calcium carbonate.
- Well graded : Having wide range in grain sizes and substantial amounts of all intermediate particle sizes.
- Poorly graded : Predominantly one grain size, or having some intermediate size missing.

NOTE: Slickensided and fissured clays may have lower unconfined compressive strengths because of planes of weakness or cracks in the soil. The consistency rating of such soils are based on penetrometer readings.

DEGREE OF WEATHERING:

- Unweathered : Rock in its natural state before being exposed to weathering agents.
- Slightly weathered : Noted predominantly by color change with no disintegrated zones.
- Weathered : Complete color change with zones of slightly decomposed rock.
- Severely weathered : Complete color change with consistency, texture, and general appearance approaching soil.

SUBSURFACE CONDITIONS:

Soil and rock descriptions on the boring logs are a compilation from field data as well as from laboratory test results. The stratification lines represent the approximate boundary between materials and the actual transition can be gradual.

Water level observations have been made in the borings at the times indicated. Note that fluctuations in groundwater level(s) may occur due to variations in rainfall, hydraulic conductivity of soil strata, construction activity, and other factors.

LOG OF BORING NO. B-201

Project Description: **Amarillo Municipal Landfill - Potter County, Texas**
 Location: **See Plan of Borings, Plate 1 Appendix 4C**
 Approx. Surface Elevation: **3724'**

Depth	Symbol/USCS	Samples	Hand Penetrometer, tsf	Penetration (1st Drive)	Penetration (2nd Drive)	Core Drilled, ft.	Core Recovered, %	MATERIAL DESCRIPTION	Liquid Limit	Plastic Limit	Plasticity Index	% Passing No. 200 Sieve	Moisture Content, %	Unit Dry Weight, pcf	Unc. Compressive Strength, tsf	Strain at Failure, %
								SILTY CLAYEY GRAVEL, light red-brown, dense, fragmented caliche, moderately cemented, with caliche (FILL) EL 3720.8: 3.5	17	15	2	30	8			
5			33	50/5½"		5.0	20	CEMENTED SAND, calcareous, red-brown and light red-brown, very hard, moderately cemented, jointed, shaly, with dissolution cavities EL 3717.8: 6.5								
								SILTY CLAY, light red-brown EL 3716.8: 7.5								
								CALICHE, very light brown, dense EL 3715.8: 8.5								
10			50/3"	50/2"		5.0	0	CLAYEY SILT, light red-brown, stiff EL 3712.8: 11.5								
								CALICHE, very light red-brown, silt with sand, weakly to moderately cemented EL 3710.8: 13.5								
15			50/4¾"			5.0	22	CEMENTED SAND, light red-brown, hard, highly cemented, vuggy, with dense silty sand seams EL 3708.3: 16.0	25	25	NP	4	12			
20						5.0	18	CLAYEY SAND, silty, light red-brown, very dense, with weakly cemented vuggy sandstone seams, fine to medium, subrounded to subangular, frosted								
25			32	46		3.5	3									
30			49	50/4½"		3.5	51	- weakly cemented for approximately 1 foot for every 5 feet				15	10			
35						3.5	0									
40												5	2			

continued on next page

Completion Depth: 76.5 ft.
 Date Boring Started: 6/7/05
 Date Boring Completed: 6/8/05
 Logged by: D. James
 Project No.: 57815

Remarks: Boring advanced using air as drilling circulation medium. Boring dry upon completion. Boring backfilled with hydrated bentonite upon completion of the drilling and sampling.



Stratification lines represent approximate strata boundaries, as in-situ the transitions may be gradual. This Log of Boring is not intended for bidding or estimating purposes. Boring log(s) should not be reproduced separately from the engineering report unless said report is specifically included by reference.

LOG OF BORING NO. B-201 (cont'd)

Project Description: **Amarillo Municipal Landfill - Potter County, Texas**
 Location: See Plan of Borings, Plate 1 Appendix 4C
 Approx. Surface Elevation: 3724'

Depth	Symbol/USCS	Samples	Hand Penetrometer, tsf	Penetration (1st Drive)	Penetration (2nd Drive)	Core Drilled, ft.	Core Recovered, %	MATERIAL DESCRIPTION	Liquid Limit	Plastic Limit	Plasticity Index	% Passing No. 200 Sieve	Moisture Content, %	Unit Dry Weight, pcf	Unc. Compressive Strength, tsf	Strain at Failure, %	
45						3.5	29	- increasing weakly cemented sandstone, vuggy, with moderately cemented caliche accretions El. 3679.3; 45.0									
50				50/ 4 3/4"		3.5	69	CEMENTED SAND, light red-brown, moderately hard, moderately cemented, calcareous, with moderately dense sand infilled cavities, intercalated with uncemented sand layers, with caliche accretions, fine to medium, frosted, subangular to subrounded									
55				50/ 5"		4.0	48										
60						5.0	46		- with clayey sand partings and seams				12	113	13.6	1.1	
65						5.0	36										
70						4.0	18	- with clayey sand seams				3	12	114	33.7	1.1	
75						5.0	40	- less cemented below 70 feet									
75					41	47											

Completion Depth: 76.5 ft.
 Date Boring Started: 6/7/05
 Date Boring Completed: 6/8/05
 Logged by: D. James
 Project No.: 57815

Remarks: Boring advanced using air as drilling circulation medium. Boring dry upon completion. Boring backfilled with hydrated bentonite upon completion of the drilling and sampling.



Stratification lines represent approximate strata boundaries, as in-situ the transitions may be gradual. This Log of Boring is not intended for bidding or estimating purposes. Boring log(s) should not be reproduced separately from the engineering report unless said report is specifically included by reference.

LOG OF BORING NO. B-202

Project Description: **Amarillo Municipal Landfill - Potter County, Texas**
 Location: **See Plan of Borings, Plate 1 Appendix 4C**
 Approx. Surface Elevation: **3728'**

Depth	Symbol/USCS	Samples	Hand Penetrometer, tsf	Penetration (1st Drive)	Penetration (2nd Drive)	Core Drilled, ft.	Core Recovered, %	MATERIAL DESCRIPTION	Liquid Limit	Plastic Limit	Plasticity Index	% Passing No. 200 Sieve	Moisture Content, %	Unit Dry Weight, pcf	Unc. Compressive Strength, tsf	Strain at Failure, %	
3.1								SANDY CLAY, light red-brown, very stiff, calcareous, with calcareous accretions, with magnesium oxide stains, with root filament holes, silty	33	14	19	52	12				
3.0																	
5			50/1 1/2"			5.0	36	CEMENTED SAND, calcareous, light red-brown and light brown, very hard, moderately cemented				5	118	12.5	1.8		
								SILTY CALICHE with sand, very light brown, very hard, moderately cemented									
								CEMENTED SAND, very light brown to light red-brown, moderately hard, highly cemented, with caliche, fine to medium, subangular to subrounded, frosted, silty									
10						5.0	44										
15			50/3"			4.5	62					7	108	23.1	0.7		
20						5.0	2	- less cemented below 20 1/2 feet									
25			37	41		3.5	31	CLAYEY SAND, silty, light red-brown with very light brown, very dense to dense, fine to medium, well graded, subangular to subrounded, frosted				20	6				
30						3.5	0	- weakly cemented with caliche from 27 to 29 feet									
35			18	21		3.5	0	- dense				32	13				
40			24	50/5"				- weakly cemented at 38 feet									
								- very dense below 41 feet									

continued on next page

Completion Depth: 81.5 ft.
 Date Boring Started: 6/8/05
 Date Boring Completed: 6/9/05
 Logged by: D. James
 Project No.: 57815

Remarks: Boring advanced using air as drilling circulation medium. Boring dry upon completion. Boring backfilled with hydrated bentonite upon completion of the drilling and sampling.



Stratification lines represent approximate strata boundaries, as in-situ the transitions may be gradual. This Log of Boring is not intended for bidding or estimating purposes. Boring log(s) should not be reproduced separately from the engineering report unless said report is specifically included by reference.

LOG OF BORING NO. B-202 (cont'd)

Project Description: **Amarillo Municipal Landfill - Potter County, Texas**
 Location: **See Plan of Borings, Plate 1 Appendix 4C**
 Approx. Surface Elevation: **3728'**

Depth	Symbol/USCS	Samples	Hand Penetrometer, tsf	Penetration (1st Drive)	Penetration (2nd Drive)	Core Drilled, ft.	Core Recovered, %	MATERIAL DESCRIPTION	Liquid Limit	Plastic Limit	Plasticity Index	% Passing No. 200 Sieve	Moisture Content, %	Unit Dry Weight, pcf	Unc. Compressive Strength, tsf	Strain at Failure, %	
45				50/ 4 1/2"		3.5	43	CEMENTED SAND, very light red-brown and red-brown, hard, moderately cemented, with caliche, intercalated with very dense sand seams, calcareous, with dense sand infilled cavities, vuggy				18	7				
						4.0	0										
50				50/ 4"		4.5	0										
55				50/ 4 1/2"													
60				45	48	4.0	0	SAND with clay, silty, light red-brown, very dense, with occasional weakly cemented sand seams and layers, calcareous accretions, fine to medium, with weakly to moderately cemented calcareous accretions, with occasional clay content				7	9				
70				47	50/ 5"												
75				50/ 5 1/2"													
80				46	50/ 4 1/2"							10	14				

EL 3672.4: 56.0

EL 3646.9: 81.5

Completion Depth: 81.5 ft.
 Date Boring Started: 6/8/05
 Date Boring Completed: 6/9/05
 Logged by: D. James
 Project No.: 57815

Remarks: Boring advanced using air as drilling circulation medium. Boring dry upon completion. Boring backfilled with hydrated bentonite upon completion of the drilling and sampling.



Stratification lines represent approximate strata boundaries, as in-situ the transitions may be gradual. This Log of Boring is not intended for bidding or estimating purposes. Boring log(s) should not be reproduced separately from the engineering report unless said report is specifically included by reference.

LOG OF BORING NO. B-203

Project Description: **Amarillo Municipal Landfill - Potter County, Texas**
 Location: **See Plan of Borings, Plate 1 Appendix 4C**
 Approx. Surface Elevation: **3763'**

Depth	Symbol/USCS	Samples	Hand Penetrometer, tsf	Penetration (1st Drive)	Penetration (2nd Drive)	Core Drilled, ft.	Core Recovered, %	MATERIAL DESCRIPTION	Liquid Limit	Plastic Limit	Plasticity Index	% Passing No. 200 Sieve	Moisture Content, %	Unit Dry Weight, pcf	Unc. Compressive Strength, tsf	Strain at Failure, %
5	●●●●							CALICHE, very light red-brown, hard, jointed, moderate to highly cemented								
10	●●●●							CLAYEY SAND, silty, light red-brown and very light brown, dense, with calcareous accretions and occasional caliche cemented sandstone seams and layers								
15	●●●●							El. 3751.1: 12.0								
20	●●●●															
25	●●●●															
30	●●●●															
35	●●●●															
40	●●●●															

continued on next page

Completion Depth: 220 ft.
 Date Boring Started: 9/7/05
 Date Boring Completed: 9/7/05
 Logged by: D. James
 Project No.: 57815

Remarks: Boring dry upon completion. Water at 169.1 feet, 20 hours after completion of drilling and sampling.



Stratification lines represent approximate strata boundaries, as in-situ the transitions may be gradual. This Log of Boring is not intended for bidding or estimating purposes. Boring log(s) should not be reproduced separately from the engineering report unless said report is specifically included by reference.

LOG OF BORING NO. B-203 (cont'd)

Project Description: **Amarillo Municipal Landfill - Potter County, Texas**
 Location: See Plan of Borings, Plate 1 Appendix 4C
 Approx. Surface Elevation: 3763'

Depth	Symbol/USCS	Samples	Hand Penetrometer, tsf	Penetration (1st Drive)	Penetration (2nd Drive)	Core Drilled, ft.	Core Recovered, %	MATERIAL DESCRIPTION	Liquid Limit	Plastic Limit	Plasticity Index	% Passing No. 200 Sieve	Moisture Content, %	Unit Dry Weight, pcf	Unc. Compressive Strength, tsf	Strain at Failure, %
45								CLAYEY SAND, silty, light red-brown and very light brown, dense, with calcareous accretions and occasional caliche cemented sandstone seams and layers								
50																
55																
60																
65																
70																
75																
80									25	21	4	13	20			

continued on next page

Completion Depth: 220 ft.
 Date Boring Started: 9/7/05
 Date Boring Completed: 9/7/05
 Logged by: D. James
 Project No.: 57815

Remarks: Boring dry upon completion. Water at 169.1 feet, 20 hours after completion of drilling and sampling.



Stratification lines represent approximate strata boundaries, as in-situ the transitions may be gradual. This Log of Boring is not intended for bidding or estimating purposes. Boring log(s) should not be reproduced separately from the engineering report unless said report is specifically included by reference.

LOG OF BORING NO. B-203 (cont'd)

Project Description: **Amarillo Municipal Landfill - Potter County, Texas**
 Location: **See Plan of Borings, Plate 1 Appendix 4C**
 Approx. Surface Elevation: **3763'**

Depth	Symbol/USCS	Samples	Hand Penetrometer, tsf	Penetration (1st Drive)	Penetration (2nd Drive)	Core Drilled, ft.	Core Recovered, %	MATERIAL DESCRIPTION	Liquid Limit	Plastic Limit	Plasticity Index	% Passing No. 200 Sieve	Moisture Content, %	Unit Dry Weight, pcf	Unc. Compressive Strength, tsf	Strain at Failure, %	
85								CLAYEY SAND, silty, light red-brown and very light brown, dense, with calcareous accretions and occasional caliche cemented sandstone seams and layers									
90																	
95																	
100													16	38			
105																	
110																	
115																	
120																	
125																	

continued on next page

Completion Depth: 220 ft.
 Date Boring Started: 9/7/05
 Date Boring Completed: 9/7/05
 Logged by: D. James
 Project No.: 57815

Remarks: Boring dry upon completion. Water at 169.1 feet, 20 hours after completion of drilling and sampling.



Stratification lines represent approximate strata boundaries, as in-situ the transitions may be gradual. This Log of Boring is not intended for bidding or estimating purposes. Boring log(s) should not be reproduced separately from the engineering report unless said report is specifically included by reference.

LOG OF BORING NO. B-203 (cont'd)

Project Description: **Amarillo Municipal Landfill - Potter County, Texas**
 Location: **See Plan of Borings, Plate 1 Appendix 4C**
 Approx. Surface Elevation: **3763'**

Depth	Symbol/USCS	Samples	Hand Penetrometer, tsf	Penetration (1st Drive)	Penetration (2nd Drive)	Core Drilled, ft.	Core Recovered, %	MATERIAL DESCRIPTION	Liquid Limit	Plastic Limit	Plasticity Index	% Passing No. 200 Sieve	Moisture Content, %	Unit Dry Weight, pcf	Unc. Compressive Strength, tsf	Strain at Failure, %	
130 135 140 145 150 155 160 165								<p>CLAYEY SAND, silty, light red-brown and very light brown, dense, with calcareous accretions and occasional caliche cemented sandstone seams and layers</p> <p>- moderate to highly cemented from 155 to 162 feet</p> <p>- coarse to medium, subrounded, frosted, gap graded to well graded, yellow-brown, less cemented to non-cemented below 162 feet</p>									

continued on next page

Completion Depth: 220 ft.
 Date Boring Started: 9/7/05
 Date Boring Completed: 9/7/05
 Logged by: D. James
 Project No.: 57815

Remarks: Boring dry upon completion. Water at 169.1 feet, 20 hours after completion of drilling and sampling.



Stratification lines represent approximate strata boundaries, as in-situ the transitions may be gradual. This Log of Boring is not intended for bidding or estimating purposes. Boring log(s) should not be reproduced separately from the engineering report unless said report is specifically included by reference.

LOG OF BORING NO. B-203 (cont'd)

Project Description: **Amarillo Municipal Landfill - Potter County, Texas**
 Location: **See Plan of Borings, Plate 1 Appendix 4C**
 Approx. Surface Elevation: **3763'**

Depth	Symbol/USCS	Samples	Hand Penetrometer, tsf	Penetration (1st Drive)	Penetration (2nd Drive)	Core Drilled, ft.	Core Recovered, %	MATERIAL DESCRIPTION	Liquid Limit	Plastic Limit	Plasticity Index	% Passing No. 200 Sieve	Moisture Content, %	Unit Dry Weight, pcf	Unc. Compressive Strength, tsf	Strain at Failure, %	
170								CLAYEY SAND, silty, light red-brown and very light brown, dense, with calcareous accretions and occasional caliche cemented sandstone seams and layers - with occasional fine rounded gravel below 212 feet									
175																	
180																	
185																	
190																	
195																	
200																	
205																	
210																	

continued on next page

Completion Depth: 220 ft.
 Date Boring Started: 9/7/05
 Date Boring Completed: 9/7/05
 Logged by: D. James
 Project No.: 57815

Remarks: Boring dry upon completion. Water at 169.1 feet, 20 hours after completion of drilling and sampling.



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LOG OF BORING NO. B-203 (cont'd)

Project Description: **Amarillo Municipal Landfill - Potter County, Texas**
 Location: See Plan of Borings, Plate 1 Appendix 4C
 Approx. Surface Elevation: 3763'

Depth	Symbol/USCS	Samples	Hand Penetration, tsf	Penetration (1st Drive)	Penetration (2nd Drive)	Core Drilled, ft.	Core Recovered, %	MATERIAL DESCRIPTION	Liquid Limit	Plastic Limit	Plasticity Index	% Passing No. 200 Sieve	Moisture Content, %	Unit Dry Weight, pcf	Unc. Compressive Strength, tsf	Strain at Failure, %	
	[Symbol: Dotted pattern]							CLAYEY SAND, silty, light red-brown and very light brown, dense, with calcareous accretions and occasional caliche cemented sandstone seams and layers El. 3549.1: 214.0									
215	[Symbol: Horizontal lines]							SHALE, red-brown and light green-gray, very stiff to hard, weathered El. 3543.1: 220.0									
220																	

Completion Depth: 220 ft.
 Date Boring Started: 9/7/05
 Date Boring Completed: 9/7/05
 Logged by: D. James
 Project No.: 57815

Remarks: Boring dry upon completion. Water at 169.1 feet, 20 hours after completion of drilling and sampling.



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LOG OF BORING NO. B-204

Project Description: **Amarillo Municipal Landfill - Potter County, Texas**
 Location: See Plan of Borings, Plate 1 Appendix 4C
 Approx. Surface Elevation: 3680'

Depth	Symbol/USCS	Samples	Hand Penetrometer, tsf	Penetration (1st Drive)	Penetration (2nd Drive)	Core Drilled, ft.	Core Recovered, %	MATERIAL DESCRIPTION	Liquid Limit	Plastic Limit	Plasticity Index	% Passing No. 200 Sieve	Moisture Content, %	Unit Dry Weight, pcf	Unc. Compressive Strength, tsf	Strain at Failure, %
5								SAND with gravel, silty, light red-brown and yellow-brown, calcareous accretions and caliche fragments, fine to medium, gap to well graded								
10																
15																
20								- with occasional weakly to moderately cemented calcareous sandstone seams and layers below 18 feet	22	16	6	9	12			
25																
30																
35																
40								SAND, yellow-brown, dense, fine to medium, gap to well graded, frosted, subrounded, with occasional caliche seams								

El. 3644.8: 35.0'

continued on next page

Completion Depth: 135 ft.
 Date Boring Started: 9/8/05
 Date Boring Completed: 9/8/05
 Logged by: D. James
 Project No.: 57815

Remarks: Boring dry upon completion. Water at 81.6 feet, 1 hour after completion of drilling and sampling.



Stratification lines represent approximate strata boundaries, as in-situ the transitions may be gradual. This Log of Boring is not intended for bidding or estimating purposes. Boring log(s) should not be reproduced separately from the engineering report unless said report is specifically included by reference.

LOG OF BORING NO. B-204 (cont'd)

Project Description: **Amarillo Municipal Landfill - Potter County, Texas**
 Location: **See Plan of Borings, Plate 1 Appendix 4C**
 Approx. Surface Elevation: **3680'**

Depth	Symbol/USCS	Samples	Hand Penetrometer, tsf	Penetration (1st Drive)	Penetration (2nd Drive)	Core Drilled, ft.	Core Recovered, %	MATERIAL DESCRIPTION	Liquid Limit	Plastic Limit	Plasticity Index	% Passing No. 200 Sieve	Moisture Content, %	Unit Dry Weight, pcf	Unc. Compressive Strength, tsf	Strain at Failure, %	
45								SAND, yellow-brown, dense, fine to medium, gap to well graded, frosted, subrounded, with occasional caliche seams									
50																	
55																	
60													4	22			
65																	
70																	
75									- moderately cemented sandstone from 74 to 75 feet								
80									- with trace clay								

continued on next page

Completion Depth: 135 ft.
 Date Boring Started: 9/8/05
 Date Boring Completed: 9/8/05
 Logged by: D. James
 Project No.: 57815

Remarks: Boring dry upon completion. Water at 81.6 feet, 1 hour after completion of drilling and sampling.



Stratification lines represent approximate strata boundaries, as in-situ the transitions may be gradual. This Log of Boring is not intended for bidding or estimating purposes. Boring log(s) should not be reproduced separately from the engineering report unless said report is specifically included by reference.

LOG OF BORING NO. B-204 (cont'd)

Project Description: **Amarillo Municipal Landfill - Potter County, Texas**
 Location: **See Plan of Borings, Plate 1 Appendix 4C**
 Approx. Surface Elevation: **3680'**

Depth	Symbol/USCS	Samples	Hand Penetrometer, tsf	Penetration (1st Drive)	Penetration (2nd Drive)	Core Drilled, ft.	Core Recovered, %	MATERIAL DESCRIPTION	Liquid Limit	Plastic Limit	Plasticity Index	% Passing No. 200 Sieve	Moisture Content, %	Unit Dry Weight, pcf	Unc. Compressive Strength, tsf	Strain at Failure, %
85								SAND, yellow-brown, dense, fine to medium, gap to well graded, frosted, subrounded, with occasional caliche seams								
90																
95																
100																
105								- with occasional fine gravel below 105 feet								
110																
115																
120																
125								GRAVELLY SAND, variegated, dense								

continued on next page

Completion Depth: 135 ft.
 Date Boring Started: 9/8/05
 Date Boring Completed: 9/8/05
 Logged by: D. James
 Project No.: 57815

Remarks: Boring dry upon completion. Water at 81.6 feet, 1 hour after completion of drilling and sampling.



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LOG OF BORING NO. B-204 (cont'd)

Project Description: **Amarillo Municipal Landfill - Potter County, Texas**
 Location: **See Plan of Borings, Plate 1 Appendix 4C**
 Approx. Surface Elevation: **3680'**

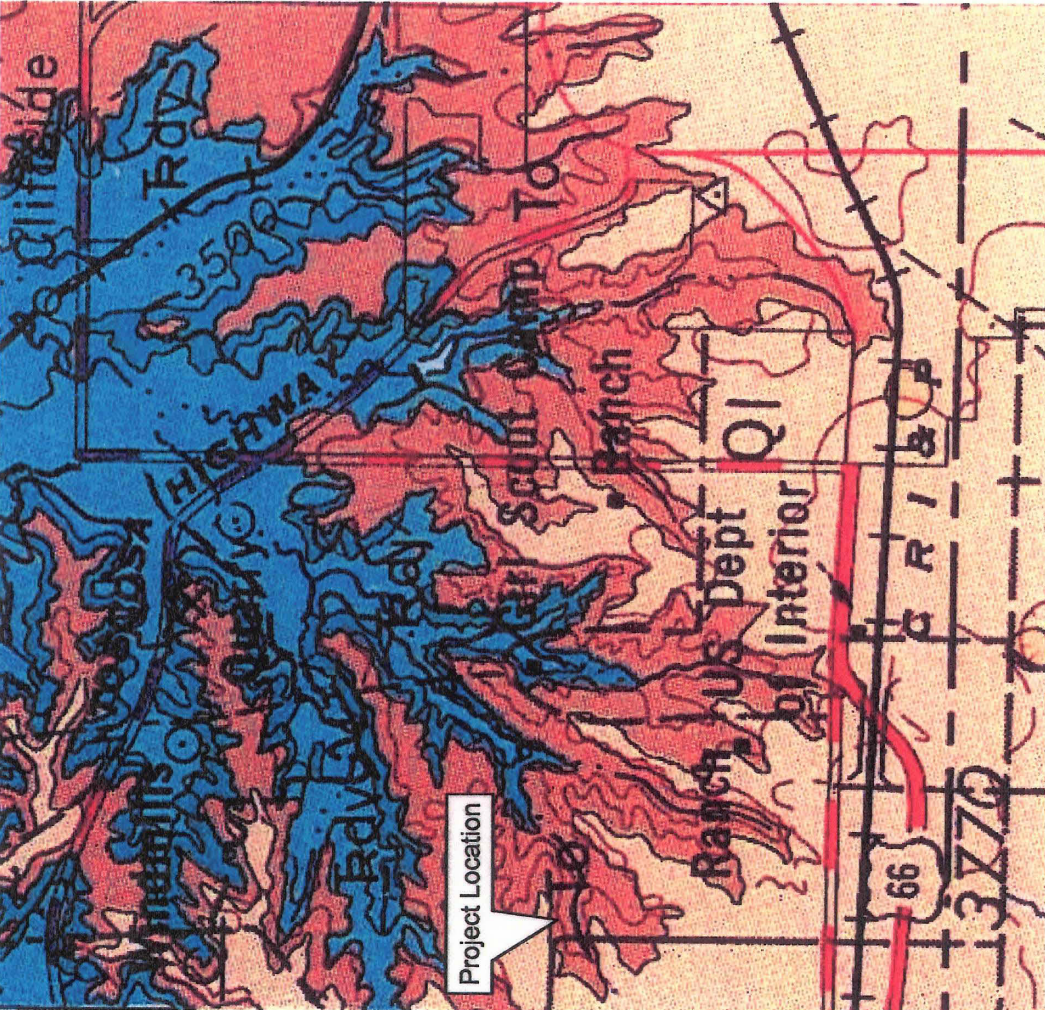
Depth	Symbol/USCS	Samples	Hand Penetrometer, tsf	Penetration (1st Drive)	Penetration (2nd Drive)	Core Drilled, ft.	Core Recovered, %	MATERIAL DESCRIPTION	Liquid Limit	Plastic Limit	Plasticity Index	% Passing No. 200 Sieve	Moisture Content, %	Unit Dry Weight, pcf	Unc. Compressive Strength, tsf	Strain at Failure, %
								GRAVELLY SAND, variegated, dense El. 3552.8; 127.0'								
130								SHALE, red-brown, and light green-gray, very stiff to hard								
135								El. 3544.8; 135.0'								

Completion Depth: 135 ft.
 Date Boring Started: 9/8/05
 Date Boring Completed: 9/8/05
 Logged by: D. James
 Project No.: 57815

Remarks: Boring dry upon completion. Water at 81.6 feet, 1 hour after completion of drilling and sampling.



Stratification lines represent approximate strata boundaries, as in-situ the transitions may be gradual. This Log of Boring is not intended for bidding or estimating purposes. Boring log(s) should not be reproduced separately from the engineering report unless said report is specifically included by reference.



Q1
Lenses

To

Windblown silt

Ogallala Formation

Sand, silt, clay, gravel, and calcic. Sand, fine to coarse-grained quartz, silty in part, calcic nodules locally, cemented locally by calcite and by siliceous, locally cross-bedded, various shades of gray, brown, and red. Minor silt and clay with calcic nodules, sandy in places, massive, white, gray, olive-green, brown, red, and maroon. Gravel, not everywhere present, composed of pebbles and cobbles of quartz, quartzite, minor chert, igneous rock, metamorphic rock, limestone, clay balls in lower part, and abraded Gryphaea in interformational channel deposits and in basal conglomerate. Calcic, not everywhere present, sandy, plioisitic, white, gray, pink, comprises four or five beds up to 12 feet thick in upper part, forms ledges and caprock. Maximum thickness 550 feet, thins westward. (Locally includes Ogallala sand which has moved downslope covering older formations)



Dockum Group undivided and Trujillo and Tecosus Formations

Dockum Group undivided, Trj, in Palo Duro Canyon. Thickness 550 feet. (Elsewhere Dockum is divided into Trujillo and Tecosus Formations.)
 Trujillo Formation, Trj, conglomerate, sandstone, and shale. Conglomerate, sandy, composed of granules and pebbles of quartz, limestone, sandstone, siltstone, minor chert, and fragments of petrified wood, massive, gray, brown. Sandstone, conglomeratic, fine to coarse grains of quartz and limestone, micaceous, calcareous locally, cross-bedded to massive, gray, greenish gray, and brown. Shale, micaceous, occurs as thin interbeds, gray and red.
 Tecosus Formation, Tec, shale, clay, siltstone, and sand. Shale, clay, and siltstone, sandy in places, micaceous, calcareous locally, reddish brown, various shades of red, maroon, gray, greenish gray, yellow, and purple. Sand, fine to medium-grained quartz, locally large, petrified logs, unconsolidated, massive, lenticular, white, and light gray. Thickness 275 feet, truncated eastward

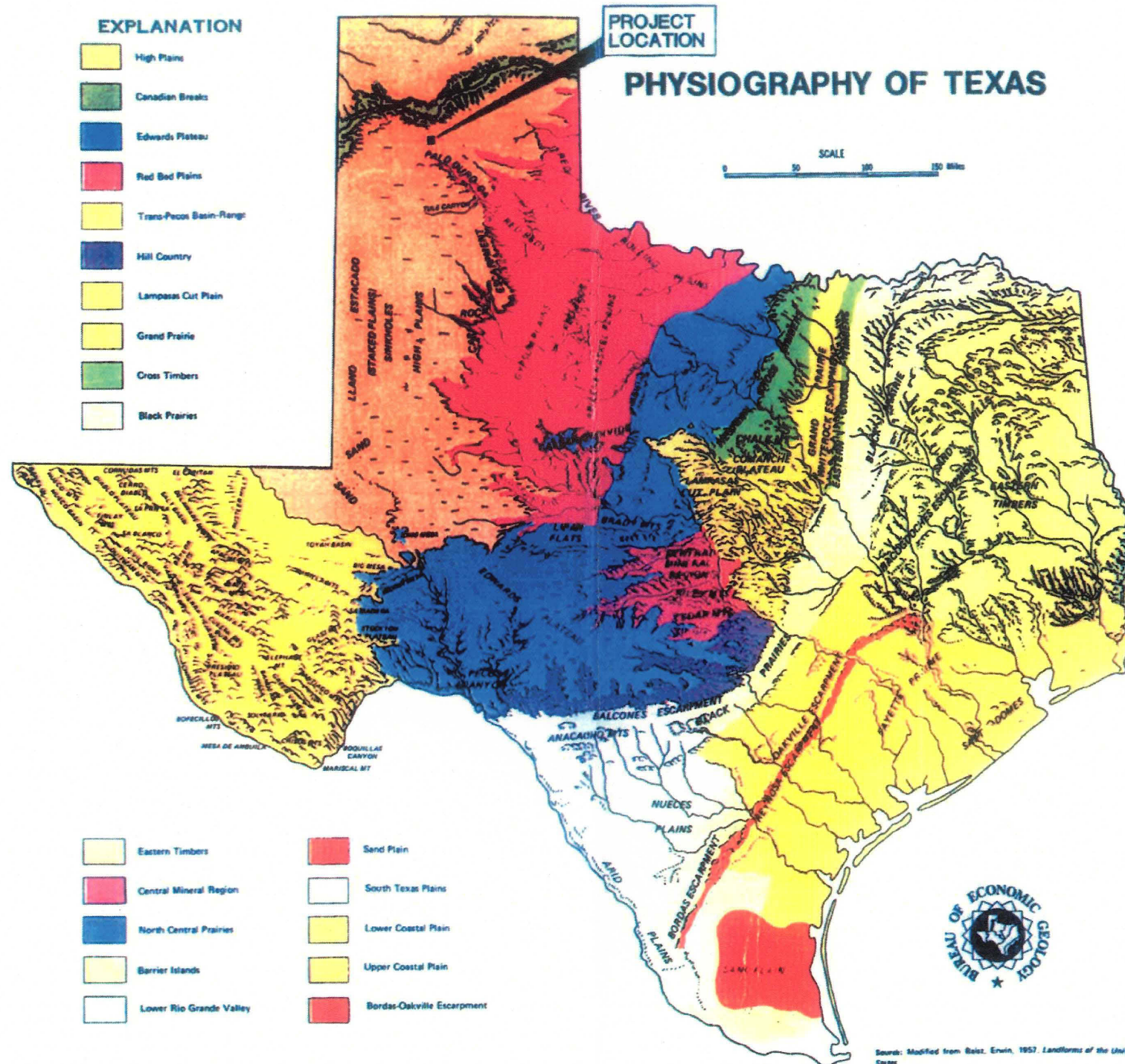
Not to scale

KLEINFELDER

GEOLOGICAL MAP
 City of Amarillo Landfill
 MSW Permit No. 73
 Potter County, Texas
 Project 57815 April 2006

Project Manager
T. MOTHKISS
Designed
HDR
Drafted
HDR
Checked

Project Number
06625-015-037
Date
NOVEMBER, 1994
Issue

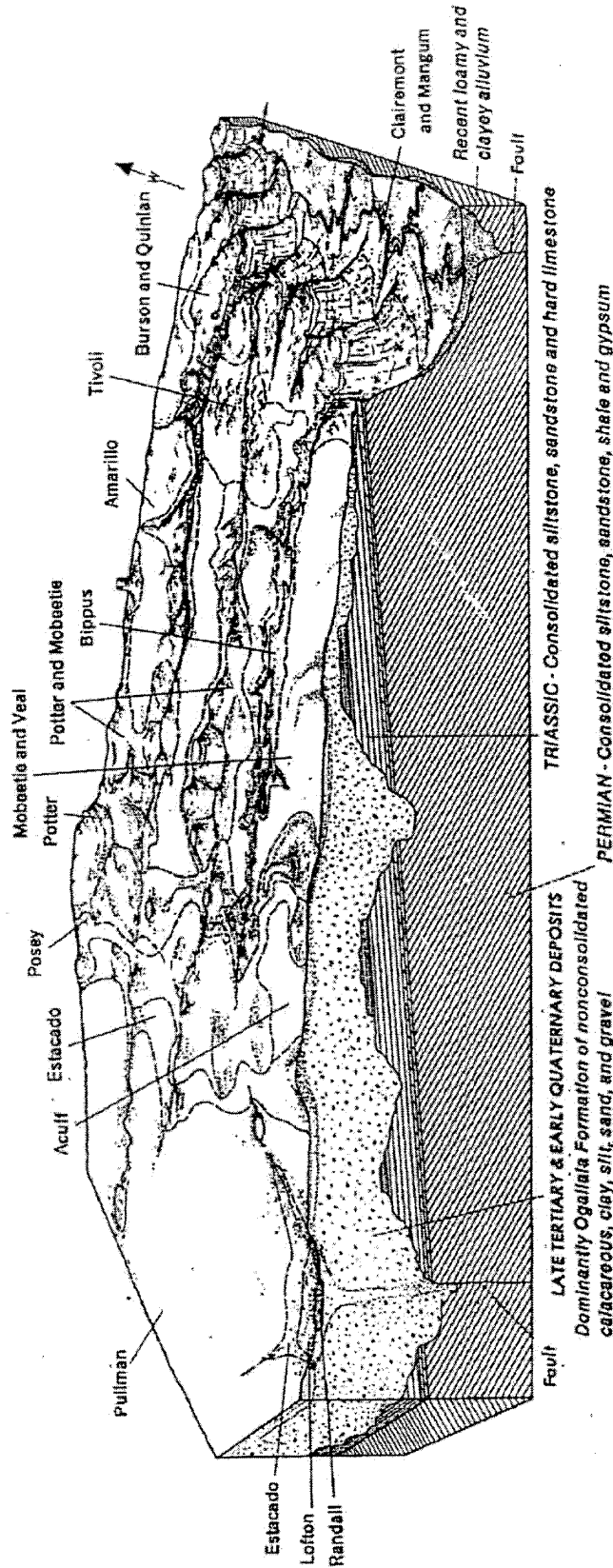




HDR Engineering, Inc.

CITY OF AMARILLO, TEXAS
MUNICIPAL LANDFILL

DISTRIBUTION OF SOIL TYPES

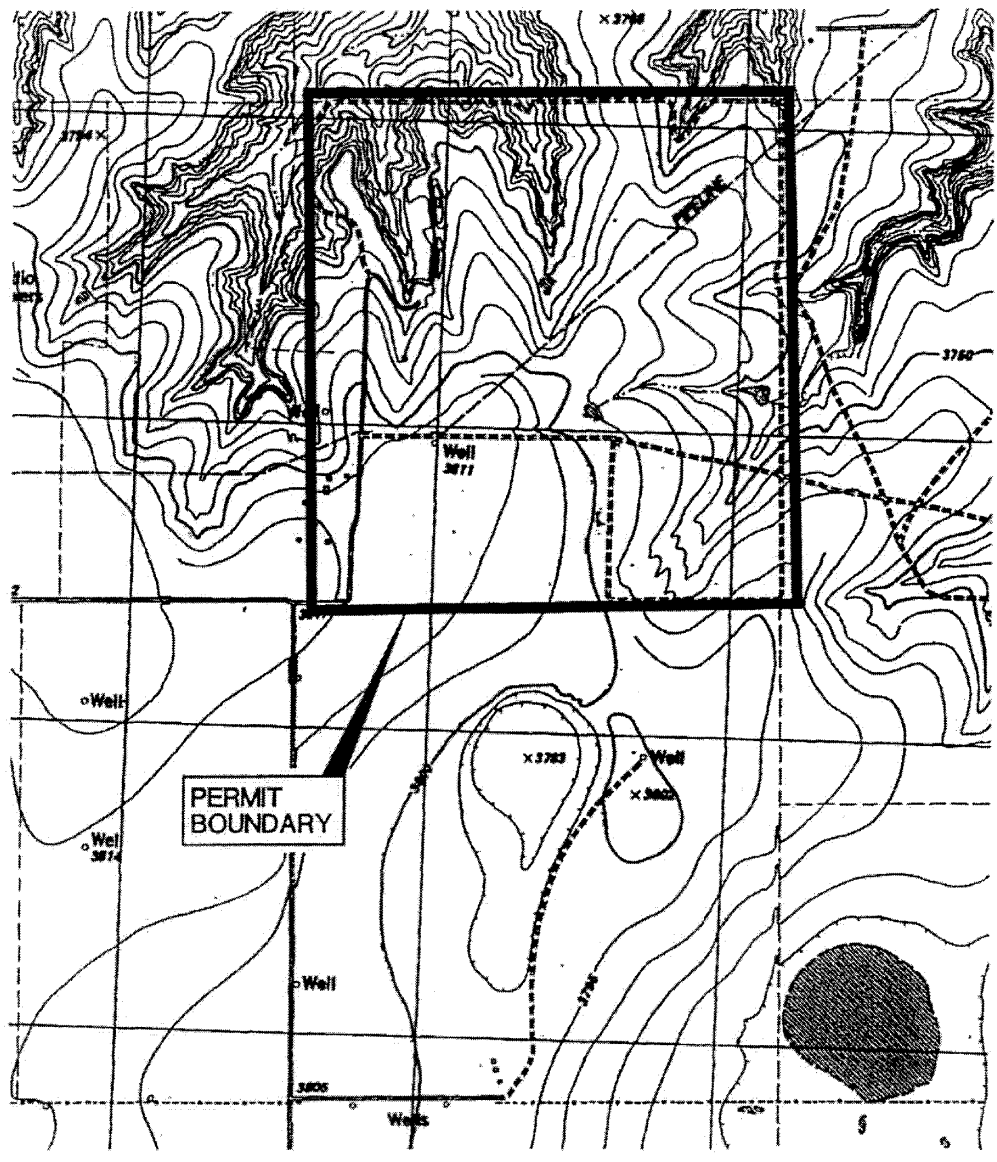
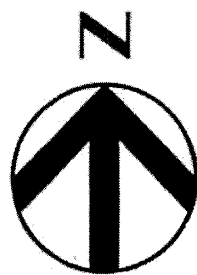


Pattern of soils in Potter County.

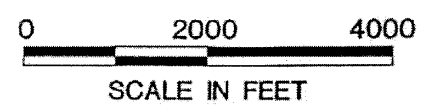
MAP SOURCE:
UNITED STATES DEPARTMENT OF AGRICULTURE
SOIL CONSERVATION SERVICE
SOIL SURVEY OF POTTER COUNTY, FEBRUARY, 1980

Date
11/94

Figure
4



MAP SOURCE:
USGS 7.5 MINUTE QUADRANGLE, BUSHLAND, TEXAS, 1984



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CITY OF AMARILLO, TEXAS
MUNICIPAL LANDFILL

TOPOGRAPHIC MAP

Date	11/94
Figure	5

FILENAME: E:\AMARILLO\DWG\AMATOPO

System	Series	Formation or Group	Thickness (feet)	Lithologic Description	Water Supply
Quaternary	Recent		0-15	Chiefly Windblown sand and silt.	Yields no water to wells. Sandy areas form excellent recharge facilities.
	Pleistocene		0-144	Sand, clay, diatomaceous earth, volcanic ash, limestone.	Mostly above water table. Does not yield large supplies.
Tertiary	Pliocene	Ogallala Formation	0-500	Fine to coarse sand and gravel; clay, silt, and caliche.	Yields large supplies of water throughout the Southern High Plains
Cretaceous		Not present in Amarillo area.	Unconformity		
Triassic		Dockum Group Tecovas Formation Santa Rosa sandstone Chinle Formation equivalent	150-1800+	Varicolored shale and sandy shale, gray or brown crossbedded sandstone and conglomerate.	Probably capable of yielding small to moderate supplies of water; most of the water is at least slightly saline.
Permian		Not present in Amarillo area.			

REFERENCE:
 SENI, S.J.
 SAND-BODY GEOMETRY AND
 DEPOSITIONAL SYSTEMS,
 OGALLALA FORMATION, TEXAS
 REPORT NO. 105, 1980



HDR Engineering, Inc.

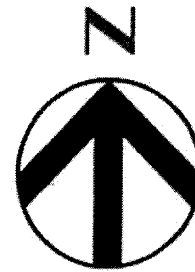
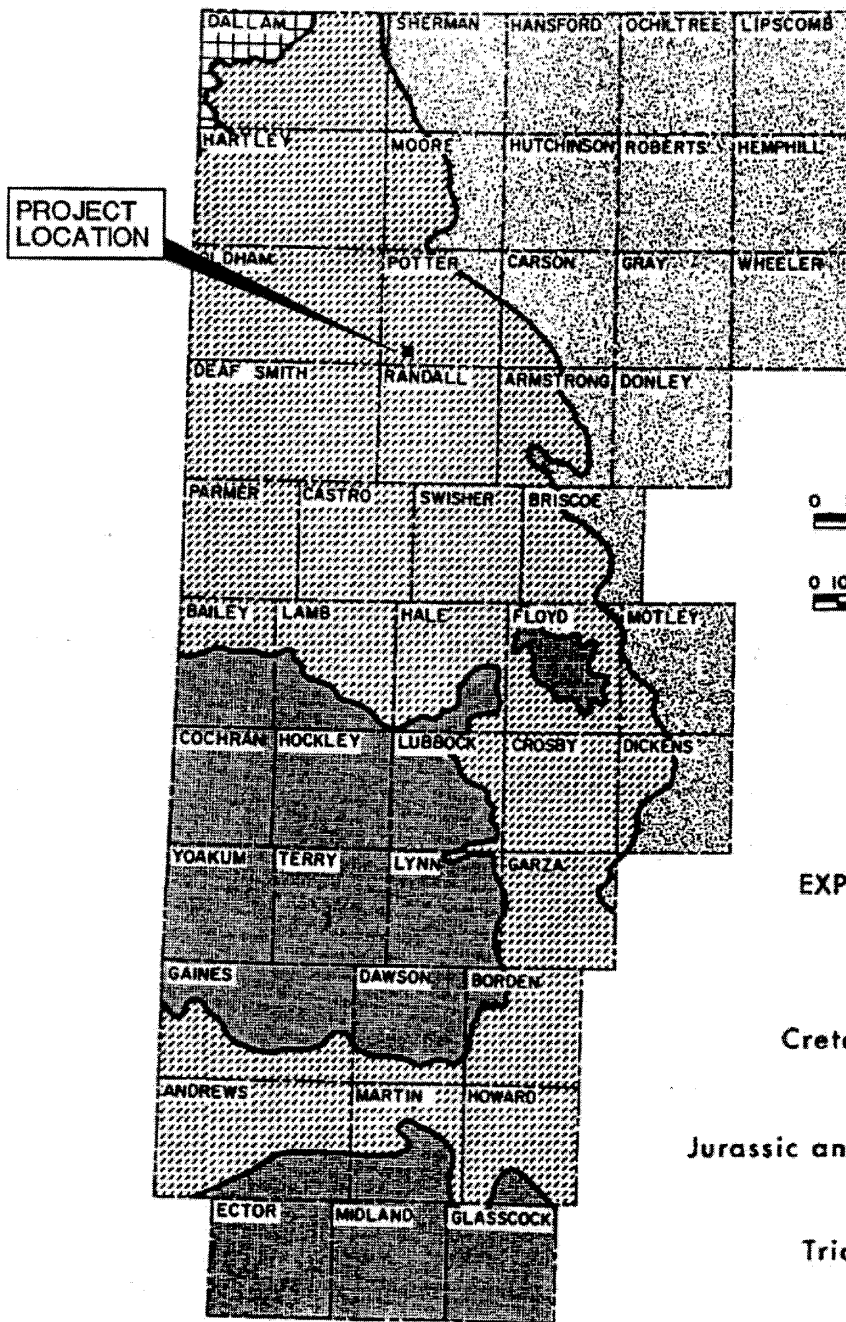
CITY OF AMARILLO, TEXAS
 MUNICIPAL LANDFILL

GENERALIZED STRATIGRAPHY

Date
 11/94

Figure
 7





FILENAME: E:\AMARILLO\DWG\AMAFIG2



0 10 20 30 40 50 60 70 Miles

0 10 30 50 70 Kilometers

EXPLANATION

-  Cretaceous rocks
-  Jurassic and Cretaceous rocks
-  Triassic rocks
-  Permian rocks

MAP SOURCE:
 EVALUATING THE GROUNDWATER RESOURCES OF THE HIGH PLAINS OF TEXAS,
 REPORT 288, VOL. I, MAY, 1984.
 TEXAS DEPARTMENT OF WATER RESOURCES



HDR Engineering, Inc.

CITY OF AMARILLO, TEXAS
 MUNICIPAL LANDFILL
 GEOLOGIC UNITS UNDERLYING
 THE OGALLALA FORMATION

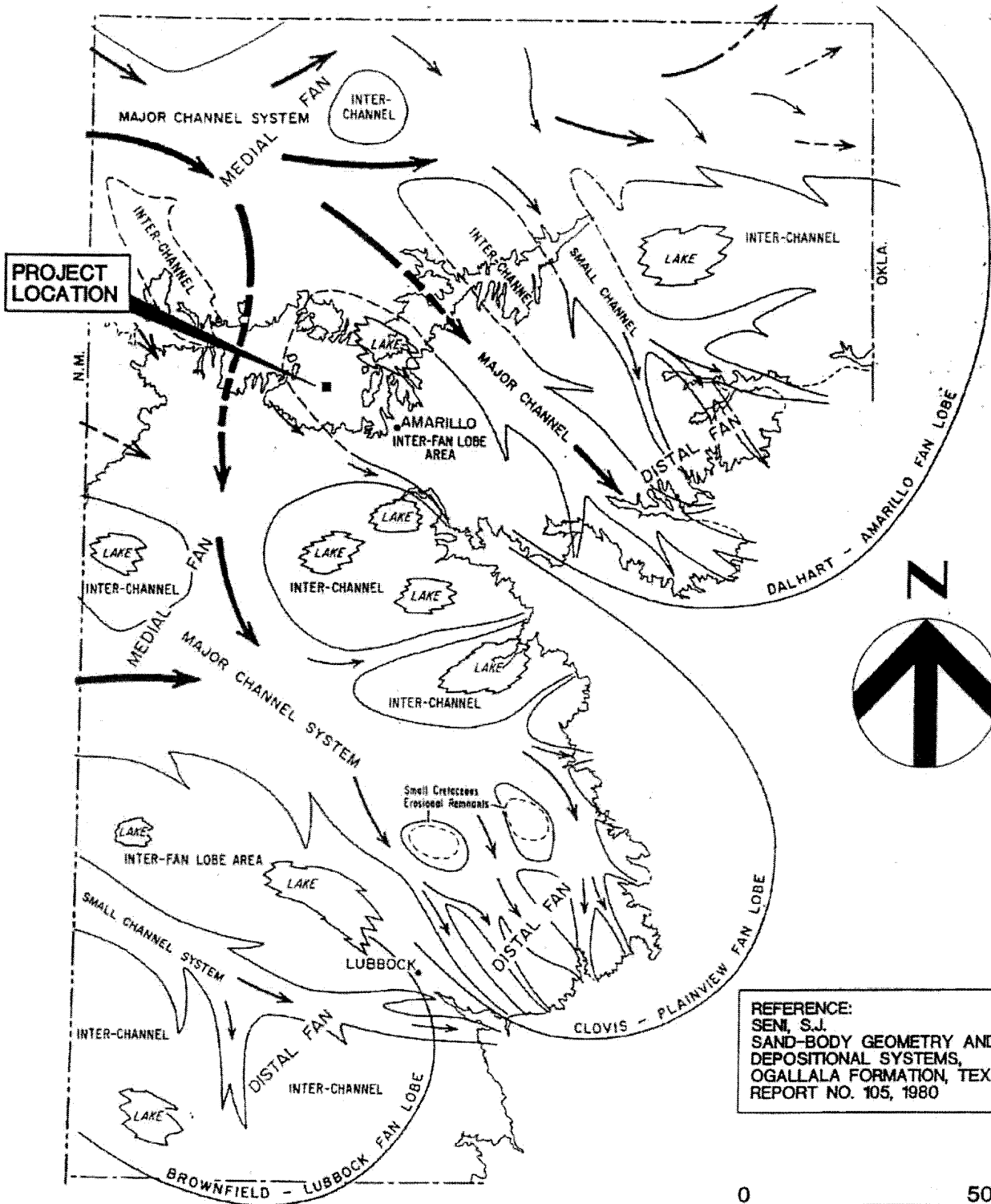
Date

11/94

Figure

8

FILENAME: \AMARILLO\DWG\AMADPFAC



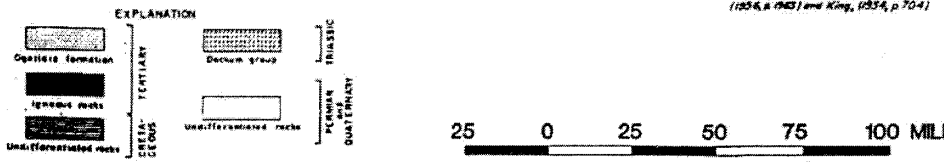
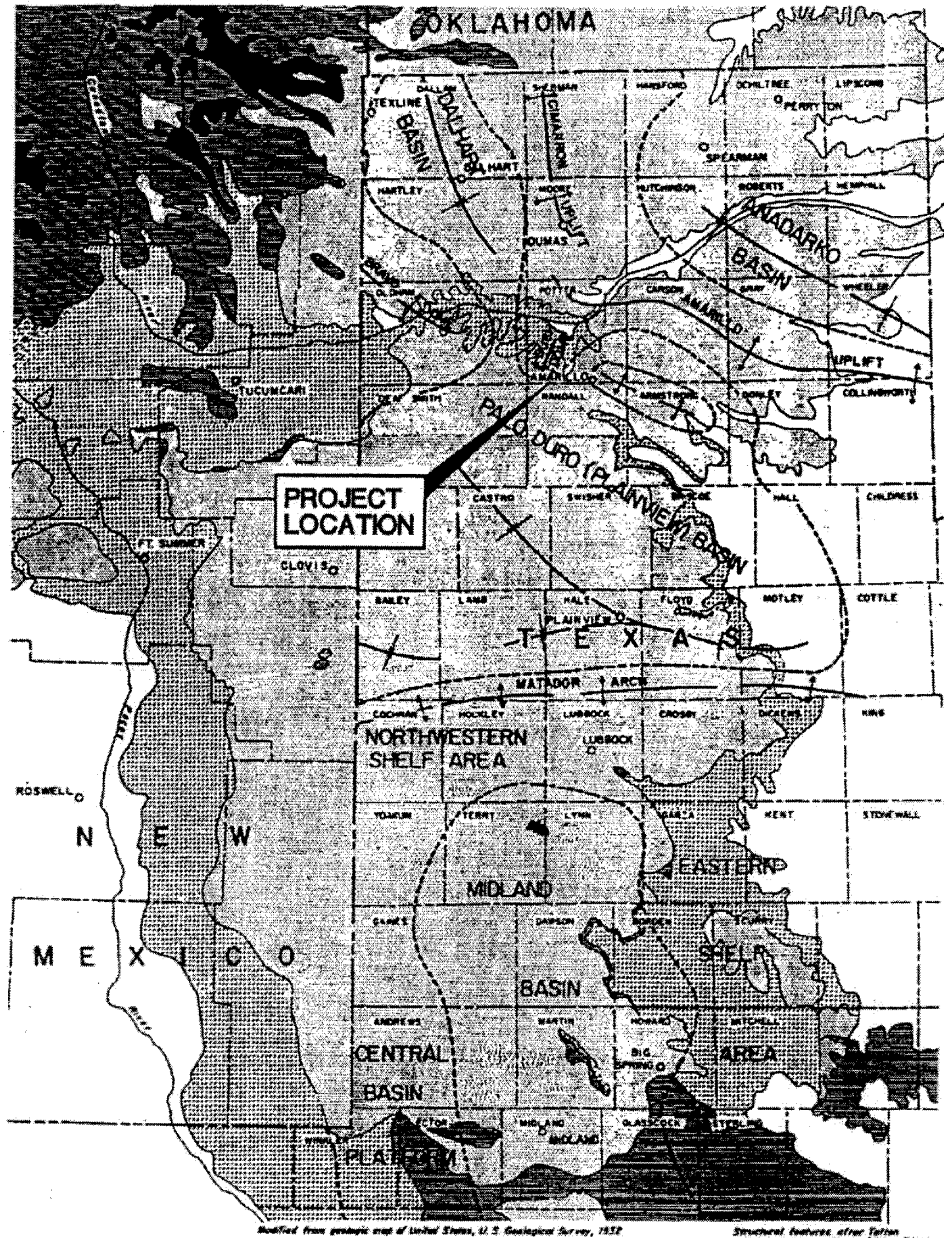
HDR Engineering, Inc.

CITY OF AMARILLO, TEXAS
MUNICIPAL LANDFILL

DEPOSITIONAL FACIES MAP

Date	11/94
Figure	9

FILENAME: \MARGSTC



REFERENCE: CRONIN, J.G.
 A SUMMARY OF THE OCCURRENCE AND DEVELOPMENT
 OF GROUNDWATER IN THE SOUTHERN HIGH PLAINS
 OF TEXAS, TEXAS BOARD OF WATER ENGINEERS,
 BULLETIN 6107, 1971.



CITY OF AMARILLO, TEXAS
 MUNICIPAL LANDFILL

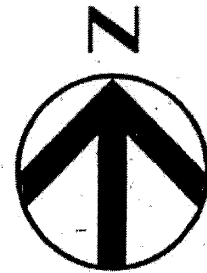
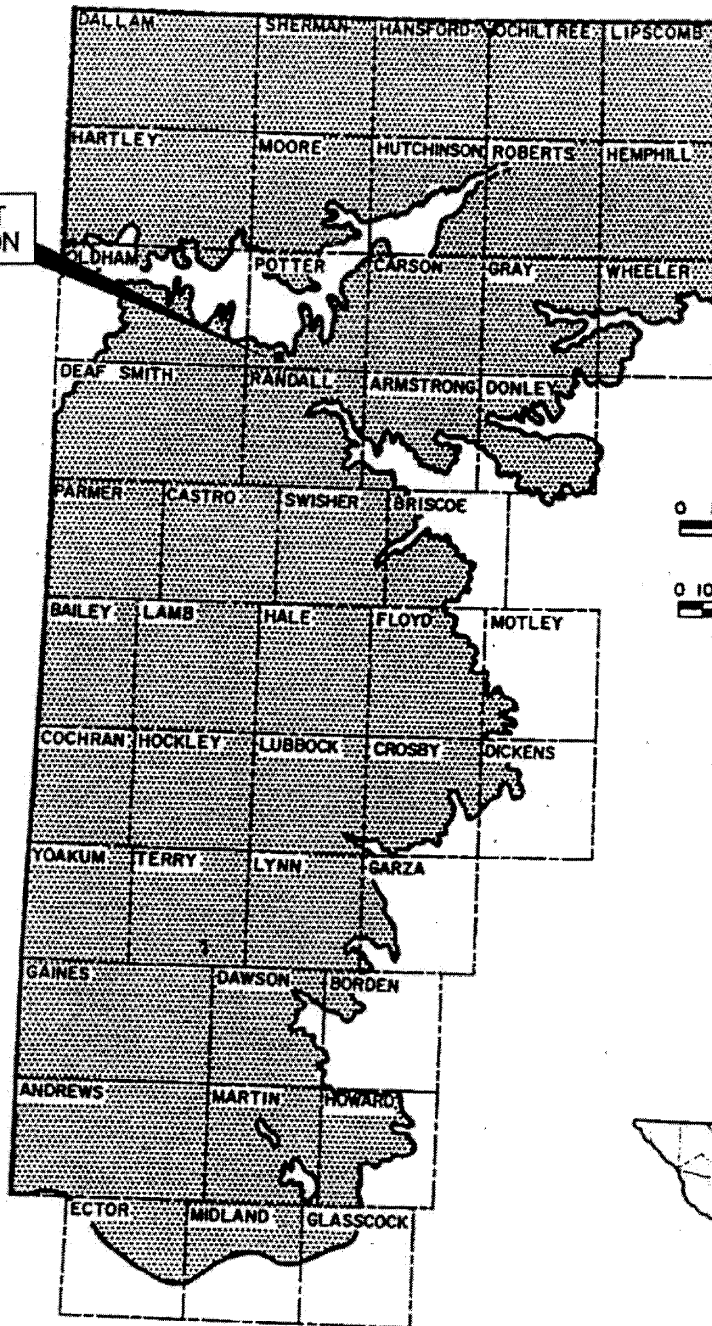
HDR Engineering, Inc.

REGIONAL STRUCTURE MAP

Date	11/94
Figure	10

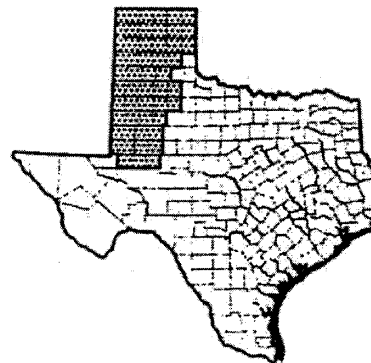
FILENAME: E:\AMARILLO\DWG\AMAFIG1

PROJECT LOCATION



0 10 20 30 40 50 60 70 Miles

0 10 30 50 70 Kilometers



MAP SOURCE:
 EVALUATING THE GROUNDWATER RESOURCES OF THE HIGH PLAINS OF TEXAS,
 FINAL REPORT, VOL. I, AUGUST, 1982.
 TEXAS DEPARTMENT OF WATER RESOURCES



HDR Engineering, Inc.

CITY OF AMARILLO, TEXAS
 MUNICIPAL LANDFILL

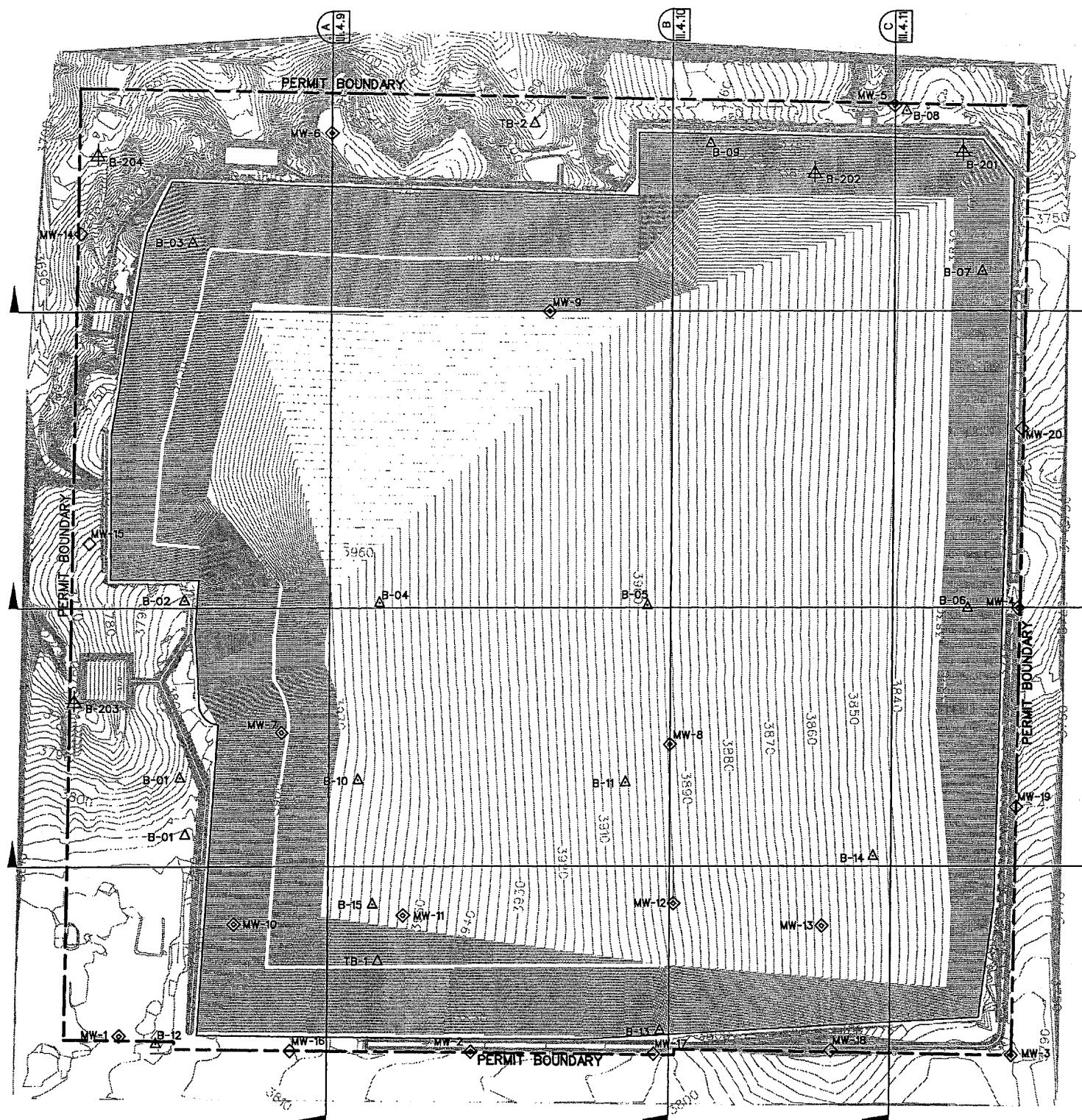
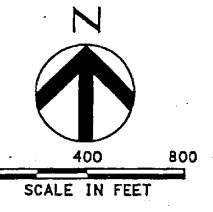
HIGH PLAINS AQUIFER

Date

11/94

Figure

11



- LEGEND**
- PERMIT BOUNDARY
 - MW-1 ◊ MONITORING WELL LOCATIONS
 - B-07 ▲ 1975 BORING LOCATIONS
 - B-201 ▲ 2005 BORING LOCATIONS
 - TB-2 ▲ 1994 BORING LOCATIONS
 - MW-15 ◊ PROPOSED MONITORING WELL

- NOTES:**
1. THE PROPOSED GRADES REPRESENT THE FINAL CONTOURS (TOP OF FINAL COVER).
 2. PROPERTY BOUNDARY INFORMATION BASED ON BOUNDARY SURVEY DATA PROVIDED BY THE CITY OF AMARILLO.

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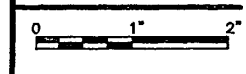


ISSUE	DATE	DESCRIPTION

PROJECT MANAGER	M. DAVISON
CIVIL ENGINEER	M. DAVISON
CHECKED BY	M. ODEN
DESIGNED	S. MILLER
DRAWN BY	B. GREEN
QA/QC	M. ODEN
PROJECT NUMBER	23358-037

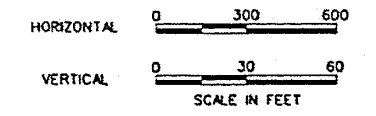
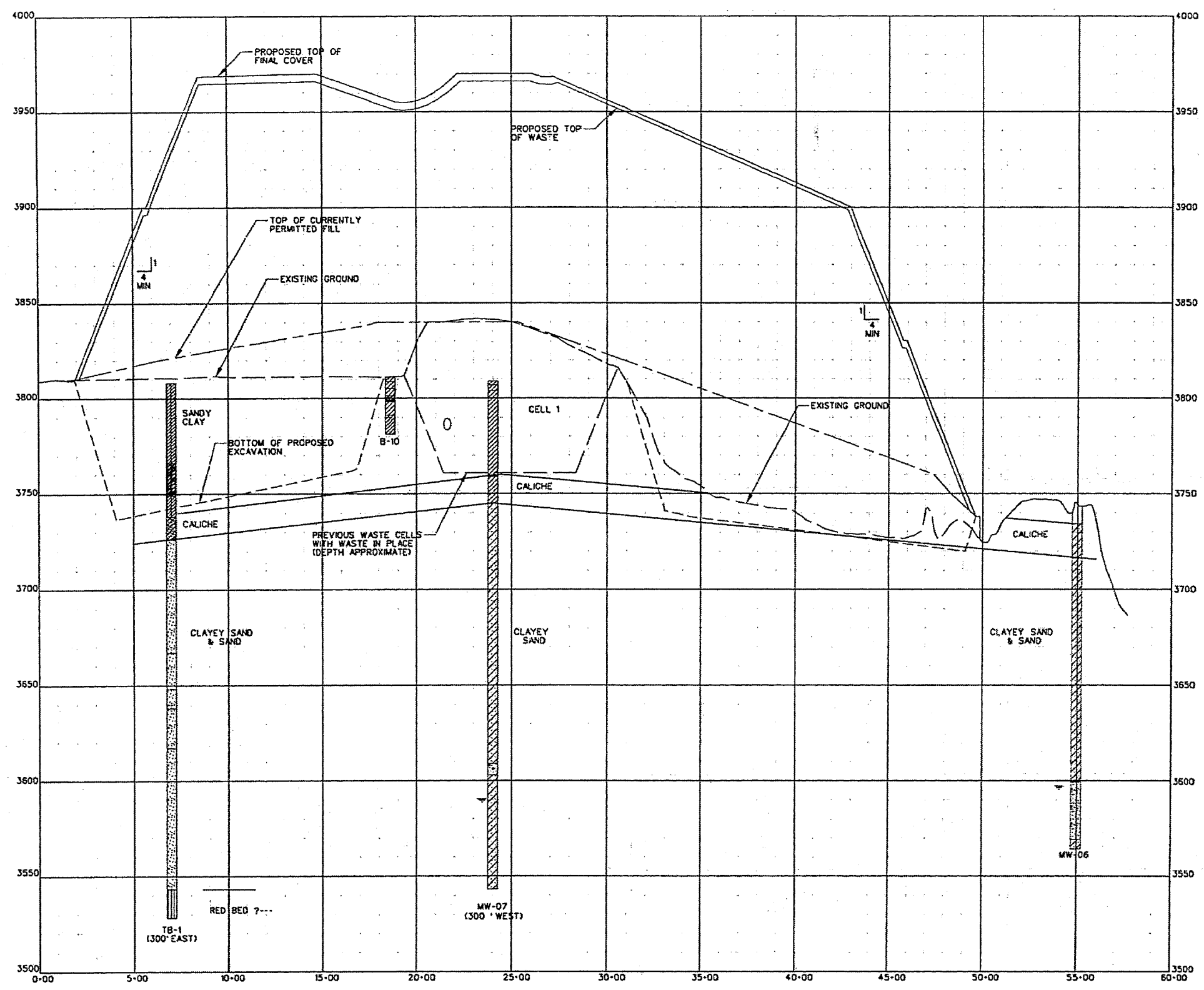
**CITY OF AMARILLO LANDFILL
 MSW PERMIT NO. 73A
 POTTER COUNTY, TEXAS**

CROSS-SECTION LOCATION MAP

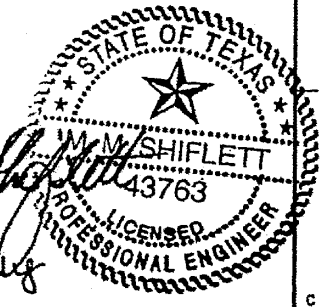


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SHEET
**Plate 8
 App. 4C**

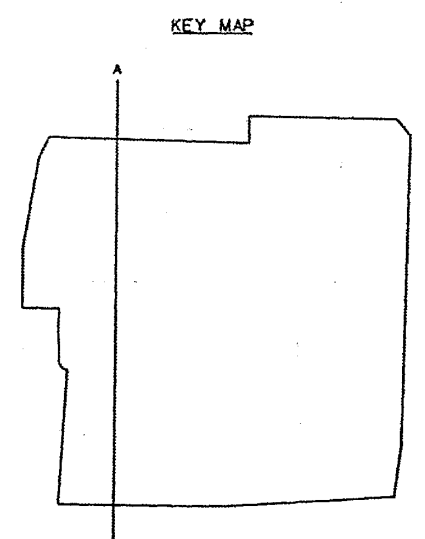


Michael C. Shiflett
 - for subsurface information only

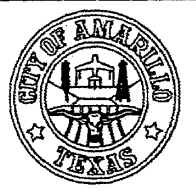


- BORING LEGEND**
- CLAY
 - SANDY CLAY
 - TOP SOIL
 - SAND
 - CALICHE

NOTE
 THE STRATA LINES ARE BASED UPON INTERPOLATION BETWEEN BORINGS, AND MAY NOT REPRESENT ACTUAL SUBSURFACE CONDITIONS.

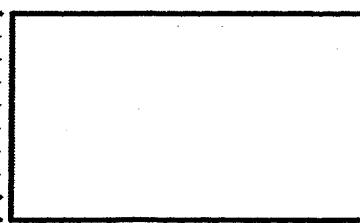


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ISSUE	DATE	DESCRIPTION

PROJECT MANAGER	M. DAVISON
CIVIL ENGINEER	M. DAVISON
CHECKED BY	M. ODEN
DESIGNED	S. MILLER
DRAWN BY	B. GREEN
QA/QC	M. ODEN
PROJECT NUMBER	23358-037



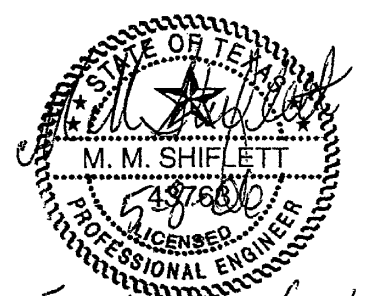
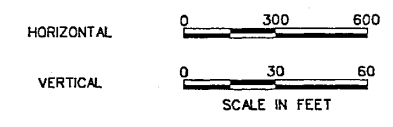
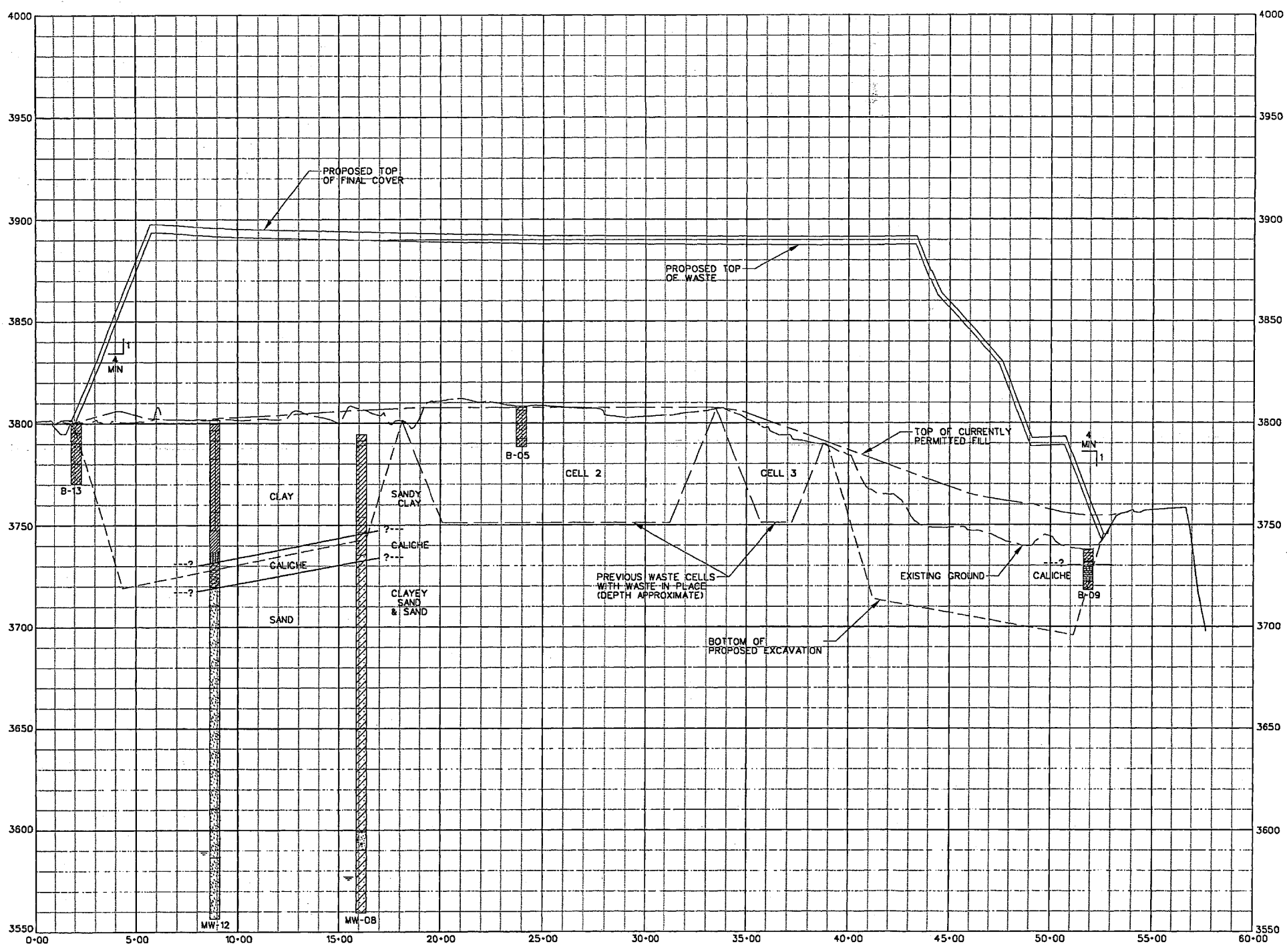
**CITY OF AMARILLO LANDFILL
 MSW PERMIT NO. 73A
 POTTER COUNTY, TEXAS**

SECTION A-A

0 1" 2"

FILENAME: \$\$\$FILE\$\$\$
 SCALE: _____

SHEET
**Plate 9
 App. 4C**



For subsurface information only.

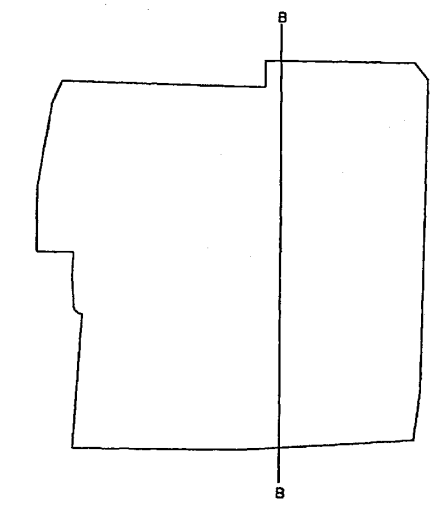
BORING LEGEND

- CLAY
- SANDY CLAY
- TOP SOIL
- CEMENTED CALICHE
- CEMENTED LIMESTONE WITH CALICHE
- SILTY CLAY
- CALICHE
- SAND
- STATIC WATER LEVEL

NOTE:

1. THE STRATA LINES ARE BASED UPON INTERPOLATION BETWEEN BORINGS, AND MAY NOT REPRESENT ACTUAL SUBSURFACE CONDITIONS.

KEY MAP



SECTION B
III. 4. 8

DATE: \$\$\$DATE\$\$\$
TIME: \$\$\$TIME\$\$\$
USER: \$\$\$USER\$\$\$
FILE: \$\$\$FILE\$\$\$

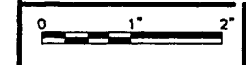


ISSUE	DATE	DESCRIPTION

PROJECT MANAGER	M. DAVISON
CIVIL ENGINEER	M. DAVISON
CHECKED BY	M. ODEN
DESIGNED	S. MILLER
DRAWN BY	B. GREEN
QA/QC	M. ODEN
PROJECT NUMBER	23358-037

**CITY OF AMARILLO LANDFILL
MSW PERMIT NO. 73A
POTTER COUNTY, TEXAS**

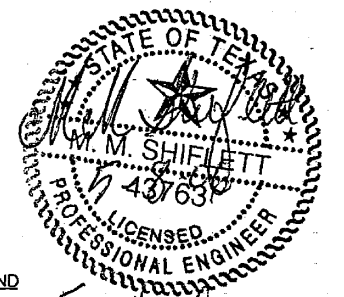
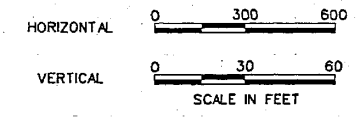
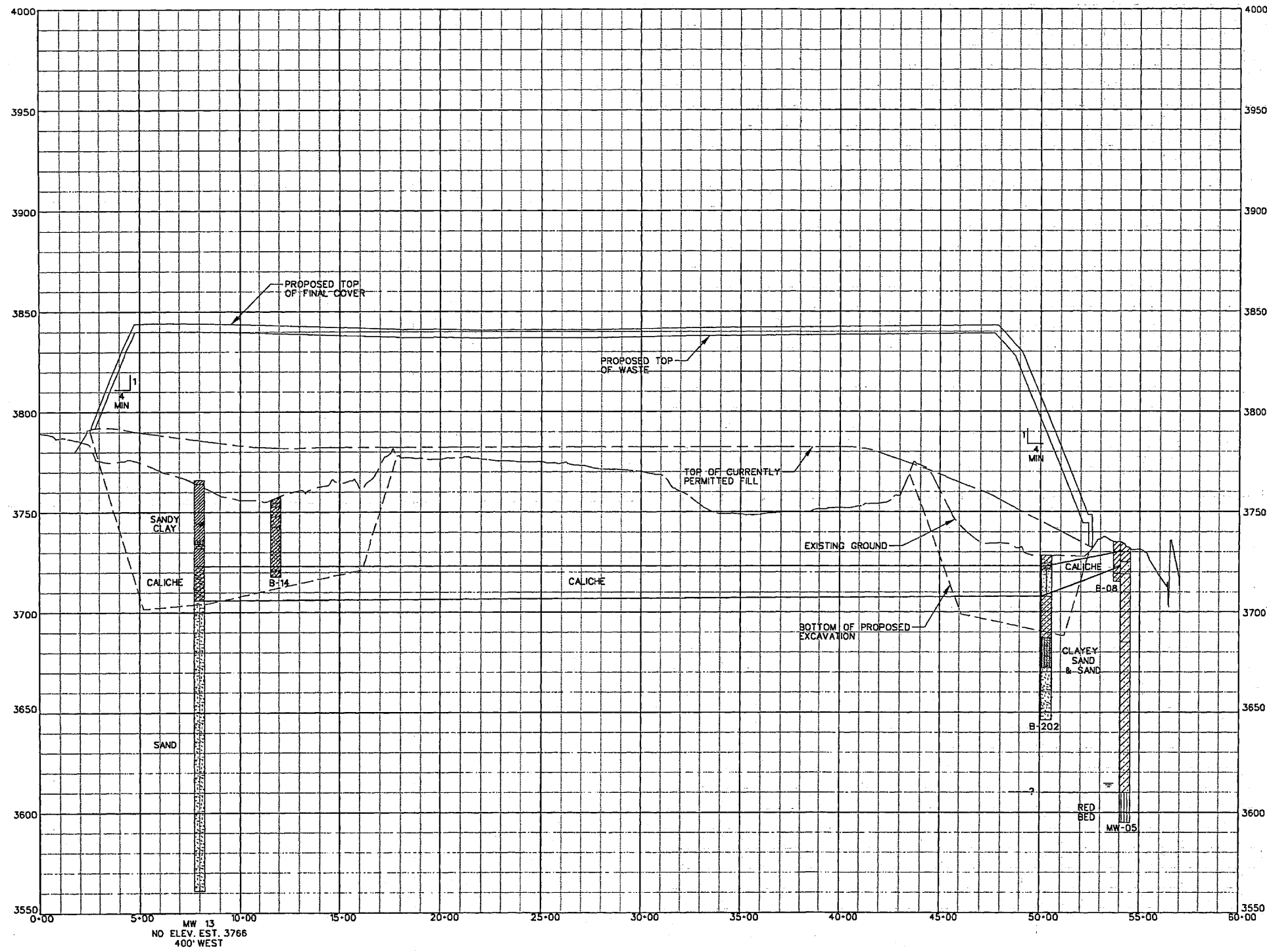
SECTION B-B



FILENAME	\$\$\$FILE\$\$\$
SCALE	

SHEET
Plate 10
App. 4C

1 2 3 4 5 6 7 8

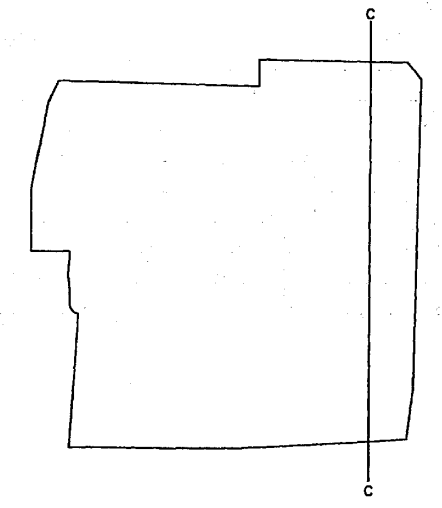


- BORING LEGEND**
- CLAY
 - SANDY CLAY
 - SILTY CLAY
 - SILTY SANDSTONE
 - SAND
 - CALICHE

For subsurface information only

NOTE:
 1. THE STRATA LINES ARE BASED UPON INTERPOLATION BETWEEN BORINGS, AND MAY NOT REPRESENT ACTUAL SUBSURFACE CONDITIONS.

KEY MAP



SECTION C-C
 III.4.B

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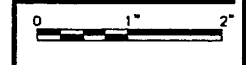


ISSUE	DATE	DESCRIPTION

PROJECT MANAGER	M. DAWSON
CIVIL ENGINEER	M. DAWSON
CHECKED BY	M. ODEN
DESIGNED	S. MILLER
DRAWN BY	B. GREEN
QA/QC	M. ODEN
PROJECT NUMBER	23358-037

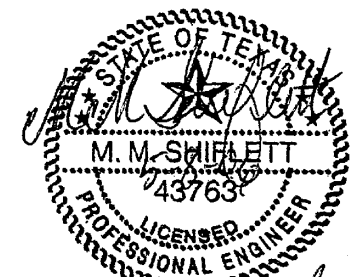
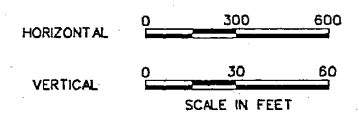
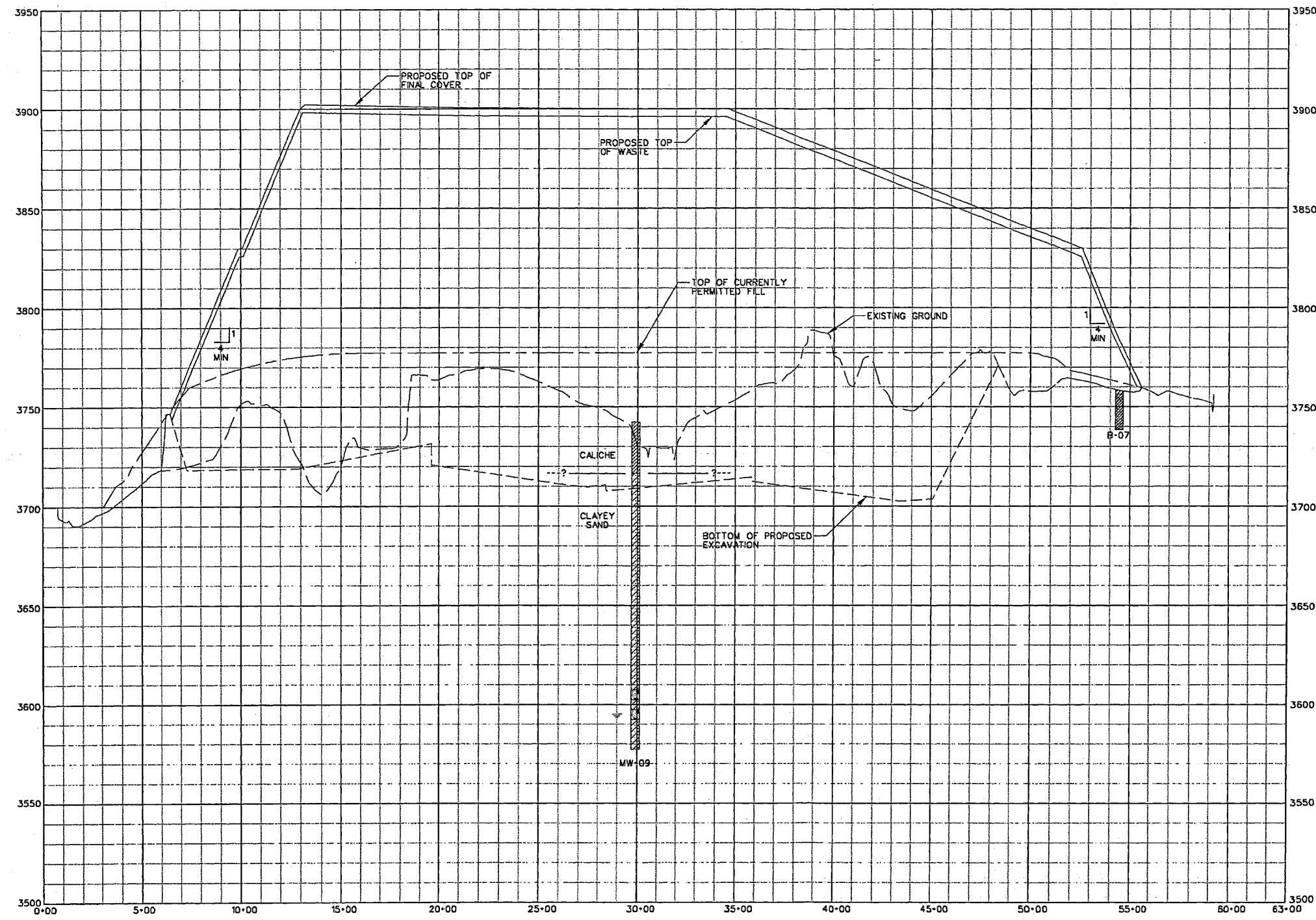
CITY OF AMARILLO LANDFILL
 MSW PERMIT NO. 73A
 POTTER COUNTY, TEXAS

SECTION C-C



FILENAME: \$\$\$FILE\$\$\$
 SCALE: _____

SHEET Plate 11
 App. 4C

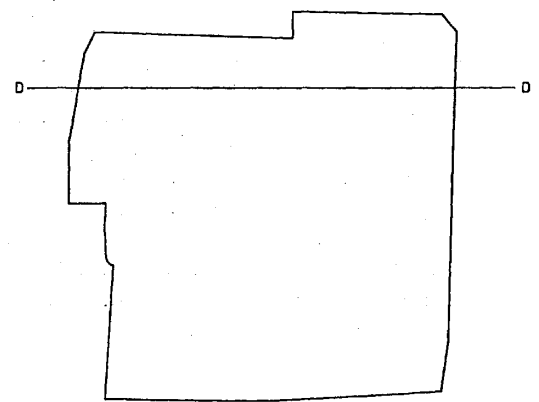


For subsurface information only

- BORING LEGEND**
- CLAY
 - SANDY CLAY
 - TOP SOIL
 - CALICHE

NOTE:
 1. THE STRATA LINES ARE BASED UPON INTERPOLATION BETWEEN BORINGS, AND MAY NOT REPRESENT ACTUAL SUBSURFACE CONDITIONS.

KEY MAP



SECTION D
 III, 4, 8

DATE: \$\$DATE\$\$
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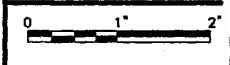


ISSUE	DATE	DESCRIPTION

PROJECT MANAGER	M. DAVISON
CIVIL ENGINEER	M. DAVISON
CHECKED BY	M. ODEN
DESIGNED	S. MILLER
DRAWN BY	B. GREEN
QA/QC	M. ODEN
PROJECT NUMBER	23358-037

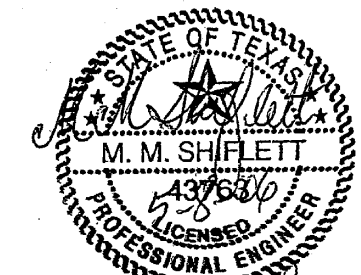
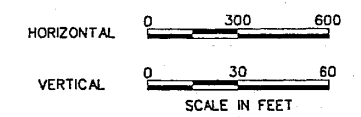
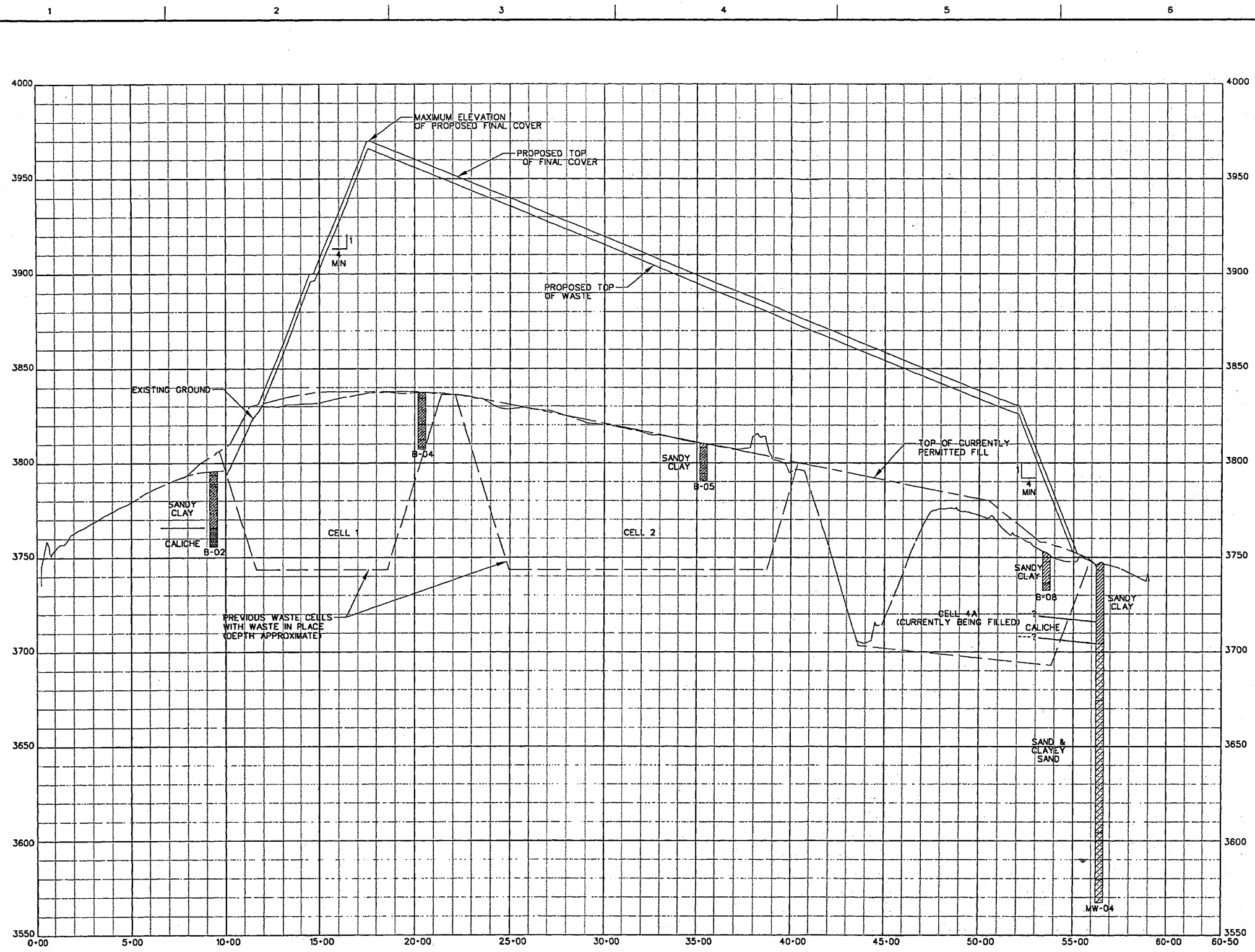
**CITY OF AMARILLO LANDFILL
 MSW PERMIT NO. 73A
 POTTER COUNTY, TEXAS**

SECTION D-D



FILENAME: \$\$FILE\$\$
 SCALE:

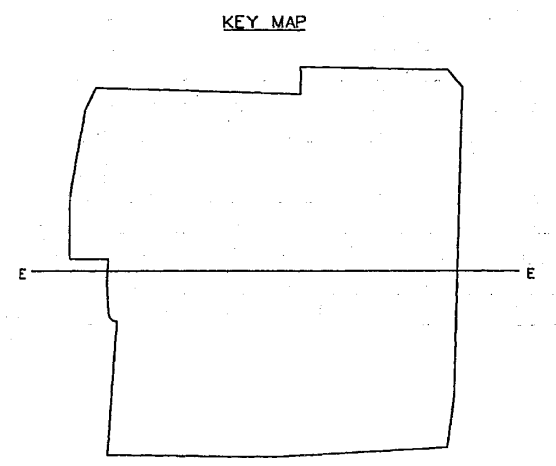
SHEET
Plate 12
App. 4C



For subsurface information only

- BORING LEGEND**
- CLAY
 - SANDY CLAY
 - TOP SOIL
 - CEMENTED LIMESTONE WITH CALICHE
 - CALICHE

NOTE:
 1. THE STRATA LINES ARE BASED UPON INTERPOLATION BETWEEN BORINGS, AND MAY NOT REPRESENT ACTUAL SUBSURFACE CONDITIONS.



SECTION E
 III. 4. 8

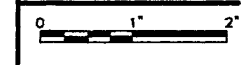
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ISSUE	DATE	DESCRIPTION

PROJECT MANAGER	M. DAVISON
CIVIL ENGINEER	M. DAVISON
CHECKED BY	M. ODEN
DESIGNED	S. MILLER
DRAWN BY	B. GREEN
QA/QC	M. ODEN
PROJECT NUMBER	23358-037

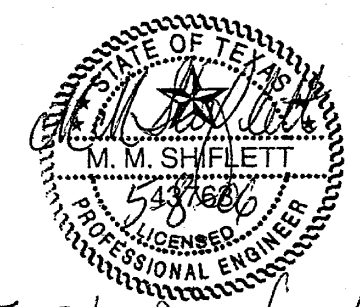
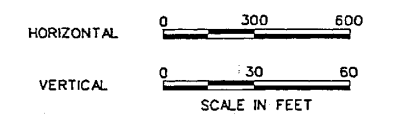
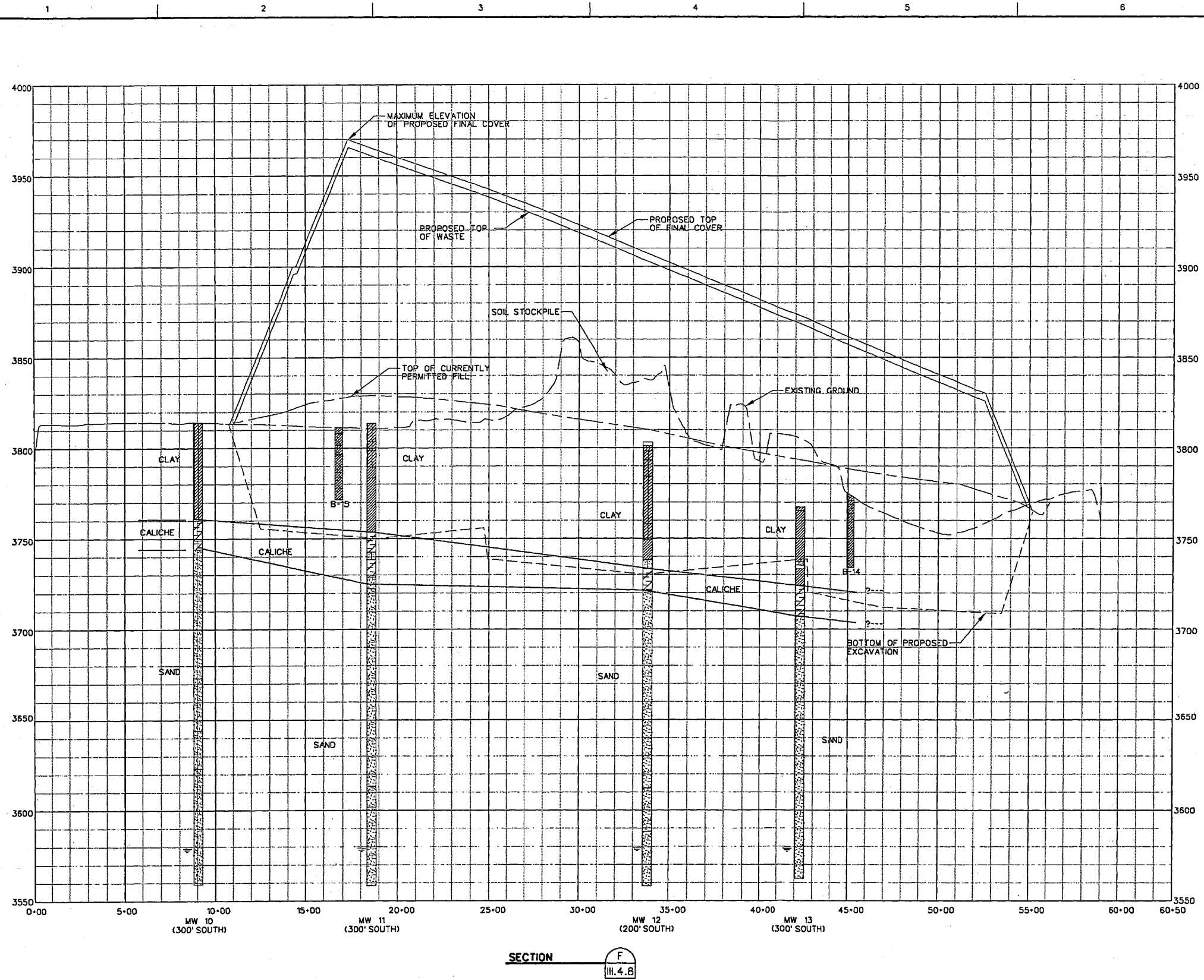
CITY OF AMARILLO LANDFILL
 MSW PERMIT NO. 73A
 POTTER COUNTY, TEXAS



FILENAME: \$\$FILE\$\$
 SCALE:

SHEET
Plate 13
App. 4C

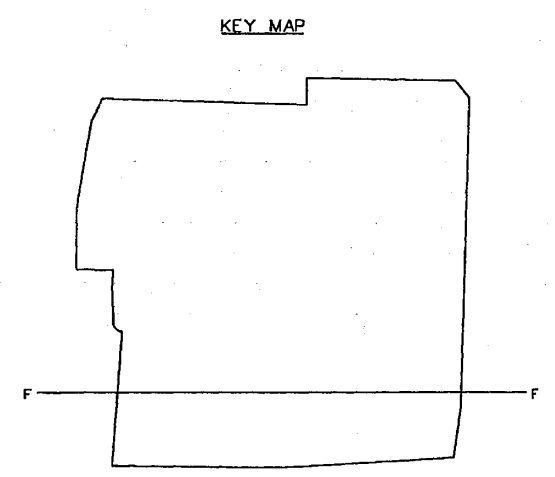
SECTION E-E



For Subsurface information only

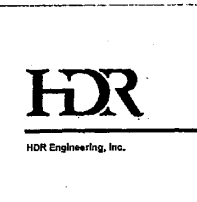
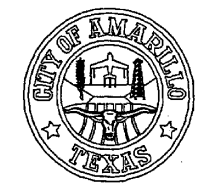
- BORING LEGEND**
- CLAY
 - SANDY CLAY
 - TOP SOIL
 - SILTY CLAY
 - SAND
 - CALICHE

NOTE:
 1. THE STRATA LINES ARE BASED UPON INTERPOLATION BETWEEN BORINGS, AND MAY NOT REPRESENT ACTUAL SUBSURFACE CONDITIONS.



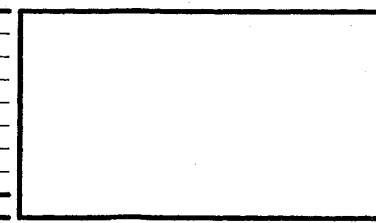
SECTION F
 III.4.B

USER: \$\$\$USER\$\$\$
 FILE: \$\$\$FILE\$\$\$
 DATE: \$\$\$DATE\$\$\$
 TIME: \$\$\$TIME\$\$\$



ISSUE	DATE	DESCRIPTION

PROJECT MANAGER	M. DAVISON
CIVIL ENGINEER	M. DAVISON
CHECKED BY	M. ODEN
DESIGNED	S. MILLER
DRAWN BY	B. GREEN
QA/QC	M. ODEN
PROJECT NUMBER	23358-037



**CITY OF AMARILLO LANDFILL
 MSW PERMIT NO. 73A
 POTTER COUNTY, TEXAS**

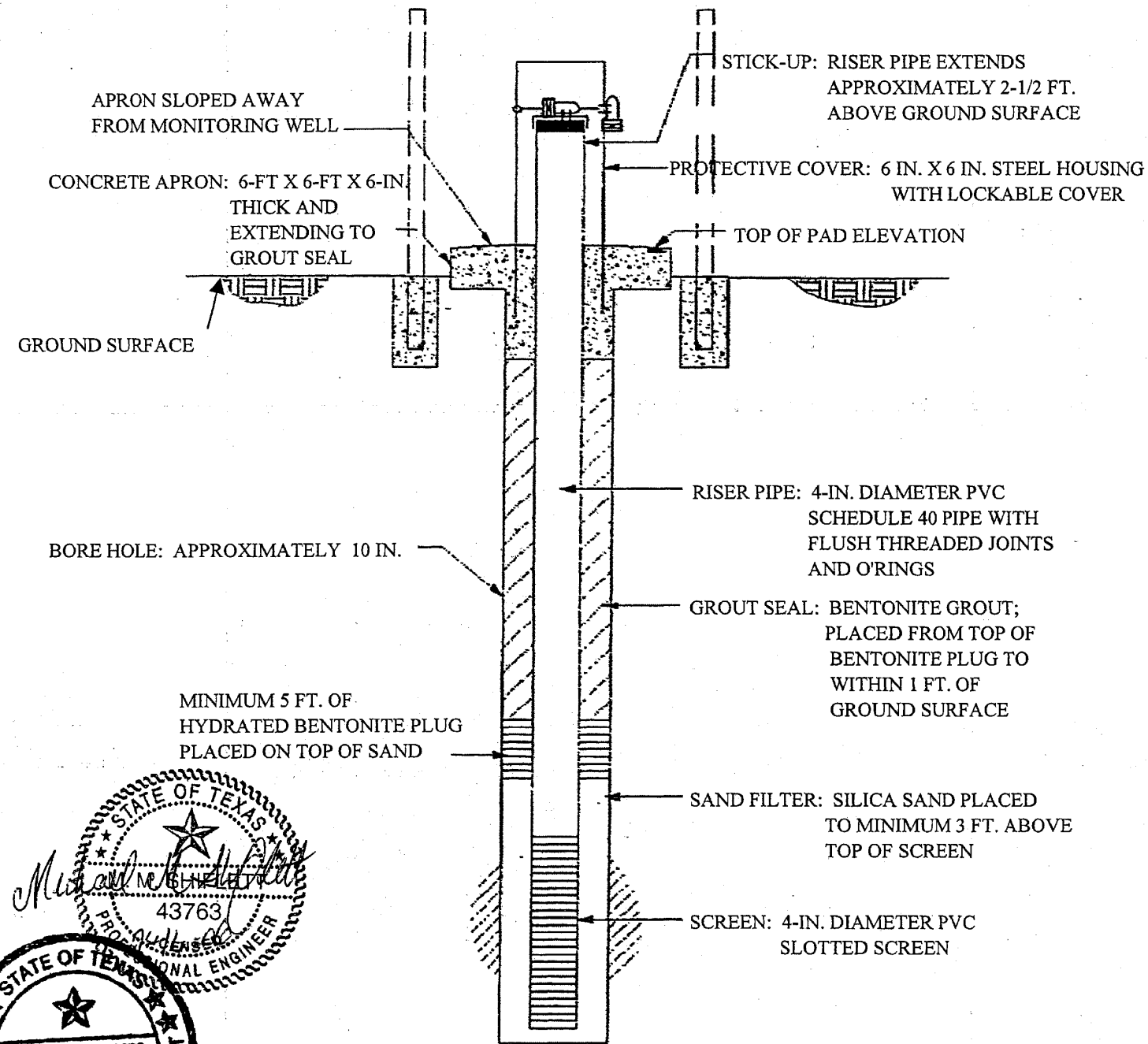
SECTION F-F

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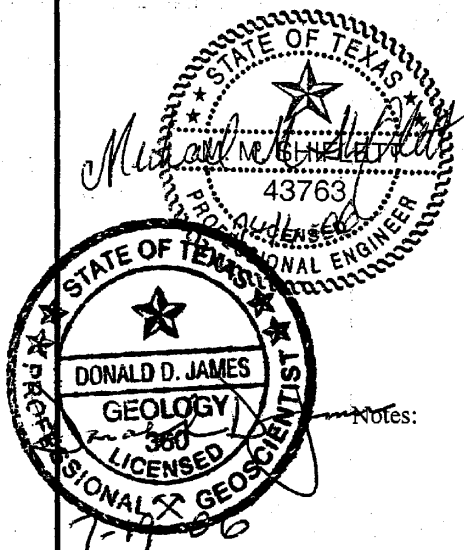
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SHEET Plate 14
 App. 4C

TYPICAL MONITORING WELL DETAIL



- Notes:
1. Typical Monitoring Well Detail as provided in the 1994 document. Table has been updated with current information.
 2. Actual monitoring depths to be confirmed at time of well installation with pilot borings.
 3. Monitoring Well locations as presented on this plate will provide the groundwater monitoring well system.



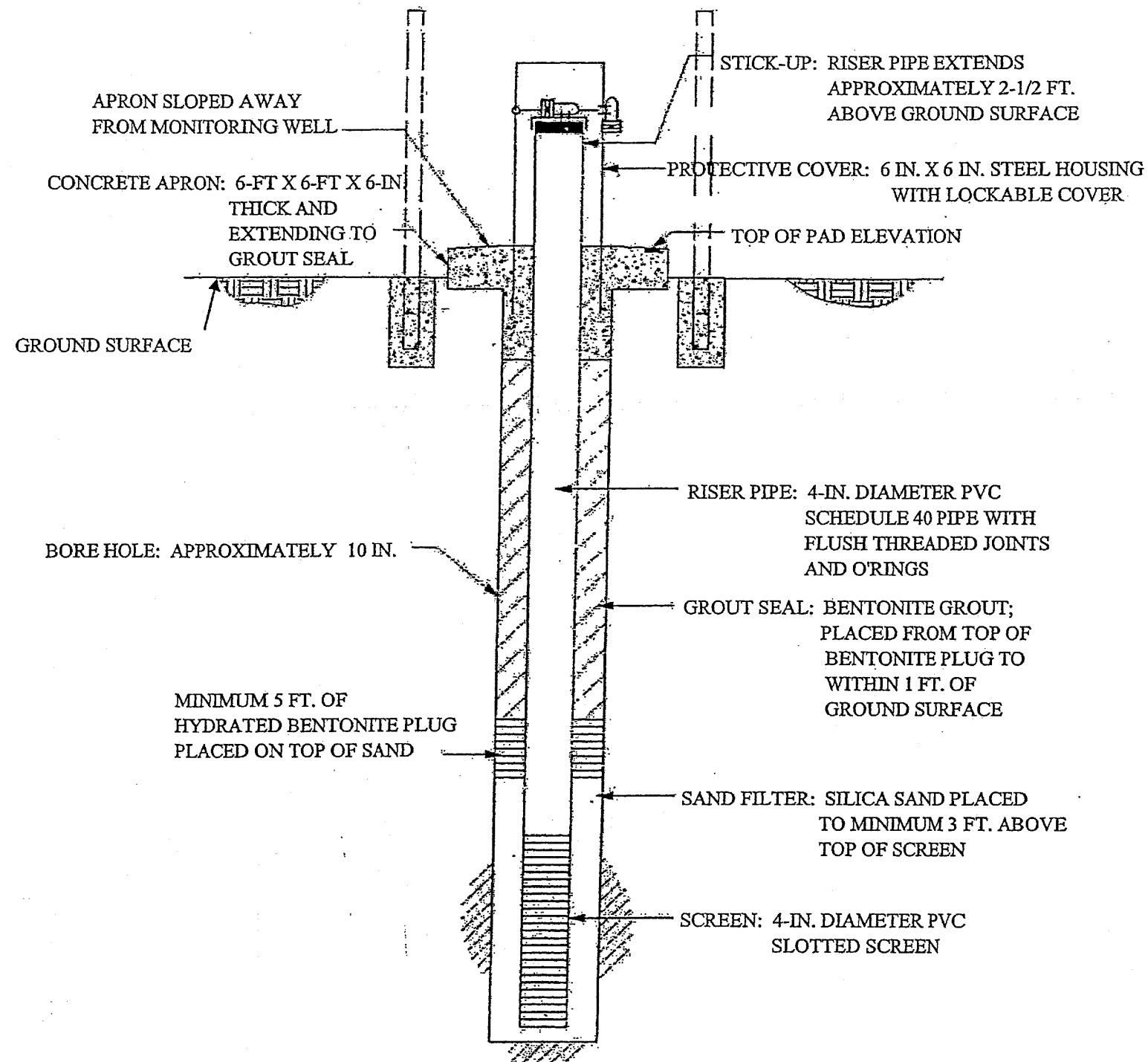
EXISTING MONITORING WELL NETWORK City of Amarillo Landfill, 2005

Monitoring Well No.	Ground Elevation	Bottom Elevation	Screened Interval		Top of Filter Pack Elevation	Top of Bentonite Seal Elevation
			From	To		
Upgradient Monitoring Wells						
MW-5	3736.64	3596.64	3651.64	3596.64	3656.64	3661.64
MW-6	3746.38	3570.38	3610.38	3570.38	3617.38	3622.38
Downgradient Monitoring Wells						
MW-1	3814.85	3561.65	3601.85	3561.65	3606.85	3611.85
MW-2	3805.39	3560.39	3600.39	3560.39	3605.39	3610.39
MW-3	3789.57	3542.57	3582.57	3542.57	3589.57	3594.57
MW-4	3746.88	3564.88	3604.88	3564.88	3610.88	3615.88

ADDITIONAL MONITORING WELLS City of Amarillo Landfill, 2005 (See Note 2)

Monitoring Well No.	Estimated Ground Elevation	Bottom Elevation	Screened Interval		Top of Filter Pack Elevation	Top of Bentonite Seal Elevation
			From	To		
Upgradient Monitoring Wells						
MW-14	3705	3550	3588	3552	3591	3596
MW-15	3775	3549	3585	3549	3588	3593
Downgradient Monitoring Wells						
MW-16	3810	3540	3577	3540	3580	3585
MW-17	3800	3540	3577	3540	3580	3585
MW-18	3780	3540	3577	3540	3580	3585
MW-19	3766	3540	3580	3540	3585	3588
MW-20	3752	3540	3589	3550	3592	3597

TYPICAL MONITORING WELL DETAIL



- Notes:
1. Typical Monitoring Well Detail as provided in the 1994 document. Table has been updated with current information.
 2. Actual monitoring depths to be confirmed at time of well installation with pilot borings.

EXISTING MONITORING WELL NETWORK City of Amarillo Landfill, 2005

Monitoring Well No.	Ground Elevation	Bottom Elevation	Screened Interval		Top of Filter Pack Elevation	Top of Bentonite Seal Elevation
			From	To		
Upgradient Monitoring Wells						
MW-5	3736.64	3596.64	3651.64	3596.64	3656.64	3661.64
MW-6	3746.38	3570.38	3610.38	3570.38	3617.38	3622.38
Downgradient Monitoring Wells						
MW-1	3814.85	3561.65	3601.85	3561.65	3606.85	3611.85
MW-2	3805.39	3560.39	3600.39	3560.39	3605.39	3610.39
MW-3	3789.57	3542.57	3582.57	3542.57	3589.57	3594.57
MW-4	3746.88	3564.88	3604.88	3564.88	3610.88	3615.88

ADDITIONAL MONITORING WELLS City of Amarillo Landfill, 2005 (See Note 2)

Monitoring Well No.	Estimated Ground Elevation	Bottom Elevation	Screened Interval		Top of Filter Pack Elevation	Top of Bentonite Seal Elevation
			From	To		
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MW-14	3705	3550	3588	3552	3591	3596
MW-15	3775	3549	3585	3549	3588	3593
Downgradient Monitoring Wells						
MW-16	3810	3540	3577	3540	3580	3585
MW-17	3800	3540	3577	3540	3580	3585
MW-18	3780	3540	3577	3540	3580	3585
MW-19	3766	3540	3580	3540	3585	3588
MW-20	3752	3540	3589	3550	3592	3597



1999 – Dyess – Peterson Testing Laboratory, Inc.

Logs of Borings PP-8 through PP-12

